

**DEVELOPMENT OF A DECISION SUPPORT SYSTEM
FOR FLOOD CONTROL MANAGEMENT**

by

Kwame A. Agyare

A Thesis
Submitted to the Faculty of Graduate Studies
in Partial Fulfillment of the Requirements
for the Degree of
MASTER OF SCIENCE
IN
CIVIL ENGINEERING

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Winnipeg, Manitoba

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ABSTRACT

A decision support system which can assist in the process of generating and evaluating alternative flood control measures for flood management is developed. The system incorporates the technologies of geographic information systems and expert systems, both of which have achieved recent successful application in several aspects of watershed management, and integrates these tools with the use of a relational database management software and optimization to facilitate the generation and selection of suitable flood control solutions. The system takes advantage of the increases in computing power currently available to the everyday user to enhance the intercommunication between each module for improved system design and operation.

A case study of the application of the decision support system to a flood management problem located near the City of Winnipeg flood control system is subsequently carried out. Several suitable flood control alternatives are generated for the area, and a methodology by which these solutions may be evaluated is put forward. Final results confirm the usefulness of developing such integrated tools to address the flood management problem and indicate that such tools can aid in the comprehension, analysis, generation and evaluation processes.

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TABLE OF CONTENTS

	Page
ABSTRACT	i
ACKNOWLEDGEMENTS	ii
LIST OF FIGURES	vii
LIST OF TABLES	viii
1. INTRODUCTION.	1
1.1 Statement of the problem.	1
1.2 Flood control planning.	4
1.3 Scope of the work.	6
2. LITERATURE REVIEW	7.
2.1 Decision support systems in water resources.	7
2.1.1 DSS in planning and management.	8
2.1.2 Expert systems within DSS.	11
2.2 Use of geographic information systems.	11
2.2.1 Watershed management using GIS.	13
2.2.2 Model data input using GIS.	14
3. DECISION SUPPORT SYSTEM DEVELOPMENT.	15
3.1 Architecture of the DSS.	15
3.2 DSS operating platform.	18
3.3 DSS shell / system manager.	19
3.3.1 NEXPERT OBJECT.	19
3.4 Modelbase component.	20

3.4.1	GRASS.	20
3.4.2	SID	22
3.4.2	EAD.	22
3.5	Display / graphics subsystem.	23
3.5.1	ORACLE	23
3.6	Database component.	24
3.7	Expert system component.	24
4.	DECISION SUPPORT SYSTEM OPERATION.	25
4.1	Flood damage analysis procedure.	25
4.2	Generating initial community status.	25
4.2.1	Field survey.	28
4.2.2	Geographic data input.	28
4.2.3	Updating the relational database.	29
4.3	Pre-disaster analysis.	31
4.3.1	Interactive modelling.	31
4.4	Generating flood management alternatives.	35
4.5	Post-disaster analysis.	36
4.5.1	Interactive modelling.	36
4.5.2	Flooding consequences	37
5.	CASE STUDY - GREATER WINNIPEG AREA FLOOD MANAGEMENT	40
5.1	Introduction.	40
5.2	Data acquisition, formatting and input.	43
5.3	Structure inventory analysis.	47
5.4.	Damage analysis.	51

5.5	Cost computation.	53
6.	DISCUSSION OF RESULTS.	54
6.1	Damage computation results.	54
6.2	Spatial interpretation.	58
7.	CONCLUSIONS AND RECOMMENDATIONS.	62
	REFERENCES	65
	APPENDIX A: Database Inventory commands	
	A1: Glossary of database fields	
	A2: Command for creating database tables	
	A3: Commands for loading data from GRASS	
	A4: Commands to output data from database	
	A5: Commands to update the database	
	APPENDIX B: Expert Systems consultations	
	B1: SID consultation	
	B2: EAD consultation	
	APPENDIX C: Fortran Programs	
	C1: Fortran Programs for formatting SID files	
	C2: Fortran Programs for formatting EAD files	

APPENDIX D: Input and Output Files

- D1: Input files for SID**
- D2: Output files for SID**
- D3: Input Files for EAD**
- D4: Output files for EAD**

APPENDIX E: Structure Inventory Listings

LIST OF FIGURES

		Page
1	Flood control management process	5
2	Proposed architectural design of DSS using a modular approach	17
3	Rule editor in NEXPERT	21
4	Diagram of the flood damage analysis procedure	27
5	Schematic of the backward-chaining process	32
6	Session control window in NEXPERT	33
7	City of Winnipeg and surrounding areas	41
8	Diagram of the study area	42
9	Stage-discharge relationship	47
10	Discharge - probability curve	48
11	Damages for the magnitudes of the 1950, 1970 & 1974 floods.	55
12	Expected annual damages for years 2004, 2024, 2044.	56
13	Equivalent annual damages	56

LIST OF TABLES

		Page
1	Typical map layers contained in a geographical map	29
2	Annual flood peaks	46
3	Stage-discharge relationship	46
4	Feasible flood control measures	49
5	Elevation-damage relationship for alternatives 4,5,7 & 8	51
6	Data for expected annual damage computations	52
7	Damage and estimated annual damage results	52
8	Estimated costs for implementing flood control measures	53

DEVELOPMENT OF A DECISION SUPPORT SYSTEM FOR FLOOD CONTROL MANAGEMENT

1. INTRODUCTION.

1.1 STATEMENT OF THE PROBLEM.

The issue of making optimal planning and policy decisions, in water resources planning and management in general and flood-control management in particular, is one that has received continued attention in recent years. This is in light of the fact that despite millions of dollars being spent each year on both structural and non-structural measures of flood-control, flooding continues to present a hazard in many parts of the world, leading to considerable damage to property and in some cases loss of life.

One main focus in attempts to deal with this problem has been to try to obtain a better and more comprehensive understanding of the cause-effect components of the situation being examined. Many of the problems encountered in water resources, however, are often ill-structured and the very nature of such problems often calls for some form of subjective evaluation or informed judgement, (Fedra and Loucks, 1985), in addition to the use of formal numerical models for their resolution. Problems also arise out of the fact that different groups of affected persons may not agree on what should be the best solution to a prevailing water resources problem.

Several approaches have been made to resolve these particular issues. These include interactively involving users or affected parties in the decision making process, (Loucks et al. 1985), (Johnson, 1990) and the use of an expert systems approach, (Savic and Simonovic, 1991), (Arnold and Sammons, 1988) to bring a high level of expert opinion into the decision-making process.

Recent trends in the solution of such problems have been to aggregate several models, both procedural and heuristic, into integrated software tools which are able to address the relevant parts of the problem domain. Such collections of interactively linked models designed for impact exploration, synthesis and evaluation have been termed decision support systems, (Sprague and Carlson, 1982).

Decision support systems (DSS) have been used in recent water resources studies, (Savic and Simonovic, 1991), (Johnson, 1990), to enhance the interactive modelling process and to aid in providing a more comprehensive understanding of water resources problems.

The development of such integrated software tools has been enhanced in recent years by the increase in the amount of computer power available to the everyday user, and also from the emergence of several technologies such as geographic information systems (GIS) and expert systems (ES) which have been successfully applied to various aspects of water resources, (Muzik, 1988), (Wolfe and Neale, 1988), (Silfer et al, 1987).

At the ninth session of the International Hydrological Programme (IHP) Council held in Paris in 1990, the council, as part of the fourth phase of the IHP (1990-1995), set up a sub-programme to study experiences with modern water resources planning and management methods taking into account risk factors. The objectives of the sub-programme are to demonstrate the usefulness of the application of computer based decision support systems in water resources planning and management and to create within water resources planners and managers, decision makers as well as within the public the need to use interactive decision making and to incorporate risk factors.

The focus of this study is to utilize the advancements in technology in the field of water resources to develop a computer based decision support system which can effectively examine the issues involved in flood management, thus leading to more effective solutions to the flooding problem. This system will combine the use of optimization techniques and other numerical models with GIS, to facilitate spatial decision support, ES and engineering

expertise to facilitate intelligent decision support in the problem domain, and the use of relational database management software to facilitate model data input and data management.

Several important issues need to be addressed in the development of such systems including the effective integration of GIS, ES and numerical modelling in a decision support framework, and the inter-communication between these modules.

Another important issue is that of facilitating data input to numerical models. The use of formal flood plain damage models such as the US Army Corps of Engineers, Flood Damage Analysis package has sometimes been hindered by the daunting task of data acquisition and formatting, and in some instances inadequate time to learn the proper use of such models results in inaccurate results being obtained. Efforts must to be made in the development of any interactive system to provide maximum assistance in data input and formatting to enhance the systems use, and the system to be developed addresses this issue.

The purpose of this research is therefore to develop a decision support system that will assist in providing solutions to flood management problems. The system is intended to address all of the issues described above and to provide the user with comprehensive support in the problem domain. Focus will be given to the role of geographic information systems towards decision-making in the domain of flood management, both as a tool for analysis and also in the role of providing graphical display of spatial data and evaluation of generated alternatives.

Subsequent to the development of the system, a case study of a flood management problem situation, located upstream of the City of Winnipeg flood control system will be performed to investigate the utility of using such a DSS, and recommendations will be made on the integration of this work into the decision-making process.

1.2 FLOOD CONTROL PLANNING.

In order to effectively address the flood control planning process (Figure 1), there is a need to be able to make optimal decisions at every point in the process. The engineering component of the process begins with the definition of engineering objectives from addressing the social needs and objectives given, through the design of the selected flood control measure or measures, to the management of the operational system. The generation and evaluation of alternative flood control measures is of prime concern in this area. It is often in this area where decisions based on poor judgement or the failure to examine all possible flood control solutions to a problem may lead to failure of the generated solution. The use of incorrect data as well as inefficient data management during the modelling process may also lead to inadequate or overdesigned solutions.

It is in these particular areas of the planning process i.e. from the process of specifying engineering objectives to the selection of an appropriate flood control plan, where this research work will focus on designing an interactive computer based decision support system to help formulate and evaluate optimal solutions towards aiding in the planning process.

Utilizing a decision support system in this area will bring into the analytical process efficient data handling and management techniques coupled with the efficient use of models both analytical and heuristic as well as a systematic, hierarchical and modular approach to the process of alternative evaluation, which would lead to better proposals being made. It is the intention in this research work to develop such a system which would provide these capabilities, resulting in optimal flood control planning and management solutions.

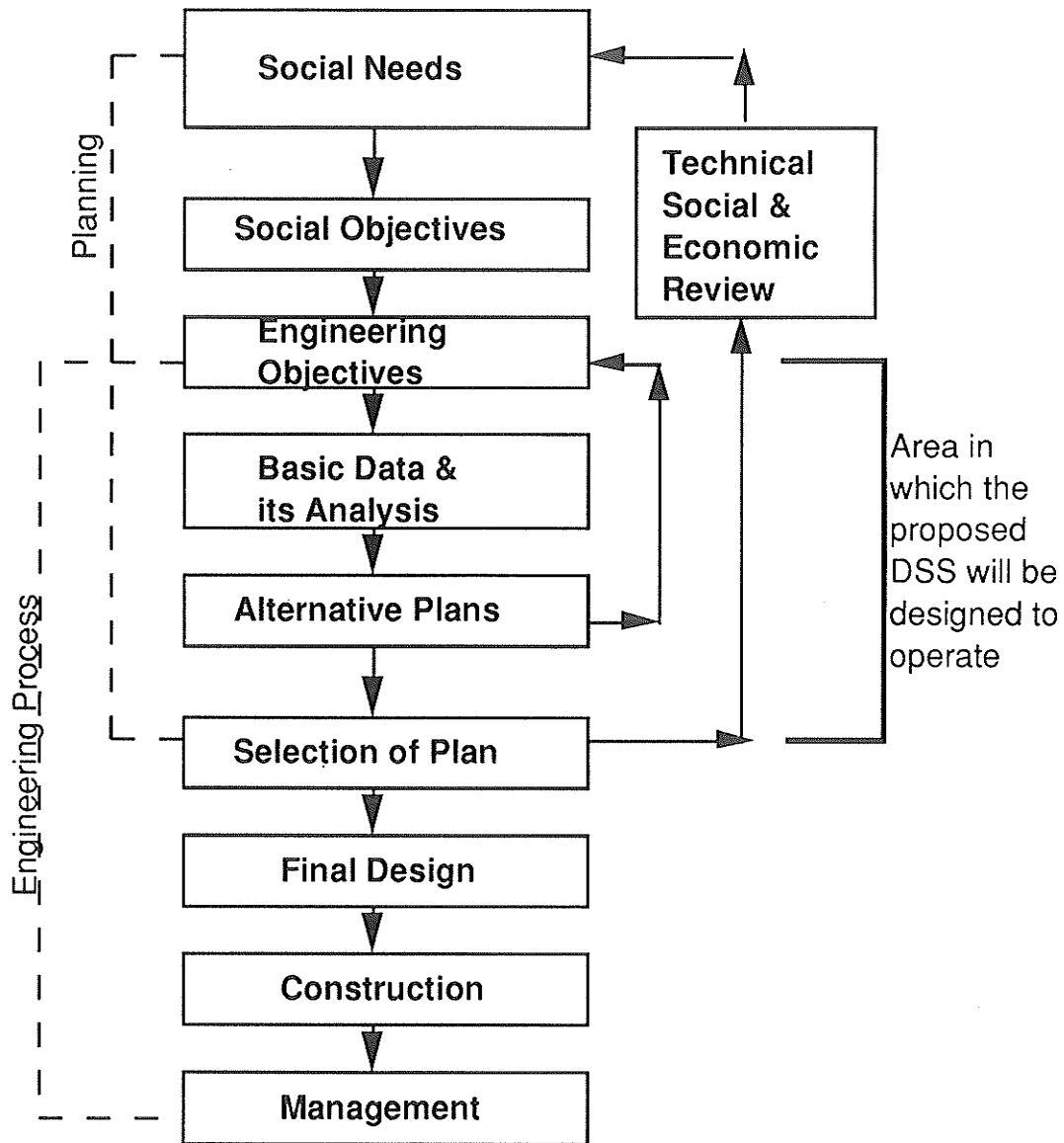


FIGURE 1. THE FLOOD CONTROL PLANNING PROCESS

1.3 SCOPE OF THE WORK.

This investigation focuses on the development of a decision support system which can assist in the generating and evaluation of alternative solutions to flood management problems, and its application to a case study flood control system. The integration of the available technologies such as geographic information systems, expert systems and optimization models into a single DSS is fairly new to the field of water resources, and it is aimed at showing the usefulness and benefits that can be derived from utilizing this approach in the domain of flood management.

Chapter 2 gives a literature review of research related to the topic. A review of recent efforts being made in the field of water resources where decision support systems have been applied to aid in watershed management is carried out. Also, a review of recent applications in the field of geographic information systems which are emerging as an effective technology for application to many flood management problems is presented.

Chapter 3 presents the various aspects and components involved in the development of the decision support system for flood management. This section gives a detailed description of each of the components of the DSS and discusses the inter-communication between each module. Also addressed are the hardware requirements and design structure of the DSS.

Chapter 4 discusses the flood damage analysis procedure and describes how the decision support system developed can be used to assist in the analysis procedure and provide a greater understanding of the problem domain to the user. Chapter 5 deals with the application of the methodology derived to a case study. The chapter deals with the use of the DSS in a flood management situation located upstream of the City of Winnipeg flood control structure, and investigates the usefulness of the DSS in this particular locality.

Chapter 6 is a discussion of the results obtained from the analyses performed in the previous chapter. Chapter 7 presents conclusions and recommendations.

2. LITERATURE REVIEW.

Current and on-going efforts in the field of water resources planning and management to incorporate the available technologies into tools for decision support are reviewed in this chapter. A review of recent applications in the field of geographic information systems as they have been successfully applied to various aspects of water resources policy and planning is also carried out, since these systems form a major component of the system to be developed in this research. The potential of GIS for being incorporated into integrated decision supporting tools is also examined.

2.1 DECISION SUPPORT SYSTEMS IN WATER RESOURCES.

Decision support systems have received much attention in the field of watershed management because of their usefulness in assisting planners and engineers in examining the various issues involved in the water resources planning process, especially their capability for providing support for the generation and evaluation of alternative solutions to such problems. One major challenge in designing such comprehensive modelling systems for policy-making and planning has been to build these models in such a way as to make them easily useable, and to make their output more useful to the prospective users, (Fedra and Loucks, 1985).

Some important and necessary characteristics of DSS have been identified by Simonovic (1990). These are:

- to assist managers in the decision-making process for un-structured and semi-structured problems;
- to support and enhance managerial judgment;
- to improve the effectiveness of the decision-maker;

- to combine the use of models or any analytical techniques with data access functions;
- to emphasize flexibility and adaptability with respect to respect changes in the context of the decision process; and
- to focus on features which make the DSS interactive.

These characteristics also serve as guidelines for potential developers of such systems in to develop complete and user-friendly systems that will provide maximum assistance to the user.

A review of some recent applications of DSS in water resources planning and management as well as a discussion of some of the issues involved in the task are herein presented.

2.1.1 DSS IN PLANNING AND MANAGEMENT.

There are currently several applications of the development of decision support systems in this area. Kunreuther and Miller (1985) developed an interactive micro-analytical modelling system to support policy analysis in dealing with flood hazards. The authors put forward a framework for policy analysis under five headings: 1) Problem Formulation - where the problem is clearly defined so that the policy analyst can structure a set of questions; 2) Interested Parties and Relevant Information - where the views of a set of interested parties are identified; 3) Developing Alternate Scenarios - where different characteristics of homeowners and different flooding situations are generated; 4) Evaluation of Strategies - where the impact of strategies on various stakeholders are examined; and 5) Learning over time - where the system may be altered to incorporate new information and analytical procedures. The central component of the decision support

system is an interactive modelling shell written in Fortran 77 code which is able to interface with several models and guides the user towards generating solutions.

The potential impacts of increased computer power with respect to the development of interactive computer models for water resources planning and policy modelling is discussed by Fedra and Loucks (1985). The authors advocate the combination of various tools under a common organizational framework such as is typified by workstation architecture, with multiple windowing displays for multi-tasking. They also stress a highly modular approach to integrated tool design which must also be hierarchically organized and allow for compatible databases, to ensure smooth transition from one mode to another or from one level of detail to another.

Several reviews have been made on the use of decision support systems in water resource management. Johnson (1986) reviews a number of examples including micro-computer based applications, flash-flood warning and regional water-monitoring systems, water supply and reservoir operating decision support systems, and the use of computer-aided planning (CAP) and expert systems to provide support for decision-making. Continued development in this direction is envisaged by the author, with anticipated increases in microcomputer technologies and decreasing costs of hardware and software equipment.

Johnson (1990) presents an interactive modelling system which aids in the reservoir operating policy modelling process for multi-purpose reservoir operations planning. The computer-aided planning system integrates state-of-the-art simulation and optimization techniques, colour graphics displays and interactive computing interfaces into a coherent system that has user-friendly interfaces to assist the decision-maker in solving domain specific problems. The software developed was embedded in a comprehensive public involvement program to enable concerned parties to learn about the reservoir system's limitations and opportunities in order to create greater participation in the operations planning process.

In an effort to streamline database design for decision support, Armstrong and Densham (1990) outline a methodology for conceptual database design for spatial decision support systems which exploits the features of a data model embedded in relational database management software (RDBMS). They outline a strategy which can be employed to construct functionally integrated spatial databases which can support locational analysis and spatial decision-making in watershed management.

Davis et al. (1991) developed a DSS which estimates the effects of potential land-use and land management policies on water quality and the cost of implementing these policies. The DSS consists of 3 modules: a policy module to generate a suite of policies; a catchment module to estimate the effects of these policies; and a query module to query the estimates obtained from the catchment module. In this particular system, policies, which in some cases may be expressed in general terms, were translated into specific instructions in order to enable computer analysis and operational interpretation. The consultation for the model developed, although utilizing a rule-based approach, did not contain any expertise incorporated into it, but this aspect of development was proposed in future modifications.

Turcotte and Mtundu (1992) describe a computer-based decision support system which determines water discharges through a network of control structures and canals. The system comprises of a relational database that provides structure information to a FORTRAN program using structured query language (SQL) statements embedded in the program. They use a RDBMS to separate structure information from discharge information, which reduces the size of the computational programs and facilitates file maintenance and also makes information on discharge control structures readily available for other initiatives.

The development of decision support systems for watershed management are ever increasing and their utility towards solving both procedural and descriptive problems is being examined in many aspects of water resources.

2.1.2 EXPERT SYSTEMS WITHIN DSS.

The use of expert system technology in the field of water resources planning has been widely documented in several sources. Knowledge-based or expert systems provide a means by which expertise, rules of thumb and engineering judgement can be incorporated into decision support systems to make available a high level of know-how which can be used to address semi- or unstructured parts of water resources problem domains.

A summary of some expert systems currently being developed to provide support for decision-making in water resources engineering is detailed in Simonovic and Savic (1990). The authors also elaborate on a pilot expert system REZES for aiding in reservoir management and operations. The inherent subjective nature of most water resources problem require the use of an approach whereby engineering expertise can be incorporated into the consultation to assist in generating optimal solutions to ill-structured problems.

Savic and Simonovic (1991), develop an interactive reservoir modelling system using the intelligent decision support system approach. An expert systems approach is combined with formal reservoir models, experience in their use, heuristics and rules-of-thumb to produce and "intelligent" DSS. This tool is developed for the purpose of aiding users in selecting and using the best formal model or models for single multi-purpose reservoir analysis.

2.2 USE OF GEOGRAPHIC INFORMATION SYSTEMS.

The analysis and resolution of water resources problems in recent years has been enhanced by the simulation of the effects of proposed solutions on a geographic database using the technology of geographic information systems (GIS). A GIS has been described as " a powerful set of tools for collecting, storing, retrieving at will, transforming, and

displaying spatial data from the real world for a particular set of purposes ", (Burrough, 1987). The application of GIS technology in hydrologic and watershed studies has been demonstrated in many recent studies, (see eg., White, 1989, Muzik, 1988, Silber et al., 1987).

GIS's have been used to perform several tasks under the watershed management domain such as basin and sub-watershed delineation and hydrologic modelling. They have also been used to aid in the visual comprehension of the results of spatial analysis. These successful applications of GIS technology in water resources have led to the investigation of possible integration of this technology into the decision support system framework to enhance the decision-making process. The inclusion of a module capable of transforming and analyzing geographic data brings an effective spatial analyzing component into DSS, and has led to such systems which rely heavily on this aspect being termed spatial decision support systems (SDSS).

Spatial decision support systems in general are designed to focus on limited problem domains, making use of a variety of data types, and they bringing numerical modelling capabilities to bear on the problem and rely on graphical displays to convey visual comprehension to the decision-maker, (Armstrong and Densham, 1990). They have also been defined as computer-based analytical systems for addressing management problems with domains having a spatial dimension, (Buehler and Wright, 1991a).

The information contained in a GIS represents a model of the real world situation and thus, providing the data is accurate, simulations of crisis events can be modelled on a geographic database and the effects of these catastrophes can be visualized and examined. There are several areas where research on utilizing GIS technology to provide decision support is being carried out, and some recent applications are discussed.

2.2.1 WATERSHED MANAGEMENT USING GIS.

GIS have been applied to hydrologic modelling in many recent studies. Muzik (1988) presents an approach whereby a hydrologic model which uses the Soil Conservation Service (SCS) rainfall-runoff procedure interfaces with a GIS to provide information on physical land characteristics for input into the model.

Oslin et al, 1988, outlines a system being developed named STREAMS (Soil, Transport, Rainfall, Erosion and Mapping System) which is designed to facilitate data transfer between computer systems for the purpose of flood plain and watershed management. This system integrates remote sensing and GIS with current hydrology, hydraulic, erosion and sediment transport models to enhance modelling processes in the watershed.

A comparison of runoff volume estimation techniques firstly, by using an SCS model and providing data input manually, and with a method relying solely on GIS, is elaborated on in Stuebe and Johnson, (1988). The authors perform trials on six watersheds of varying nature and results obtained indicate that the use of GIS in this task represents a viable alternative to traditional modelling techniques, and the authors suggest that the GIS method may prove advantageous in large and complex study areas where large amounts of data need to be manipulated.

Hodge et al, (1988), discusses efforts to link a distributed physical process model ARMSED to the geographic information system GRASS. This model has since become part of the GRASS GIS program and obtains input from the user as well as a basin delineation program also incorporated in GRASS named WATERSHED. The WATERSHED program utilizes an elevation map layer and uses it to derive watershed and sub-basin boundaries.

Vieux et al, (1988) describe a method for finite element analysis of hydrologic response areas using GIS. Their method, based on the Green and Ampt equations, utilizes

a Triangular Irregular Network (TIN) generated by the GIS software ARC/INFO to determine the hydrologic response for various nodes in the watershed.

2.2.2 MODEL DATA INPUT USING GIS.

The use of a geographic database to provide input data to hydrologic models has been highlighted in several studies. Cline et al. (1989) use a commercially available computer-aided drafting package, AutoCAD, to input geographic data into a Watershed Information System developed to assist users in the preparation of input files for a hydrologic simulation model HEC-1. Wolfe and Neale (1988) use the GIS GRASS to generate input data for a distributed parameter hydrologic model (FESHM). By using the GIS in data development they cut down on the processing time for this typically time-consuming task. Oloufa et al, 1992, describe a method for extending a GIS to represent boreholes as complex three-dimensional objects. They also elaborate on a method for storing such data in a relational database.

Sasowsky and Gardner (1991) use a grid-cell GIS to parameterize a quasi-physically based surface runoff model named SPUR (Simulation of Production and Utilization of Rangelands), in which a watershed is configured as a set of stream segments and contributing areas. GIS programs were written for the processing of digital elevation data, digital soil maps and also to create tabular files for soil characteristics to facilitate the task.

The growing number of applications of GIS in the water resources planning and management field are an indication of the growing wide acceptance of these models, and the work undertaken in this research project investigates their utility in a decision support system framework.

3. DECISION SUPPORT SYSTEM COMPONENTS.

As a prelude to the development of the DSS, focus needs to be made on several issues pertinent to the proposed system including the most appropriate architectural structure to use as well and the issue of providing a suitable operating system platform and environment in which the DSS will function. These issues, including a description of the various features of the integrated tool developed, are discussed in this chapter.

3.1 ARCHITECTURE OF THE DSS.

Traditionally, the architecture of decision support systems has been classified into three main approaches, (Simonovic, 1990). This classification evolved to give potential designers a conceptual tool for constructing a DSS; to support the evaluation and characterization of possible systems; and to present a practical and constructive definition of a DSS, (Simonovic, 1990). These approaches include the functional approach which is decision process oriented; a tool based architecture; and a third approach, which is a combination of the first two, and utilizes beneficial features from both. This latter approach, known as the combined architecture approach, is modular and adaptive, and is particularly suited for integrating several components of the system which may be accessed randomly.

Several practical applications of this modular approach have been proposed by Johnson (1990) and Arnold and Sammons (1988). An adaptation of the modular approach was derived for the development of the decision support system. This design was selected in order to facilitate communication between the various components of the system and also to be able to incorporate the respective technologies into one tool for

addressing different parts of the flood management problem. This design is illustrated in Figure 2.

In general, a DSS is made up of 3 major components, the system manager, database module and the modelbase module. The system manager which is centrally located, is the component which integrates the other parts of the system and also controls all the processes in the system. The database component is the module that handles data storage manipulation and extraction from the system. It also provides facilities for updating and modifying data used by the system. The modelbase component of the system is the part which contains the different process models pertinent to the problem domain. This module provides the facilities for integration between models and also provides the facilities for linking these models with the database. The inclusion of a display and graphics subsystem into the DSS enhances the input of data into the models, provides an improved user interface for the user, and aids in the visual comprehension of spatial information used by the model. A more detailed description of each subsystem is discussed in sections 3.3 to 3.7.

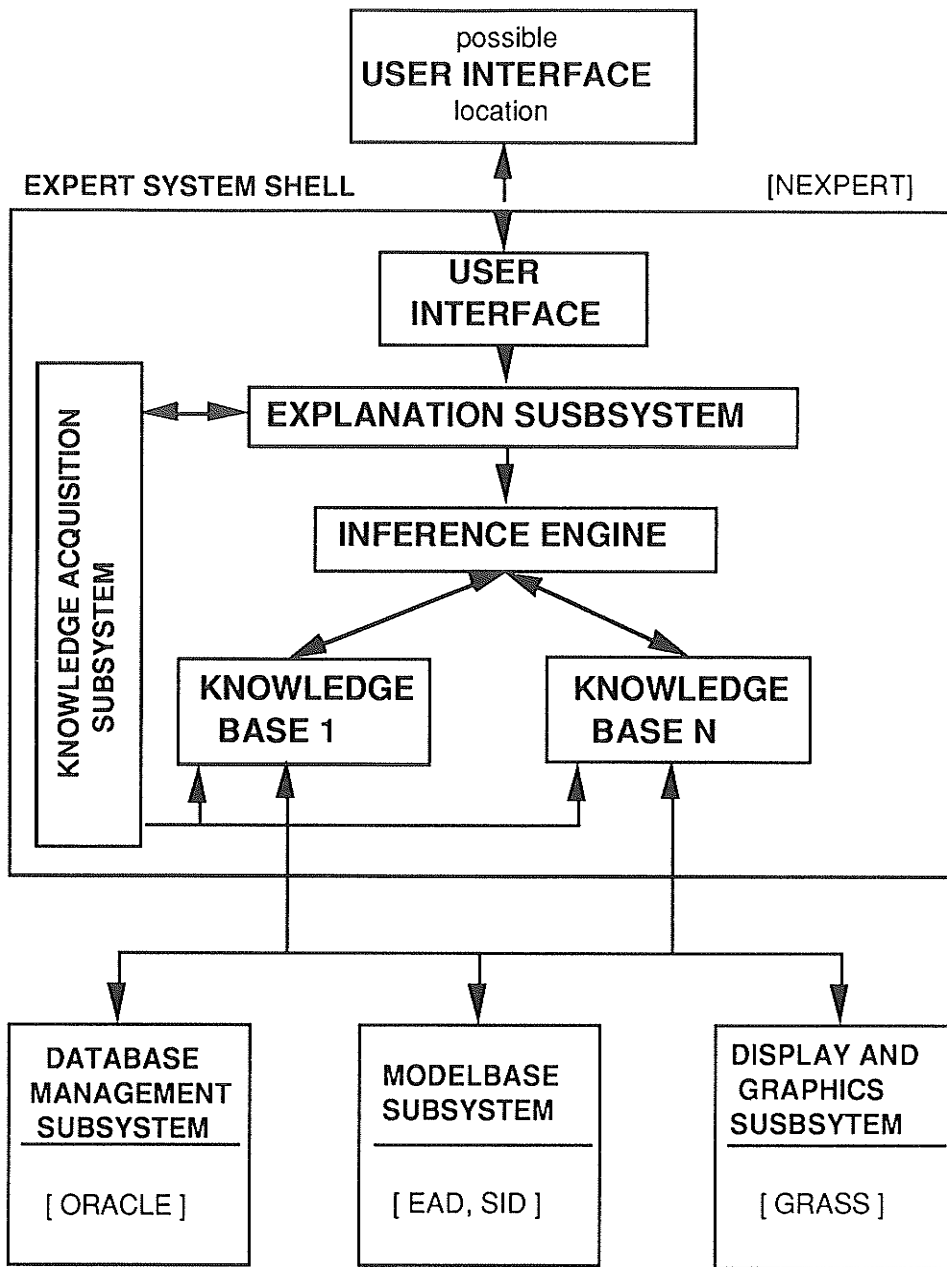


FIGURE 2. PROPOSED ARCHITECTURAL DESIGN OF DSS UTILIZING A MODULAR APPROACH.

3.2. DSS OPERATING PLATFORM.

With cheaper and more computer power becoming available to potential developers of integrated systems the task of model development is facilitated by quicker data access and quicker inter-communication between different module components running on the same platform. This situation also enhances the creation of interfaces engineered to support traditional planning and decision-making procedures, which will in turn lead to greater comprehension and a greater acceptance of models developed. In the development of decision support systems it is important to select an operating platform which provides the capability of communication between each module of the system and also allows for easy linkage between these components. A workstation platform provides these capabilities as well as providing the environment for the performance of multiple tasking.

A Sun Microsystems Sparc 1+ workstation with a 340MB hard disk and 28MB of RAM memory was selected as the platform for development of the DSS. This computer is also connected to a 150MB cartridge tape drive and an Epson LX-810 line printer for data entry and printing output respectively.

There are several benefits to be derived from developing decision support systems on a workstation platform. Firstly, the computing power that is a general characteristic of these platforms enables fast and efficient systems to be developed. They also enable multi-tasking to be performed with ease and several applications may be run simultaneously. Also, the multiple windowing display programs often coupled with these applications, allow several screens to be displayed at once, thus the operator can interact with different components of the model to the detail required. This also aids in comprehension of model output both analytically and visually (in this particular case, the OpenWindows windowing system is used). Workstation display screens can, in general display a larger work area than personal computers due to their larger screens. For these reasons the workstation platform was selected as the most suitable one for DSS development.

3.3 THE DSS SHELL/ SYSTEM MANAGER.

The central feature of a DSS is the system manager which controls the various parts of the system. This centrally located component (or shell) co-ordinates the individual tasks carried out by the respective parts of the system and is directly linked to the user interface of the system which is the link between the user and the system. The tasks that must be performed by the system manager are to control purposes and integrate other parts of the system so it must be centrally located, (Simonovic, 1990).

There are several issues to be considered in selecting or designing this component including the type of communication required between each module, the speed of communication and the time-frame of development. The shell used in the DSS development is discussed below.

3.3.1 NEXPERT OBJECT.

The module selected in this research to control the various parts of the system is a knowledge-based expert system shell named NEXPERT OBJECT, herein referred to as NEXPERT. This shell was chosen for its ability to be readily integrated, on the Sun workstation, with the other components of the system such as a relational database management system and the GIS, which run on the same platform.

Selecting a shell which can communicate with other software that is to be integrated into the system also has the advantage of cutting down on the time taken to develop a prototype for trials by the developer and by prospective clients. Using an already manufactured shell frees the developer from the tedious task of writing masses of computer code to link each module to the rest.

NEXPERT contains a graphical user interface that is the link between the user and the system. It is also directly linked to the explanation subsystem of the ES which has the capability of providing the user with help screens. This explanation subsystem can also be

customized by the developer to provide query-specific help instructions which provide help related to the specific task being performed. It is also possible with this particular shell to link to a more comprehensive or more graphical interface which is tailored to a particular institution's needs.

The inference engine of the ES shell is the actual component which determines the search strategy and order that is utilized to develop the required knowledge. This engine triggers in turn, the knowledge bases that need to be fired and in the correct order. Both forward chaining and backward chaining search strategies are available in the shell.

Several knowledge bases may be contained in the system. Each of these knowledge bases has access directly to the other modules of the DSS, e.g, the database management subsystem, the modelbase subsystem and the display/graphics subsystem, as shown in Figure 2. NEXPERT incorporates an applications development environment which facilitates the process of entering rules to the knowledge base. Rules may be entered through a rule editor (see Figure 3.) in the standard IF, THEN format.

3.4 MODELBASE COMPONENT.

The modelbase subsystem of the DSS contains analytical models which are accessed by the knowledge bases to perform procedural and analytical tasks. For this particular problem domain, i.e. flood management, this module is comprised of software for carrying out a structure inventory of damage (SID), computing the estimated annual damage or flood damage from a particular flood event (EAD), and also the geographic information system (GRASS). These programs are discussed below.

3.4.1 GRASS .

The Geographic Resource Analysis Support System, (GRASS), GIS, was developed by the US Army Corps of Engineers and is a public domain geographic

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Figure 3. Rule editor in NEXPERT

information system. It is an integrated set of programs designed to provide digitizing, image processing, map production and geographical information system capabilities to users. GRASS provides many routines which assist in analyzing watersheds and also provides capabilities to display geographic data on screen which can assist the user in the visual comprehension of queries performed.

3.4.2 SID.

The Structure Inventory of Damage (SID) analysis program is part of the Flood Damage Analysis Package developed by the US Army Corps of Engineers. It is designed to assist in the systematic and expeditious collection, management, and processing of data related to structures subject to flooding. Its prime function is to generate elevation-damage functions by damage categories and reaches. SID can also perform an analysis of some non-structural flood control measures and generate a modified elevation-damage curve based on user input specified. Non-structural measures which SID is capable of analyzing are Flood proofing, structure relocation and raise- to- target - elevation analysis.

3.4.3 EAD.

The Expected Annual Damage (EAD) analysis program was developed to assist in economic evaluation of flood plain management plans, US Army Corps of Engineers (1989). The program computes inundation reduction benefits. Damage may be computed in three modes:

- Damage for a specific event;
- Expected annual damage for a specific year or years; and
- Equivalent annual flood damage given a particular discount rate and period of analysis.

In calculating damage for a specific event several damage categories such as urban, agricultural and residential may be analyzed at the same time and these are totalled for each

plan and each reach selected. Expected annual damage may also be computed for conditions existing in the past or expected in the future. Equivalent annual damage can be computed when a discount rate and a period of analysis is specified. EAD also has the capability to analyze several structural flood control measures.

3.5 DATABASE SUBSYSTEM.

The database subsystem is the part of the system which facilitates data storage and manipulation. It is important, in the development of large applications programs which utilize large amounts of data and have several programs communicating with each other, to have a module which has the capability of providing efficient data storage, handling and manipulation services to each program and the system as a whole. A relational database manager named ORACLE was selected for the task and some of its features are discussed below.

3.5.1 ORACLE.

The database management system contains a relational database management system, ORACLE, which can be used for making queries of the domain specific information as well as being used for intermediary or final report generation. NEXPERT is fully integrated with ORACLE through a database bridge whereby instructions made through the "actions" block of the knowledge base rules in Structured Query Language (SQL) are readily interpreted by ORACLE and the required information is generated. Data from other components of the system can be loaded into ORACLE and manipulated by SQL commands and can be output in the required format for use by pertinent models.

3.6 DISPLAY/ GRAPHICS SUBSYSTEM

One of the major roles of the display/graphics subsystem is to improve the comprehension of the spatial and time-dependent information utilized by the system by providing visual diagrams of the results of analyses performed. This feature aids the decision-maker in comprehending the results of various alternatives thus leading to a more optimal choice of measure.

The user interface developed for the system to be designed plays a key role in the effective interpretation of commands from the user and results from the system. In this particular case, NEXPERT, which is to control the consultation session, contains a built-in user interface called the session controller which provides an adequate user-machine communication interface for most general purposes. NEXPERT, however, has the capability of enabling a more graphical user-interface to be built on top of the application and this interface may be customized to a particular firm's or agency's needs.

3.7 EXPERT SYSTEM COMPONENT.

The use of an expert system shell as the central part of the system provides an easy way whereby heuristics and rules-of-thumb can be incorporated into the consultation in areas where engineering expertise may benefit the user. Any rule or hypothesis in the knowledge base can be expanded to include subjectivity and heuristics into the consultation by specifying the knowledge base in the required rule.

The use of NEXPERT as the system manager also allows the DSS to take advantage of many of the features that are characteristic of such expert system shells and use these to an advantage. One such feature is the consultation trace option normally found

in most ES shells. This allows the user to monitor the reasoning which led to the arrival of a particular conclusion or solution.

Expert systems provide a way in which a high level of engineering expertise can be provided in a limited domain to the user of the system in order to assist him in providing solutions to the specific task on hand. They can also be used to enrich the experience of the user towards the particular task, thus enabling him to make more informed decisions to ill-structured problems. Such knowledge bases containing heuristics and rules-of-thumb may be accessed by the user as required.

4. DECISION SUPPORT SYSTEM OPERATION.

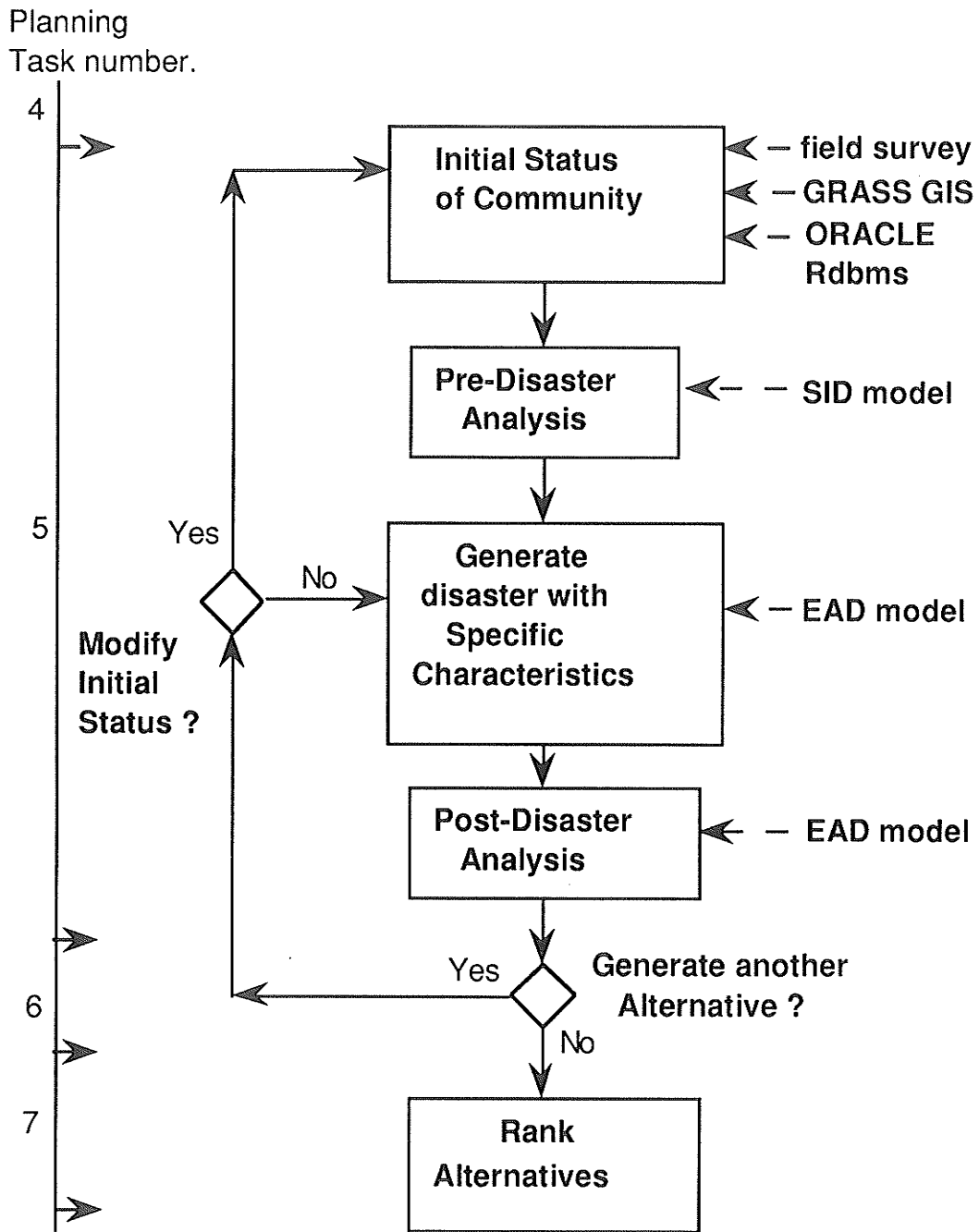
4.1 FLOOD DAMAGE ANALYSIS PROCEDURE.

The DSS provides support for carrying out the flood damage analysis procedure as shown in Figure 4. The first part of the procedure comprises the survey of all information related to the flood plain, including locational and structural data. This data is then transferred into the SID program which performs a structure inventory of damage and outputs the aggregated elevation-damage curves for each reach. This data is then transferred to a data storage file for use by the EAD program which computes the flood damage or expected annual damage based on specified flooding parameters. Other consequences of each flood such as the total area flooded and also the cost of implementing

flood proofing measures is computed and made available for alternative comparison. The detailed procedure for the analysis is elaborated on below.

4.2 GENERATING INITIAL COMMUNITY STATUS.

The process of generating the initial status of the communities in the study area is discussed under three main headings; conducting a field survey of the region, geographic data input using the GIS and updating the relational database.



- 4 - Eng. Objectives
- 5 - Basic Data & Analysis
- 6 - Alternative Plans
- 7 - Selection of Plan

FIGURE 4. DIAGRAM OF THE FLOOD DAMAGE ANALYSIS PROCEDURE

4.2.1 FIELD SURVEY

A field survey is normally carried out to obtain detailed information on the characteristics of the study area if detailed information on the basin is not available. Information such as the type, cost and ownership of buildings in the region must be obtained to be able to accurately represent the amount of damages that will be incurred by each homeowner as well as the region as a whole. However, where adequate data on these characteristics have already been documented, or where certain characteristics such as house prices do not vary much within the basin, average values may be used throughout the basin for preliminary analysis purposes. A detailed field survey should however be made before any major flood control plan is implemented. Data from this process is entered into the study area database as will be described in the following sections.

4.2.2 GEOGRAPHIC DATA INPUT

A major aspect in the use of any simulation model is the task of acquiring the necessary data for its effective use. As well, this data usually has to be formatted specifically (pre-processed) before it can be used in the model. Advances in the field of remote sensing technology have, over the years, made geographic data more readily available as input to geographic information systems and hydrologic models, and these procedures have been documented in several studies, as detailed in Chapter 2. Geographical features such as land-use, land cover and elevation data can be extracted from areal photos or satellite pictures more easily than before, and this has led to such information being cheaper and easier to obtain. Such data often may be obtained from provincial or federal departments, or it may be input from ordinary paper maps by the use of a scanner or a digitizer. Data which is input by the user by scanning or digitizing normally has to be checked for accuracy and errors due to equipment.

Data obtained from provincial or federal agencies may consist of several map layers, each containing features which contribute towards the complete description of the

study area. A typical cross-section of map layers which make up a study area are as listed below:

Layer A	Designated Area	e.g., golf courses, airstrips;
Layer B	Building	e.g., fire stations, houses, museums;
Layer C	Structure	e.g., smoke stacks, storage tanks;
Layer D	Roadway/Railway	e.g., paved roads, bridges, rail lines;
Layer E	Utility	e.g., electrical poles, water towers;
Layer G	Hydrography	e.g., bogs, ditches, dykes, marshes, ponds;
Layer H	Hypsography	e.g., contours, water levels;
Layer J	Land Cover	e.g., orchards, trees;
Layer K	Textual	e.g., road names, cities, towns, villages.

Table 1. Typical map layers contained in a geographical map.

GRASS facilitates the task of data input and management by providing the routines for analyzing and extracting data from these map layers to assist in generating a complete inventory of the flood plain, i.e., assisting in the field survey process. Data such as topographical data and structural data are input into the GIS and manipulated to produce output files, which can in turn be loaded into the relational database manager, ORACLE. This is part of the process of building up the community inventory database.

4.2.3 UPDATING THE RELATIONAL DATABASE

The relational database contains fields which represent the parameters which the structure inventory analysis model (SID) requires for the program to run effectively. This comprises data such as the location of each building in the flood plain, the owner, the cost of structure the damage category of each structure, etc. Appendix A-1. details the list of

fields contained in the database and what they represent. Appendix A-2. also lists the SQL commands used to create these fields in the database. Data from GRASS provides input for the fields ROWN, COLE, IBDLG, ADJ and IDRCH. The information on the location, reach and structure identification number are obtained from GRASS by running the {sites} program in GRASS. This program performs a site occurrence report based on 1 or more map layers, and writes these statistics to a data file. The data output produced by this program can be read and re-formatted by a Fortran computer program and then loaded into the database fields in ORACLE by using the SQL command SQLLOAD, (Appendix A-3).

This information, inputted from GRASS, then serves as the basis for entering the information required for the other fields. This can easily be done using SQL commands. For example, the SQL command

```
UPDATE Adolphe  
SET V1FS = 50000  
WHERE IBDLG = 365;
```

performs the task of assigning a value of \$50,000 to building number 365,(IBDLG=365).

Thus the existing conditions in the flood plain can be efficiently documented by using the information from the GIS and field survey. The completely updated database can be output to a file using the SQL command SQLREPORT (Appendix A-4), making such information available for use by SID.

4.3 PRE-DISASTER ANALYSIS.

An important task of the DSS is in providing input for the two damage models to be used in the flood damage analysis, namely SID and EAD. NEXPERT, as the system manager, assists in the input of data into these models by providing a sequential consultation designed to maintain the focus of the user on a particular task till each sub-task is completed. This is important because the manner in which records are listed in these models' input files, which corresponds to the manner in which records are read, does not cater to the focusing on one specific task from start to end. This also prevents the user from omitting necessary data needed to run the model based on the criteria he specifies, and thus save costly time which may be spent in debugging the input data.

Such a hierarchical procedure also improves the comprehension of the user towards the analysis procedure as a whole and can thus help in the selection of different alternatives to examine. It also leads to a greater acceptance of the DSS since the analysis procedure can more easily blend into the decision-making process. This interactive process is described below.

4.3.1 INTERACTIVE MODELLING

The rules stored in the expert system's knowledge base govern the order in which each question is put to the user. These rules are listed in Appendix B-1. A backward-chaining inference control strategy was used to provide an efficient consultation, since the number of possible outcomes was not large. A diagram illustrating the backward-chaining layout is shown in Figure 5.

For the SID consultation, the user is first prompted by the Session controller in NEXPERT for a title for the particular run, (as shown in Figure 6), which will be used on all output for the program. After this, the user is then prompted to specify whether any non-structural flood control measures will be applied to structures in the flood plain, and if

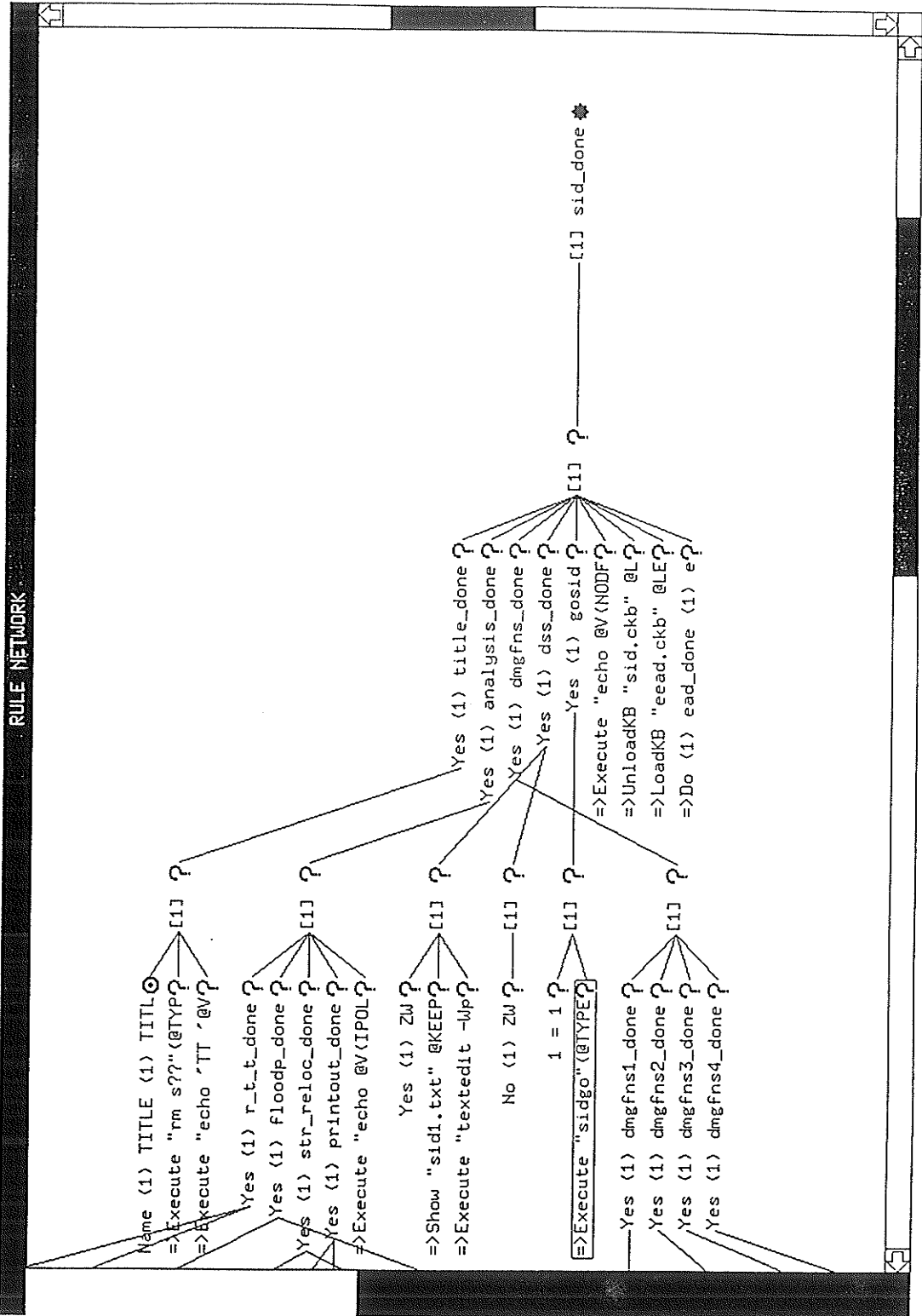


Figure 5. Schematic of the backward-chaining process

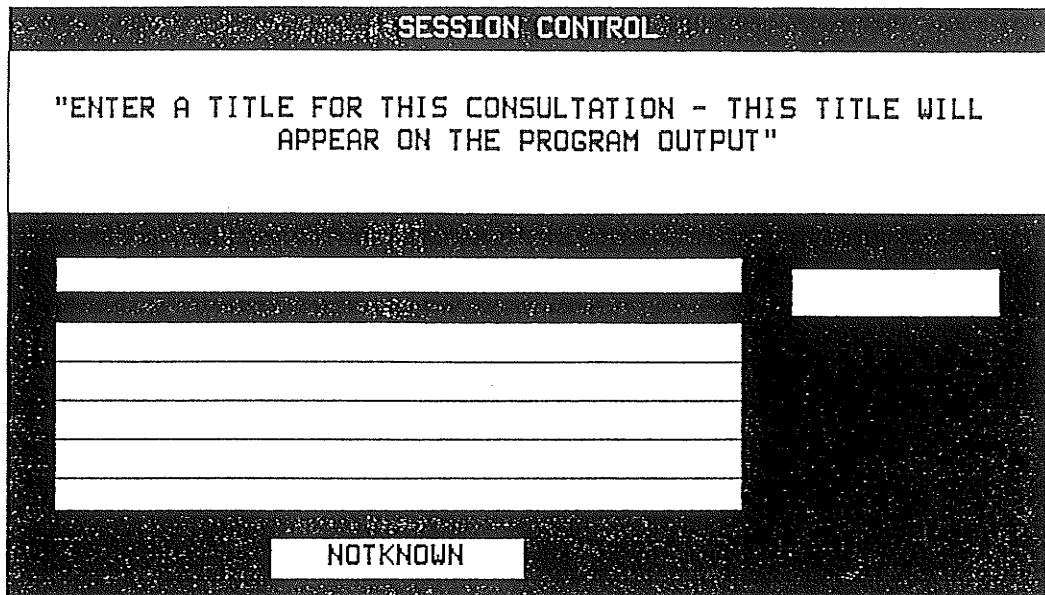


Figure 6. Session Control window in NEXPERT

so the type of measure to be applied. Three options are provided in the model namely, raise-to-target-elevation analysis, flood-proofing analysis and relocation of structures analysis, to be used for the analysis. For each measure selected, the inference mechanism determines the rules which need to be selected in order to prompt the user for information which must be provided for the proper implementation of the measure.

The system then prompts the user for information related to the flood plain such as the number of damage categories, the number of damage reaches and the different damage

functions that may be applied to a particular category. The damage function for a particular structure or category of structures represents the manner in which the elevation-damage relationship is defined for that particular category or structure. The damage function may be represented as an elevation - percent-damage relationship (i.e. if the flood level is 1ft above the first floor level then 20% of the structure value can be said to be lost, and so on), or it may be represented as an elevation - direct-damage relationship (where the different flood levels correspond to a certain amount of damage). The user, upon specification of a damage category is prompted for a name of a damage function and also whether the damage function values to be input are elevation - percent-damage values or elevation - direct-damage values, and then NEXPERT prompts for these values to be input. The session continues until all values needed for the model to run are input.

All the values obtained from this hierarchically oriented consultation process are written to data files whose filenames correspond to the respective record names of the program for efficient program documentation (i.e., all input data for record 'J1' are written to a file named 'sJ1', 'J2' records to 'sJ2', etc) . After all the necessary values are obtained, Fortran programs, (listed in Appendix C), read the respective files and combine these results with the output obtained from the ORACLE session to produce an input data file for use by the SID model. Thus the user can generate several different scenarios using NEXPERT and obtain the elevation-damage relationships for them.

The user has the option, after running the SID program, to specify that the output be written to a data storage utility named HECDSS, where it may be accessed subsequently by the EAD program.

4.4 GENERATING FLOOD MANAGEMENT ALTERNATIVES

The selection of the type of structural or non-structural flood control measures to use in a given situation depends on several factors such as the physical and economic feasibility of the proposed measure, the stage of the expected flood, the amount of flood warning time that may be given, and the velocity and duration of the expected flood. For the most part, flood control measures classified as structural are normally implemented over a regional scale such as reservoirs, dyke and dams, whilst non-structural measures are generally implemented to individual or small groups of structures.

The optimal choice of implementation of structural or non-structural measures or a combination of both must be based both on the physical parameters outlined above and also on engineering expertise in the area of flood management. Expertise is required for several reasons. For example, incentives may be provided to householders in the flood plain to implement certain types of flood control measures for their own safety, but regardless of the risk, they may for one reason or another refuse to implement these measures. They may also be reluctant to provide funds in the form of levies or taxes for large scale structural flood control measures if the anticipated floods have not materialized in recent times, even though severe flooding is likely to occur in the region. Attractive flood insurance rates may also not be taken advantage of due to a false sense of security by these residents.

This human factor as well as the experience of engineers in applying the available measures in other relevant flooding situations needs to be taken into account when selecting flood control measures for a particular area, and one way in which this information can be collated and provided to the user of the DSS to access and make an informed decision is through the use of expert systems.

Although an expert system which incorporates this necessary knowledge is currently not integrated into the system, it is planned to be added in future research work to be implemented on the system.

4.5 POST-DISASTER ANALYSIS

Subsequent to the generation of the elevation-damage relationships produced by the SID model, the system loads up the knowledge base containing the consultation for the damage model, EAD. Likewise, NEXPERT generates a systematic hierarchical consultation for the input of the required data needed to run the model. A description of the consultation is given below.

4.5.1 INTERACTIVE MODELLING

The user is first prompted to enter a title for the consultation which will be used on all program output. Then the user is asked whether a period of analysis consultation is to be performed and if this is true the necessary data needed is prompted for. This data includes the length of the period of analysis, the year representing existing conditions, the year in which the plan becomes operational, and other relevant data. The user may also specify an affluence factor which represents the change in the value of a structure or its contents over the period of analysis.

The user is then asked to specify the number of different plans to be evaluated in this particular computer run. This is the number of different flooding scenarios to be used in this particular consultation. Upon specifying the number, the user is asked how the flood data for this run will be input. Data may be input in three different formats, exceedance-frequency values, flow values or stage values. Each format may require

additional data to be provided and NEXPERT prompts the user to provide additional information as shown below:

SELECTION	REQUIRED DATA	ADDITIONAL DATA
Exceedance-frequency values	----> flow-frequency values	----> stage- flow values
	----> stage-frequency values	-
Flow values	----> stage-flow values	-
Stage values	-	-

All the above options also require the input of information on the elevation-damage relationships existing in each reach. This data may be input manually or may be retrieved directly from the HECDSS data storage file created by the SID program by specifying the alternative name and pathname of the data.

All the data received from the consultation are written to data files and upon completion of the input process a Fortran program reads these files and formats the data into an input file which is read by EAD. The rules for the consultation are listed in Appendix B-2. The EAD program is then run and the values of damage or expected annual damage can be obtained.

4.5.2 FLOODING CONSEQUENCES

There are several indicators that may be computed in order to determine the consequences of a particular flooding event or a series of flooding events. These indicators provide some of the necessary information which can be utilized to rank the set of

alternative flood control plans generated. A number of indicators may be generated from the consultation process developed, and these are discussed below.

Expected Annual Damage

The expected annual damage is a frequency weighted sum of damage for a range of possible damaging flood events, and can be visualized as what might be expected to occur in the present or any future year. By using the EAD program, the expected annual damage is determined by computing a damage-frequency matrix from input data and then weighting each damage value according to its percent chance of exceedance.

Specific Event Flood Damage

Damage may be computed for a specific event, such as a historical flood event or a future anticipated event, by selecting this option in the EAD program consultation and entering in the required value.

Area Flooded by a Specific Event

The area flooded by a specific flood event may be computed by using the GRASS program. The elevation corresponding to the particular event is input to NEXPERT and the flooded area corresponding to this stage is displayed on the elevation map. The GRASS program {report} is then accessed to generate a report on the total area taken up by the displayed flooded area, and this is then multiplied by actual area of each cell to arrive at the actual flooded area.

Individual Structure Damage

Individual structure damage may be determined by first comparing the flood stage for the particular event to the ground elevation of the building as listed in column ADJ of the structure inventory database. If flooding is found to have occurred, by the ground

elevation being lower than the flood stage, then a multiplication of the damage function for the particular structure and the cost of the structure will yield the damage done to it.

5. CASE STUDY - GREATER WINNIPEG AREA FLOOD MANAGEMENT.

5.1 INTRODUCTION

The city of Winnipeg in Manitoba, Canada, and areas along the banks of the Red River upstream of the city, (see Figure 7.), have a history of flooding which dates back several decades. These floods have caused much damage and destruction, the most notable in recent decades being the Red River flood of 1950. In the years subsequent to this event several flood control measures were put in place, aimed at providing flood protection for the residents of the city of Winnipeg. A primary dyking system was constructed soon after the 1950 flood to protect some of the low-lying areas along the Red, Assiniboine and Seine rivers throughout the city. The Red River floodway was completed in 1968; the Portage diversion in 1970; and the Shellmouth Reservoir in 1972. The operation of this flood control system maintains upstream water levels to their natural levels, and thus does not reduce the flood hazard of areas upstream of the Red River floodway. During the most recent instances of high water levels on the Red River, i.e., 1974 and 1979, residents upstream of the floodway incurred heavy damages with some buildings being washed away and several residents having to be evacuated from the area.

The area chosen for this study, highlighted in Figure 7 and detailed in Figure 8, represents an area of 10 x 13 sq km. just upstream of the inlet control structure and Red River floodway which provide flood protection for the City of Winnipeg. The main community in the region is St Adolphe, Manitoba. The main occupation of dwellers in the area is farming. The average cost of buildings in the township is \$80,000 and in surrounding areas the average cost is \$50,000. A dyke known as the West dyke which is part of the flood control works for the city of Winnipeg, runs from north to south through

CANADA



Figure 7. City of Winnipeg and surrounding areas

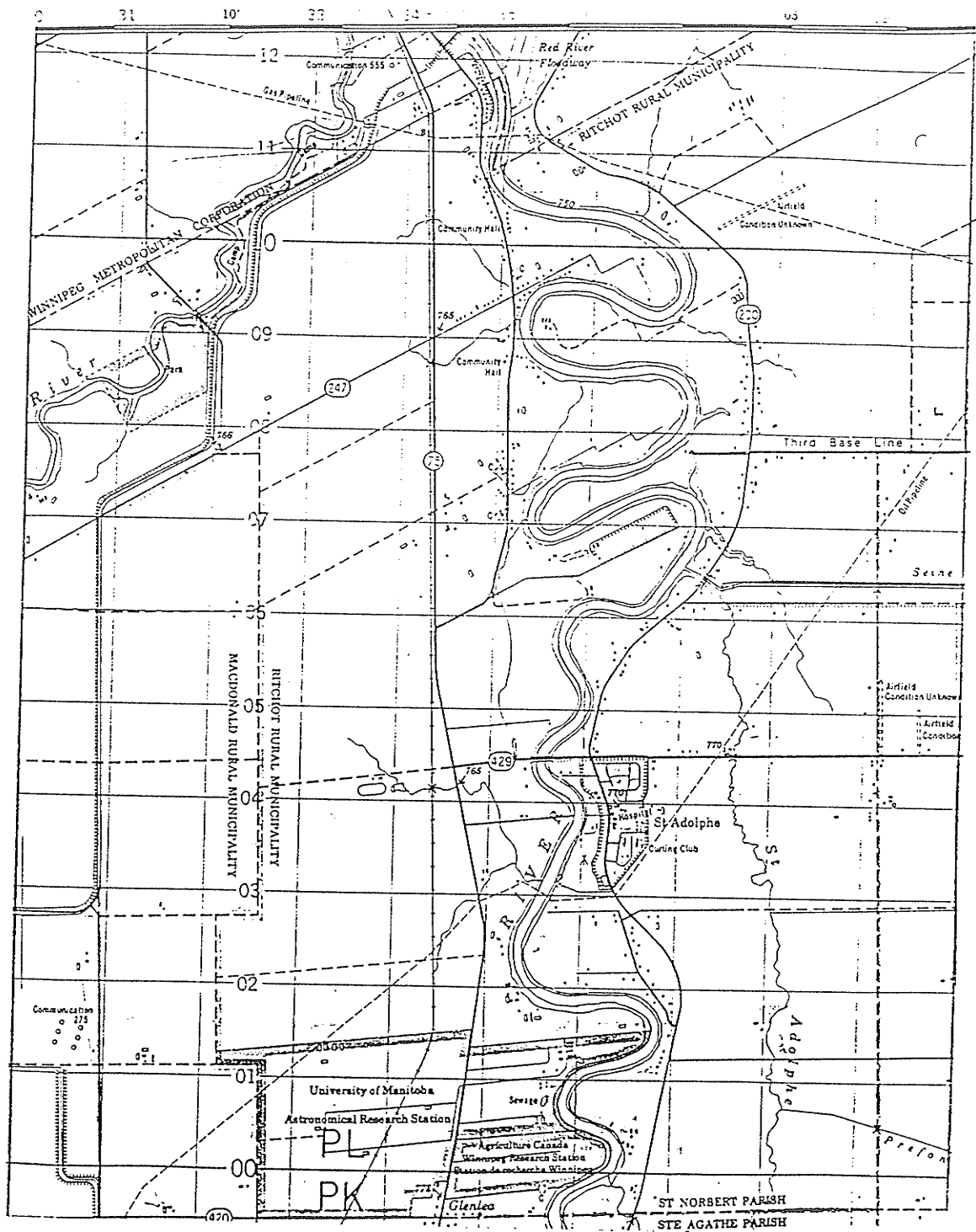


Figure 8. Diagram of the study area

the western part of the study area. Buildings located west of this dyke are protected to a height of 787.4 ft above sea level, which is the elevation of the dyke.

Apart from a few ring dykes around some of the buildings in the region, the area is vulnerable to floods which in general have a small return period. It is intended to use the DSS to generate and evaluate suitable flood control measures for the area and recommend measures which can be taken to protect the communities in the region .

5.2 DATA ACQUISITION, FORMATTING AND INPUT.

Data for the study area was obtained from several agencies including the Water Resource and Remote Sensing Branches of the Manitoba Department of Natural Resources. Pre-processing of data for model input is discussed under the headings geographic data, hydrologic data and database input.

Geographic Data

In Winnipeg, the Remote Sensing division of the Manitoba Department of Natural Resources is the agency that distributes geographic data. These data comes in files covering a typical 1:20000 map area and each file consists of several map layers. Pre-processing was done after obtaining the data files from the agency. The data was obtained in the DLG format, which was close to an acceptable format used in the GRASS GIS software. The GRASS program import.to.vect was used to translate these files into GRASS digit format which is the format used by GRASS to perform analyses. Vector data files that made up the study area were joined together by running the GRASS program Vpatch. The two main map layers to be used in the analysis i.e., the *elevation* map layer and the *buildings* map layer, were pre-processed as follows.

To prepare the *elevation* map layer, the GRASS program digit was run and lines and areas that were not assigned contour values were given values by clicking on them with the mouse and assigning them. These vector files were then converted to raster format using the vect.to.cell program in GRASS. In order to generate a continuous surface from the contour layers the program Gsurface was run. This program fills grid-cell values with interpolated values, using numerical approximation techniques. The resultant map was edited after this program was run to ensure that important features on the map such as the West Dyke had the correct elevations. This was done by running the digit program to digitize the corrections on a new map and then by combining the old map and the corrections map using the combine program. This procedure resulted in obtaining a corrected and authentic *elevation* map layer.

The elevation map for the study area, generated from the above procedure, contained elevations that ranged from 705.4 ft at the surface of the Red river to 820.2 ft at the top of the Inlet Control structure. The contour intervals obtained after running the interpolation program {Gsurface} was 3.3 ft. A diagram of this is shown in Figure 9. Thirty-four intermediate values were generated.

With respect to processing the *buildings* map layer, the GRASS program {digit} was also run. In order to be able to determine the elevation at a particular structure or building a single point was marked for every building on a new cell map. By overlaying this new map on the elevation map the elevation corresponding to these points is determined, and this is taken to be the ground elevation for each respective building. These reference elevations are used in the subsequent analyses. The {sites} program was used to perform analyses on the *buildings* map layer and the *elevation* map layer to generate information on the coordinates of each building in the flood plain as well as the ground elevation at each location. Each building was given a unique identification number in the process. The information i.e. North coordinate position, East coordinate position,

identification number and ground elevation, provide the necessary data to fill the ROWN, COLE, SITENO and ADJ columns respectively in the database.

Hydrologic Data

Data for the annual flood peaks (see Table 3) and the stage-discharge relationship (see Table 4 and Figure 12) at the inlet control structure were obtained from the Water Resources Branch of the Manitoba Department of Natural Resources. The average cost of buildings in built up areas was \$80,000 and elsewhere \$50,000. The majority of buildings in the township were classified as two-storey no-basement (2SNB) buildings and the average classification elsewhere was single-storey no-basement (1SNB) buildings, and these values were used as approximate values throughout the study area. The elevation - percent-damage function relationships were obtained from U.S. Federal Insurance Agency (1970) curves for similar building categories. The discharge - probability-exceedance frequency curve was generated for the flow values obtained in Figure 13. Buildings east of the West Dyke were assigned to category 1 and buildings west of the West Dyke were classified as being in category 2.

Database Input

Data from the GRASS program is input into the database by the commands given in Appendix A-3. These values are used as the basis for updating the remaining columns in the database. The commands used to update the database which are based on information pertinent to the study area are as listed in Appendix A-5. The resultant updated database is as listed in Appendix F.

YEAR	FLOW (cfs)	YEAR	FLOW (cfs)	YEAR	FLOW (cfs)
1913	45100	1935	15000	1957	23100
1914	15600	1936	37700	1958	18500
1915	11500	1937	7750	1959	35000
1916	71200	1938	15400	1960	68700
1917	39700	1939	12600	1961	17000
1918	14300	1940	17600	1962	59600
1919	23500	1941	41800	1963	23300
1920	22200	1942	45600	1964	35400
1921	58700	1943	42200	1965	64200
1922	23100	1944	17400	1966	88200
1923	42000	1945	52500	1967	61000
1924	13400	1946	38100	1968	18000
1925	51400	1947	38100	1969	75800
1926	32200	1948	36700	1970	80100
1927	36800	1949	69000	1971	58900
1928	24300	1950	48100	1972	57600
1929	37500	1951	103600	1973	18900
1930	38700	1952	37600	1974	96500
1931	24300	1953	12600	1975	61900
1932	37500	1954	18500	1976	64800
1933	38700	1955	53700	1977	6600
1934	15600	1956	68800	1978	67000

Table 2. Annual Flood Peaks

STAGE	FLOW (cfs)	STAGE	FLOW (cfs)	STAGE	FLOW (cfs)
708*	13000	749	54000	759	94000
712*	15000	750	57000	760	100000
716*	17000	751	60000	761	106000
720*	19000	752	64000	762	115000
724*	21000	753	68000	763	126000
728*	24000	754	72000	764	140000
732*	26000	755	75000	765	160000
736*	30000	756	80000	766	180000
740*	35000	757	84000	767	205000
744*	41000	758	88000	768	230000
748	50000				

* - estimated values

Table 3. Stage-discharge values for St. Adolphe

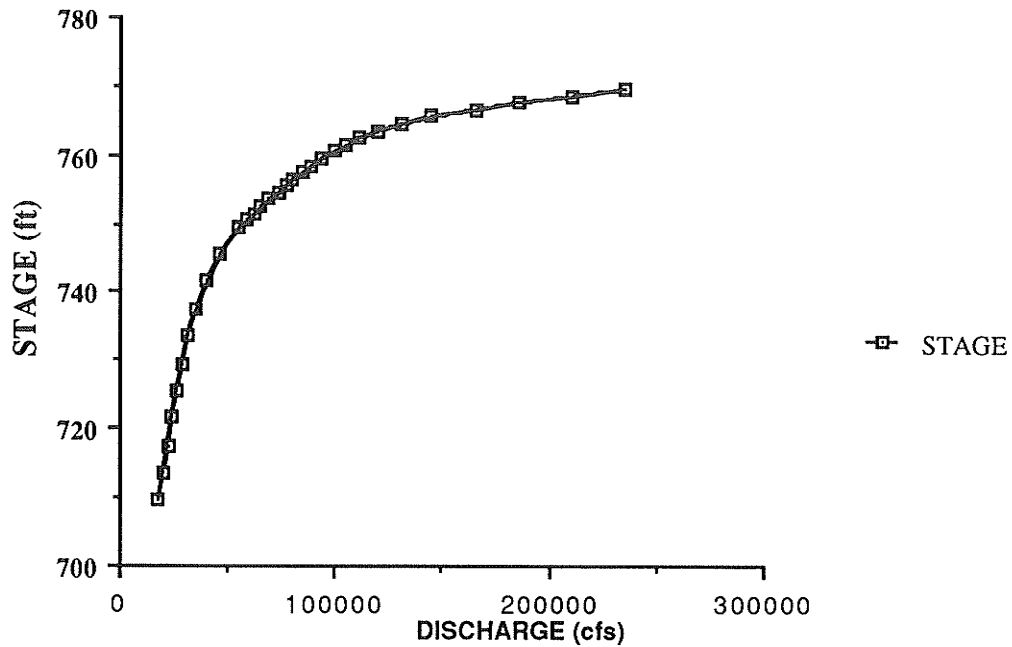


Figure 9. Stage-discharge relationship.

5.3 STRUCTURE INVENTORY ANALYSIS.

The SID program was used to determine the elevation-damage relationship for the existing conditions in the region. The consultation for data input into the model was as described in the previous chapter. Buildings situated in the area west of the West Dyke are protected from flooding of the Red River to a height of 787.4 ft and this was taken into

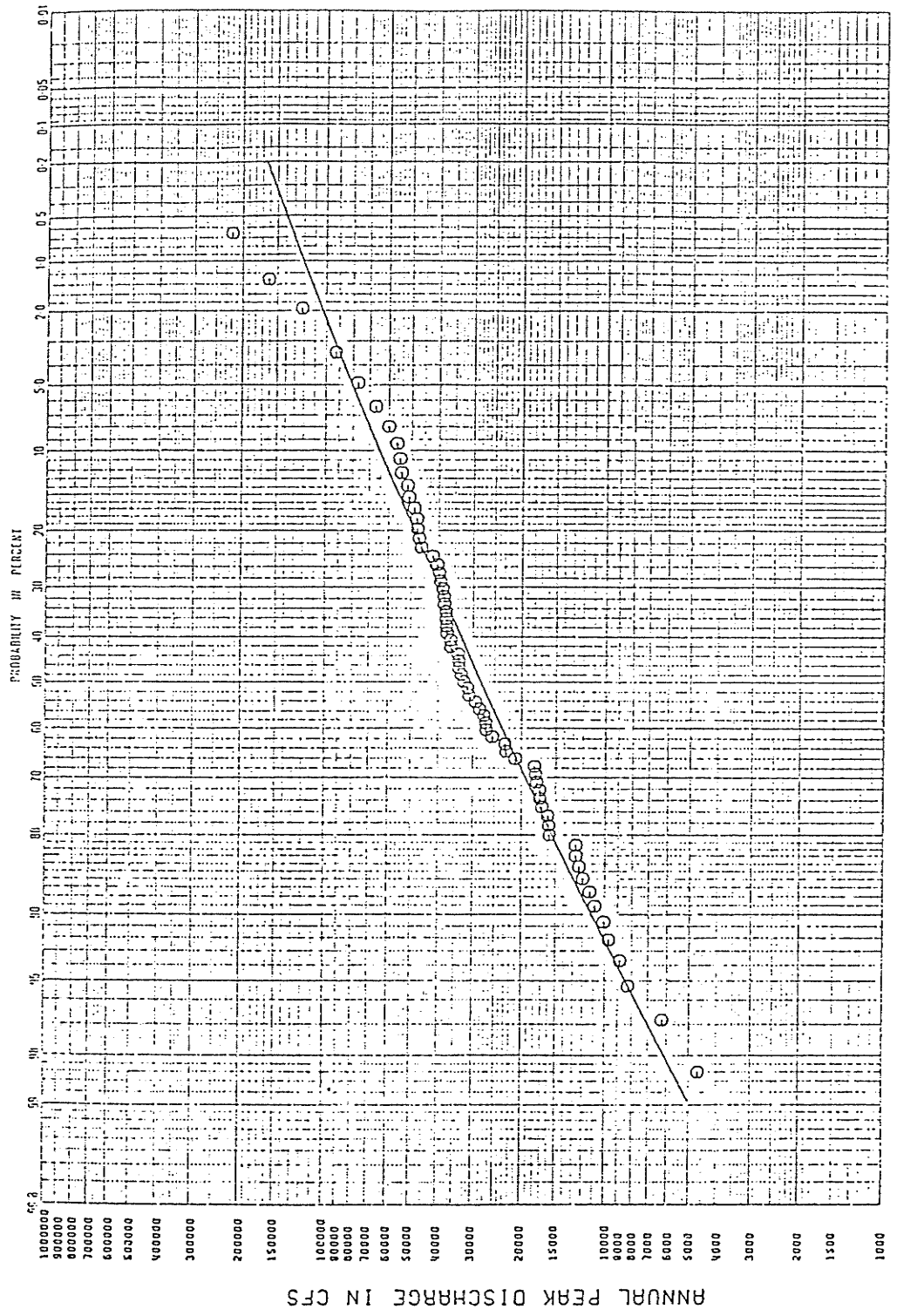


Figure 10. Discharge - probability curve

account when generating the elevation-damage relationship for this area, by specifying in the consultation that all these buildings are flood-proofed to a height of 787.4 ft.

The elevation-damage relationship was also generated for a number of flood control measures that were deemed both physically and economically feasible to be applied to the region. These measures were applied to only the buildings east of the west dyke, since the West Dyke offered the remaining dwellings some form of protection. Three non-structural measures and one structural measure were considered as both economically and physically feasible measures in the region.

The feasible flood control measures investigated are as shown in Table 4 below

1. Existing Conditions.
2. Raising individual structures to a height of 3ft.
3. Raising individual structures to a height of 5ft.
4. Flood Proofing individual structures to a height of 3ft.
5. Flood Proofing individual structures to a height of 5ft.
6. Relocation of structures to above the 754.0 ft.
7. Dyking along the Red River to the 725.4 ft level, i.e, a 20ft dyke.
8. Dyking along the Red River to the 745.4 ft level, i.e, a 40ft dyke.

Table 4. Feasible flood control measures.

Raising individual structures and flood proofing analyses were performed to a maximum height of 5 ft which is the recommended maximum height taking into account the economic burden to householders and aesthetics, (U.S. Army Corps of Engineers, 1987). Also, average annual cost as a percentage of structure value data was available for the application of such measures to heights of 3ft and 5ft, and since a cost of measure analysis was to be performed these heights were chosen.

Relocation of structures above a height of 750.4ft was also investigated. Several structures had ground elevation below this elevation and from an inspection of the flood plain, there was land available to relocate these structures above this level. The only structural flood control measure considered in the analysis was dyking of the Red River. This was investigated to heights of 20ft and 40ft.

The SID consultation was performed for each of the eight options, and the formatted input files and the output generated from each of these consultations are listed in Appendix D-1 and Appendix D-2, respectively. Output from the SID program for consultations from alternatives 1, 2, 3 and 6 were saved in a data storage utility provided with the programs named HECDSS. This utility makes the elevation-damage data readily available for use by the damage model EAD. The SID model did not permit flood-proofing analysis to be performed on more than one category, and so for options 4,5,7 and 8 the elevation-damage relationship was calculated for category 1 and then added manually to the elevation-damage relationship for category 2 obtained from consultation 1. The elevation-damage relationships for these categories are shown in Table 5.

STAGE (ft)	Alternative 4 (x \$1000)	Alternative 5 (x \$1000)	Alternative 6 (x \$1000)	Alternative 7 (x \$1000)
709	0	0	0	0
713	23.8	23.8	0	0
717	27.5	27.5	0	0
721	35.1	35.1	0	0
725	48.2	48.2	0	0
729	70.8	50.0	70.8	0
733	77.5	77.5	95.1	0
737	124.5	124.8	124.8	0
741	149.2	149.2	172.2	0
745	331.9	179.7	364.6	0
749	497.0	497.0	598.2	598.2
753	837.9	837.9	961.7	961.7
757	1435.3	1230.0	1435.0	1435.0
761	2677.8	1757.6	2787.4	2787.4
765	4167.8	3484.2	4487.8	4487.8
769	5752.2	5752.2	6649.8	6649.8
773	8555.0	8555.0	11374.0	11374.0
777	23001.0	16018.0	23062.0	23062.0

Table 5. Elevation-damage data for alternatives 4,5,7 & 8.

5.4 DAMAGE ANALYSIS.

Two particular damage analyses were performed: damage for a specific flood event and expected annual damage over a 50 year period.

Damage for a Specific Event

An analysis of damage for specific events was performed for 3 separate flood events, i.e., the 1950, 1970 and 1974 floods. The 1950 flood was the largest flood in 100 years, and the 1974 flood was the largest in recent decades. The damage accruing from each of these alternatives is shown in Table 7.

Expected Annual Damage

The analytical model EAD was used to compute the expected annual damage for a period of 50 years . The consultation was run interactively as described in the previous section and data from the SID model consultation was loaded into the EAD model for the respective options. The data values used for the computation of the expected annual damage are as listed below

1	Period of Analysis	50 years	
2	Study Year	1992	Year representing existing conditions
3	Base Year	1995	Year when plan takes effect
4	Dollar Year	1992	
5	Affluence Factor	1.2	
6	Discount Rate	5%	
7	Price Level Index	1.0	

Table 6. Data for expected annual damage computations.

Measure	Damage for specific event			Expected Annual Damage			Equivalent Annual Dam.
	1950	1970	1974	2004	2024	2044	
1	2571.0	1319.3	2212.8	389.8	525.0	707.2	435.6
2	1613.7	979.6	1446.1	269.2	362.6	488.4	300.9
3	1261.9	779.9	1137.2	208.4	280.7	378.1	232.9
4	2479.0	1288.4	2149.7	354.8	477.9	643.7	396.5
5	1673.2	1133.9	1533.4	301.3	405.9	546.7	336.8
6	865.0	0	592.1	44.7	60.2	81.1	49.9
7	2571.0	1319.3	2212.8	379.4	510.9	688.2	423.9
8	2571.0	1319.3	2212.8	293.7	395.5	532.7	382.2

Table 7. Damage and estimated annual damage results

5.5 COST COMPUTATION.

Average annual costs as a percentage of structure value data were obtained from U.S. Federal Insurance Agency (1970) data on estimate costs of implementing specific flood control measures. These values are listed in Table 8. The total estimated cost of implementing each non-structural flood control measure in the study area is computed by multiplying the number of structures to which the measure was applied by the cost of each measure. There were 702 buildings in category 1, having an average price of \$50,000, and 509 buildings in category 2, with an average price of \$80,000. The resultant annual costs are shown in the Table 8.

	Estimated Average annual cost as a percentage of Structure value	Total Cost (x \$1,000)
Existing Conditions	-	-
Flood Proofing to 3ft - Flood Wall	1.2	909.8
Flood Proofing to 3ft - Levee	0.5	379.1
Flood Proofing to 5ft - Flood Wall	1.6	1213.1
Flood Proofing to 5ft - Levee	0.7	530.7
Raising Structures to 3ft	2.1	1592.2
Raising Structures to 5ft	2.1	1592.2
Relocation of Structures - Demolish old ones	4.6	3487.7
Relocation of Structures - Leave structures standing	8.7	6596.3
Dyking Red River to height of 240m	-	-
Dyking Red River to height of 241m	-	-

Table 8. Costs of implementing flood control measures.

6. DISCUSSION OF RESULTS.

The decision support system developed in this research work was used to automate the process of generating alternative measures of flood control, and was used to compute indicators of the inundation-reduction benefits to be obtained from applying each measure such as damage from specific events, expected annual damage and the equivalent annual damage. The plots of the values computed for these indicators are shown in Figures 14-16 respectively. The results are discussed in the next section.

6.1 DAMAGE COMPUTATION RESULTS

An observation of the damage caused by specific events, Figure 11., shows that alternative 6 (i.e., relocating structures above a height of 754.0ft) was the measure that reduced damages the most in all the flood events. In the case of the flood of 1970 magnitude, this measure was successful in preventing any damage being incurred by householders living in the region. Alternatives 2 through 5 were also successful in reducing the damage below that which would prevail if existing conditions were to remain. Raising structures by a specified amount however proved to be more effective in reducing damages from these events than flood proofing to similar heights. This was generally due to the fact that both flood protection measures are breached by the selected floods, and since the damage curve for the raising structures options would begin at a higher elevation than that of the flood proofing options, damage by raising structures to 3ft and 5ft was less than flood proofing to 3ft and 5ft.

The expected annual damage, as mentioned previously, is the frequency weighted sum of damage for the full range of possible damaging flood events. It represents the damage for a particular set of hydrologic, hydraulic and damage conditions. Expected annual damage

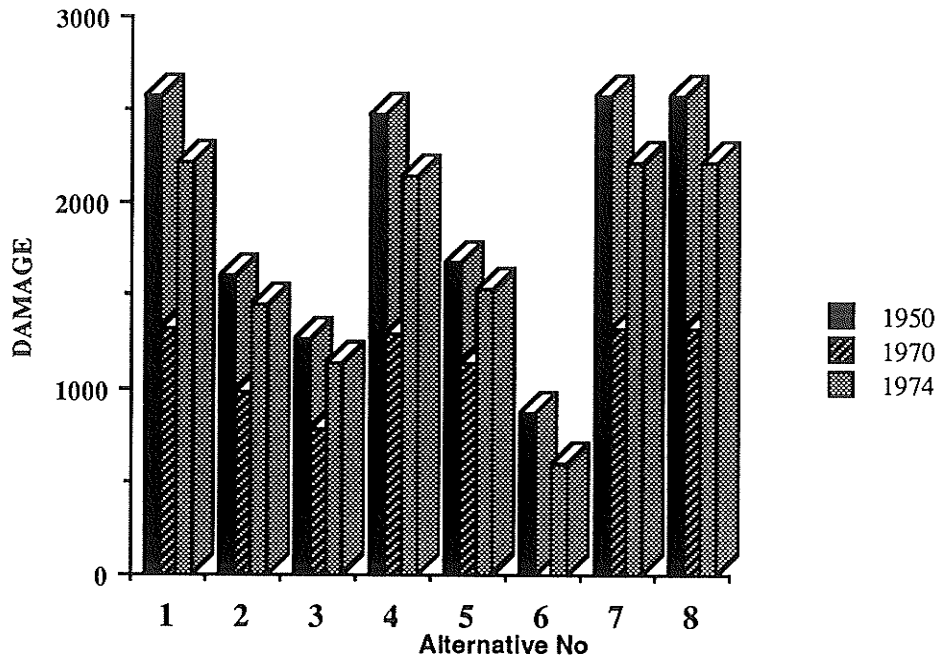


Figure 11. Damages for the magnitudes of the 1950, 1970 & 1974 floods

was computed for each year of the period of analysis and used in computing the equivalent annual damage. In determining the equivalent annual damage, each year's expected annual damage is discounted back to the base year and then amortized over the period of analysis.

The discounting formula used was:

$$P = F * \frac{1}{(1+i)^N}$$

where

P = Present amount of some future amount.

F = Future amount.

N = Number of years the future amount is from present.

i = Discount rate.

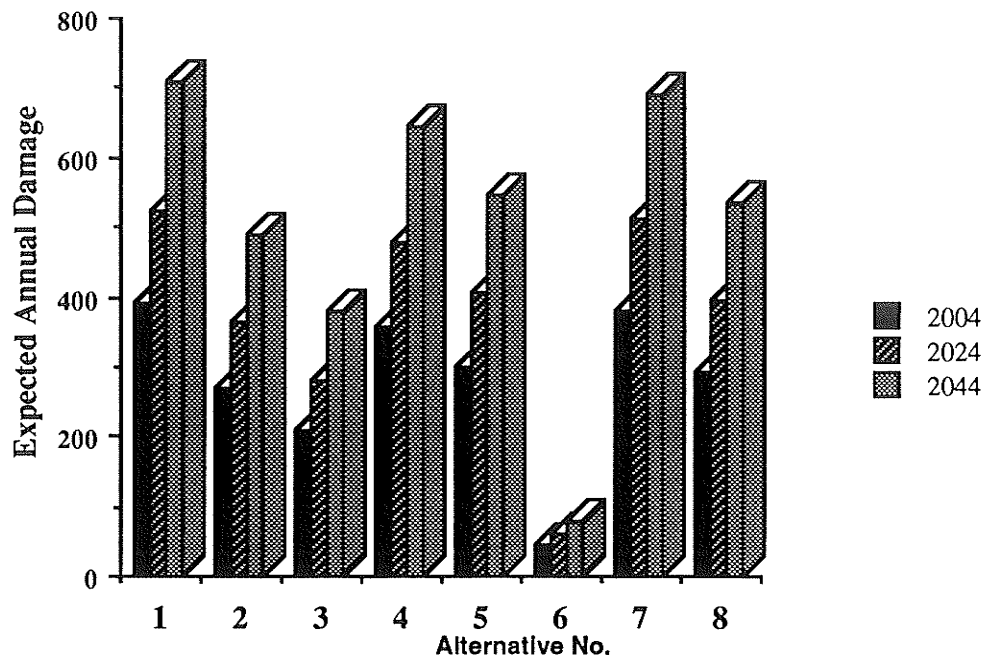


Figure 12. Expected annual damages for years 2004, 2024 & 2044.

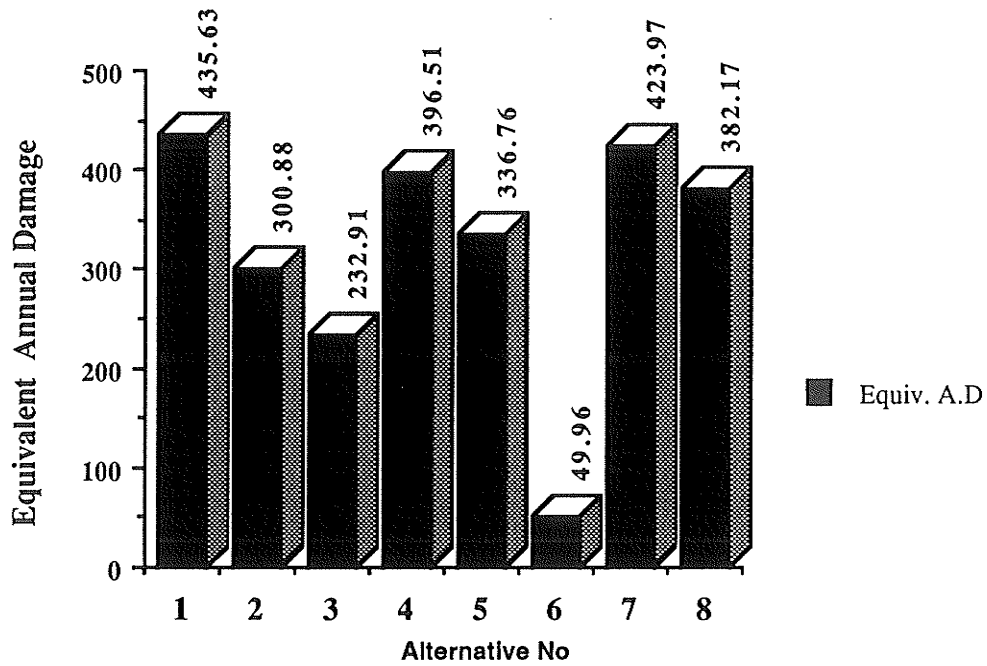


Figure 13. Equivalent Annual Damages.

The present amount of all future amounts over the period of analysis is then amortized using the formula:

$$A = P * \frac{i(1+i)^N}{(1+i)^N - 1}$$

where A = Equivalent annual amount.

The values obtained for the equivalent annual damages for each of the alternative measures are shown in Figure 13. It is seen that alternative number 6 is the measure that has the lowest value of equivalent annual damage, whilst alternative number 7 has the lowest value next to the existing conditions. The structure raising alternatives had lower equivalent annual damage values than the corresponding flood proofing values. Alternative 7, which is the dyking of the Red River to a height of 745 ft proved to be a more efficient measure than flood proofing to a height of 3ft, on the basis of these values.

The inundation reduction benefits of a flood plain management measure are the flood damages prevented by the plan. If it is assumed that the equivalent annual damage computed for the period of analysis represents damage to activities which would occupy the flood plain without a flood management plan, then the inundation reduction benefits can be computed by subtracting the equivalent annual damage for each measure from the equivalent annual damage without the plan.

Average annual costs of implementing the chosen flood control measures to the community as a whole were computed and shown in Table 8. These values showed that the flood proofing options would be the least costly to implement and the relocation of structures and the Red River dyking options the most expensive.

All the values obtained through the consultation are indicators of the benefits and costs that are associated with the implementation of the various structural and non-structural flood control measures that were selected for the analysis, and these values may form the basis for a multi-objective analysis in order to select the most suitable measure for implementation.

6.2 SPATIAL INTERPRETATION

The incorporation of the GIS software into the decision support system architecture provides a powerful tool for the display and manipulation of the results of the analyses performed in the previous chapters. This helps the user of the integrated tool to visualize the results obtained from the various alternatives generated in the previous sessions and allow the user to examine the consequences of these floods in detail, thus enabling a more complete understanding of each measure. There are several ways in which the GIS incorporated can provide visual support to the planning process and these are discussed below.

Showing the flooded areas

In cases where it is desired to examine the consequences of flooding from specific events, flooded areas resulting from these measures can be displayed both in 2-dimension and 3-dimensional overlay on an elevation map layer. This gives a representation of the area which will be flooded by this event. It is possible to utilize the routines provided in the GRASS GIS program to assist in performing backwater calculations along the reach to determine accurately the elevations at various points along the reach. For small reaches or study areas, such as the current project area under study with a size of 10 x 13km, the stage

to which a particular flood rises may be displayed as a constant level surface across the reach to provide an adequate flooded area representation.

Displaying damage by elevation.

Another visual display which can help the user to select the particular measure to be applied to the study area is a display of the resultant damage at every point in the reach for every level of elevation. For example, at elevation 750.4 it will be useful to display the variation in damages throughout the reach for a particular flood control alternative. This will assist in locating areas at high risk of sustaining major damages due to a particular flood at a particular elevation and thus highlighting these areas for special attention measures such as possible relocation of structures.

To be able to derive these maps, the damage function relationships for each structure or category of structures is utilized to obtain the elevation-damage relationships. These functions are used in conjunction with the GRASS program Ginfer to generate a new map which is an aggregation of the damages incurred by each building in the reach at a particular elevation. The GRASS program Ginfer is an inference engine which applies a set of user-specified rules to named map layers, U.S.Army CERL, (1988).

The procedure to be used is as follows:

1. The damage functions are first used to determine the actual damage to each building at intervals of 3ft.

2. The GRASS program Ginfer is used to interpret rules listed in a text file by the user and interpretes these to produce a new map layer. A typical rule that is used to generate the damage value for a building is as follows:

IFMAP	flooded area	725ft
ANDIFMAP	elevation	705ft
ANDIFMAP	buildings	1
THENMAPHYP	result	40000

Interpreted, this rule means that if the 3 maps "flooded area", "elevation" and "buildings" are overlain on each other, and there is a value representing 725ft in the map layer named "flooded area" and there is a value representing 705ft in the "elevation" map layer and if there is a cell representing category 1 in the "building" layer, the assign the value of 40,000 to this cell in a new map layer named "result".
[\$40,000 is the value computed to be the damage to a building of category 1 submerged to 20ft (725 ft - 705 ft)]

3. By establishing similar rules for the range of the damage function in intervals of say 3ft, the damages incurred for each cell in the map at a particular map layer can be computed and displayed in varying colours for easy interpretation.
4. The consultation for viewing these damage maps is controlled by NEXPERT, which would first prompt the user for the flood to use (i.e. 1970 flood). Then the consultation would then prompt for an elevation layer to view and upon

selection of an elevation layer the damages for every cell on the map is displayed.

7. CONCLUSIONS AND RECOMMENDATIONS

The research work presented in this thesis dealt with the development of a computer aided decision support system designed to provide comprehensive support in the domain of flood control planning, and outlined ways in which such a software tool comprising of an integration of technologies such as expert systems, geographic information systems, flood damage models and other routines can be used towards enhancing the solution process.

The interactive nature of the consultations outlined in the report, as well as the useful domain specific help facilities associated with each rule in the knowledge base of NEXPERT enable the user to quickly familiarize himself with the various tasks involved, such as data input to damage models and the proper selection of variables for model input. The use of already developed interactive shell, NEXPERT, with integratable capabilities also eliminated the time that would have been used in writing linkage code in order to establish the communication links between the various parts of the system.

The running of all the software to be integrated on a similar platform, the workstation platform, enables efficient linkage and inter-communication between the various system components and enables runtime speeds to be kept minimal. The workstation architecture also provided a conducive environment for the development of the system.

Geographic information systems played a key role in addressing the spatial aspects of the problem domain, from its role in providing data input to the damage models to help generate the complete structure inventory to its role in aiding the decision-maker in the visual comprehension of the consequences of the various flood management alternatives. There are several other ways in which GIS can be used to enhance the planning process. In the analysis performed individual structures or categories of structures were predefined from maps and these categories were then flood proofed using the same measure. The GIS

could be used to identify clumps or clusters of buildings which are amenable to be grouped into one category whereby joint flood control measures such as a ring dyke may be built around these structures. Identifying criteria such as a proximity distance of 20metres and and elevation range of 3 to 5 ft may be used to determine which structures may be grouped.

The use of a relational database to handle the storage and retrieval of data for use by the damage model facilitated the data handling process. In this project, the study area which made up an area of 10 x 13 km contained 1213 buildings. With a larger and more built up area under examination the data requirements would become large, and the question of ease of data storage and retrieval would be highly important if an efficient database manager were not employed. By being able to easily access, modify and retrieve information stored in the structure inventory database different flood plain scenarios can be constructed and investigated. The information in the database can also be retrieved and used for other inter-agency purposes and will serve as a valuable resource of watershed statistics which can be updated periodically.

There are several areas where the current system can benefit from further work and these are discussed briefly

FUTURE RESEARCH WORK

A complete inventory of all entities within the flood plain such as crops, livestock, utilities, etc, will provide a basis for inputting and obtaining a complete account of the study area and a more accurate damage assessment can then be carried out.

The incorporation of knowledge bases containing engineering expertise to be applied in semi- or ill- structured areas such as the selection of the type of non-structural

measures to apply and how to administer these measures (whether applied to individual structures or groups of structures) would further enhance the interactive process by providing online expertise to the user's fingertips.

The collection of additional hydrologic and hydraulic data such as channel morphology, and the inclusion of a model for hydrologic computations such as the HEC-2 model would enable accurate water surface elevation computations to be determined along the river reach.

The possible incorporation of multi-media applications such as animation - whereby the flood wave is simulated along the flood plain - and sound effects - providing accompanying sound which varies depending on the flood magnitude may help to improve the consultation process.

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APPENDIX A:

DATABASE INVENTORY
COMMANDS

APPENDIX A

APPENDIX A-1: GLOSSARY OF DATABASE COMMANDS

KODE1	-	Identification record.
IDRCH	-	Damage reach identification code.
IBDLG	-	Structure identification code.
ROWN	-	North coordinate point.
COLE	-	East coordinate point.
ADJ	-	Elevation of reference flood at the structure in feet.
STOPO	-	Elevation of reference point selected for the structure in feet; either of (1) First floor elevation, or (2) Ground flood elevation.
DELT	-	Distance between water surface elevation that can cause damage to begin, and first floor.
DELTB	-	Distance between elevation of basement floor and first floor.
DELTG	-	Distance between first floor and ground floor.
NEWSTR	-	(0) for existing structure, (1) for new structure.
KODE2	-	Identification record.
IDCAT	-	Damage category to which structure is assigned.
ID1FS	-	I.D. code for damage potential function of structure.
V1FS	-	Total value of structure in \$1,000.
ID1FC	-	I.D. code for damage potential function of contents.
V1FC	-	Total value of contents in \$1,000.
ID1FO	-	I.D. code for damage potential function of other items.
V1FO	-	Total value of other items in \$1,000.
IADDR	-	Column for comments and record keeping.

APPENDIX A

APPENDIX A-2

COMMANDS FOR CREATING DATABASE TABLES.

.....

```
CREATE TABLE ADOLPHE
(KODE1          CHAR(5),
 IDRCH          CHAR(5),
 IBDLG         NUMBER(8),
 ROWN          NUMBER(8),
 COLE          NUMBER(8),
 ADJ           NUMBER(8),
 STOPO         NUMBER(8),
 DELTZ         NUMBER(8),
 DELTB         NUMBER(8),
 DELTG         NUMBER(8),
 IFUNC         NUMBER(2),
 NEWSTR        NUMBER(1),
 KODE2         CHAR(5),
 IDCAT         CHAR(8),
 ID1FS         CHAR(3),
 V1FS          NUMBER(5),
 ID1FC         CHAR(3),
 V1FC          NUMBER(5),
 ID1FO         CHAR(3),
 V1FO          NUMBER(5),
 IADDR         CHAR(32),
 CATEGNO       NUMBER(4),
 DAMAGENO      NUMBER(2));
```

APPENDIX A

APPENDIX A-3

COMMANDS FOR LOADING DATA FROM GRASS.

LOAD DATA

INFILE siterpt.rst

INTO TABLE ADOLPHE

(IBDLG	POSITION(01:05) INTEGER EXTERNAL,
COLE	POSITION(08:14) INTEGER EXTERNAL,
ROWN	POSITION(18:25) INTEGER EXTERNAL,
DAMAGENO	POSITION(29:30) INTEGER EXTERNAL,
CATEGNO	POSITION(35:37) INTEGER EXTERNAL)

APPENDIX A

APPENDIX A-4

COMMANDS TO OUTPUT DATA FROM DATABASE

```
#DT 1 1 3 8 9 13 17 18 25 27 33 38 41 46 49 55 57 63 65
72 73 74 75 #
#DT 2 1 3 8 9 13 17 18 24 25 28 29 33 34 36 37 41 42 44
45 49 50 81 #
.DECLARE KODE1 a2
.DECLARE IDRCH a1
.DECLARE IBDLG 9999
.DECLARE ROWN 9999999
.DECLARE COLE 999999
.DECLARE ADJ 999
.DECLARE STOPO 999
.DECLARE DELTZ 9
.DECLARE DELTB 9
.DECLARE DELTG 9
.DECLARE IFUNC 9
.DECLARE KODE2 a2
.DECLARE IDCAT a7
.DECLARE ID1FS a3
.DECLARE V1FS 99999
.DECLARE ID1FC a3
.DECLARE V1FC 99999
.DECLARE ID1FO a3
.DECLARE V1FO 99999
.DECLARE IADDR a31
.DEFINE seldata
    SELECT KODE1, IDRCH, IBDLG, ROWN, COLE, ADJ, STOPO,
    DELTZ, DELTB, DELTG, IFUNC,
    KODE2, IDRCH, IBDLG, IDCAT, ID1FS, V1FS,
    ID1FC, V1FC, ID1FO, V1FO, IADDR
    INTO KODE1, IDRCH, IBDLG, ROWN, COLE, ADJ,
    STOPO, DELTZ, DELTB, DELTG, IFUNC, KODE2,
    IDRCH, IBDLG, IDCAT, ID1FS, V1FS, ID1FC,
    V1FC, ID1FO, V1FO, IADDR
    FROM ADOLPHE
    WHERE IBDLG > 0
    ORDER BY IBDLG
```

APPENDIX A

```
..  
.DEFINE body  
  #T 1 .PRINT  
  KODE1 #NC  
  .PRINT IDRCH  
  #NC .PRINT  
  IBDLG #NC  
  .PRINT ROWN  
  #NC .PRINT  
  COLE #NC  
  .PRINT ADJ  
  #NC .PRINT  
  STOPO #NC  
  .PRINT DELTZ  
  #NC .PRINT  
  DELTB #NC  
  .PRINT DELTG  
  #NC .PRINT  
  IFUNC #NC  
  #TE #T 2  
  .PRINT KODE2  
  #NC .PRINT  
  IDRCH #NC  
  .PRINT IBDLG  
  #NC .PRINT  
  IDCAT #NC  
  .PRINT ID1FS  
  #NC .PRINT  
  V1FS #NC  
  .PRINT ID1FC  
  #NC .PRINT  
  V1FC #NC  
  .PRINT ID1FO  
  #NC .PRINT  
  V1FO #NC  
  .PRINT IADDR  
  #NC #TE  
.DEFINE head  
.DEFINE foot  
.REPORT seldata body head foot  
.STOP
```

APPENDIX A

APPENDIX A-5

COMMANDS TO UPDATE THE DATABASE

```
UPDATE ADOLPHE
SET     KODE1 = 'SL'
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     KODE2 = 'SD'
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     IDRCH = '1'
WHERE  IBDLG > '0';
UPDATE ADOLPHE
SET     DELTZ = '0'
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     DELTB = '0'
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     DELTG = '2'
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     IFUNC = '0'
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     NEWSTR = '0'
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     ADJ = '705.0'
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     ID1FS = 'HR1'
WHERE  DAMAGENO = '2';
UPDATE ADOLPHE
SET     ID1FS = 'HR2'
WHERE  DAMAGENO = '1';
UPDATE ADOLPHE
SET     IDCAT = 'CAT1'
WHERE  IBDLG < '1114';
```


APPENDIX A

```
UPDATE ADOLPHE
SET     IDCAT = 'CAT2'
WHERE  IBDLG > '1113';
UPDATE ADOLPHE
SET     STOPO = (CATEGNO + 214)/0.3048
WHERE  IBDLG < '2000';
UPDATE ADOLPHE
SET     V1FS = '50'
WHERE  DAMAGENO = '1';
UPDATE ADOLPHE
SET     V1FS = '80'
WHERE  DAMAGENO = '2';
UPDATE ADOLPHE
SET     IADDR = 'EAST_OF_DYKE'
WHERE  IBDLG < '1114';
UPDATE ADOLPHE
SET     IADDR = 'WEST_OF_DYKE'
WHERE  IBDLG > '1113';
```

APPENDIX B:

EXPERT SYSTEMS
CONSULTATIONS

APPENDIX B1:

RULES FOR SID CONSULTATION.

```

CONDITIONS :
  Yes      r_t_t_done
  Yes      floodp_done
  Yes      str_reloc_done
  Yes      printout_done
HYPOTHESIS : analysis_done
ACTIONS :
  Execute  "echo @V(IPOL) @V(IPROF) @V(IEVAC) @V(IPRNT) >> sJ1" @TYPE=EXE;
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show     "/home/agyare/txt/df1.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name     IT      IT
  Name     NSTAG   NSTAG
HYPOTHESIS : df_done
ACTIONS :
  Execute  "echo @V(IT) >> sdf" @TYPE=EXE;
  Execute  "echo @V(NSTAG) >> sdf" @TYPE=EXE;
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show     "/home/agyare/txt/dmgfns1.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name     NODF    NODF
  Name     1      counter3
  Yes      loop3
HYPOTHESIS : dmgfns1_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show     "/home/agyare/txt/dmgfns2.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name     NODC    NODC
  Execute  "echo @V(NODC) > sDC" @TYPE=EXE;
  Name     1      counter4
  Yes      loop4
HYPOTHESIS : dmgfns2_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show     "/home/agyare/txt/dmgfns3.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name     NODR    NODR
  Name     1      counter5
  Yes      loop5
HYPOTHESIS : dmgfns3_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show     "/home/agyare/txt/dmgfns4.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name     AGG     AGG
HYPOTHESIS : dmgfns4_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Yes      dmgfns1_done
  Yes      dmgfns2_done
  Yes      dmgfns3_done
  Yes      dmgfns4_done
HYPOTHESIS : dmgfns_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show     "/home/agyare/txt/drt.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name     JDR     JDR
  Name     DTITLE  DTITLE
  Name     REFFLD  REFFLD
  Name     STRELV  STRELV

```

```

Execute      "echo @V(NODR) >> sDR"    @TYPE=EXE;
Execute      "echo @V(JDR) >> sDR"    @TYPE=EXE;
Execute      "echo @V(DTITLE) >> sDR"  @TYPE=EXE;
Execute      "echo @V(REFFLD) >> sDR"  @TYPE=EXE;
Execute      "echo @V(POLELV) >> sDR"  @TYPE=EXE;
Execute      "echo @V(PROELV) >> sDR"  @TYPE=EXE;
Execute      "echo @V(EVCELV) >> sDR"  @TYPE=EXE;
Execute      "echo @V(STRELV) >> sDR"  @TYPE=EXE;
HYPOTHESIS : drt_done
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Yes        ZW
HYPOTHESIS : dss_done
ACTIONS :
  Show       "/home/agyare/txt/sid1.txt" @KEEP=TRUE;@WAIT=FALSE;@RECT=0,275,480,340;
  Execute    "textedit -Wp 0 660 -Ws 480 200 sSDM" @TYPE=EXE;
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  No        ZW
HYPOTHESIS : dss_done
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Is        IPROFv "NEW STRUCTURES WRT ZERO DAMAGE"
HYPOTHESIS : floodp1_done
ACTIONS :
  Do        4      IPROF
  Do        j5_done j5_done
  Do        j6_done j6_done
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Is        IPROFv "NEW STRUCTURES WRT TARGET LEVEL"
HYPOTHESIS : floodp1_done
ACTIONS :
  Do        2      IPROF
  Do        j5_done j5_done
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Is        IPROFv "ALL STRUCTURES WRT ZERO DAMAGE"
HYPOTHESIS : floodp1_done
ACTIONS :
  Do        3      IPROF
  Do        j5_done j5_done
  Do        j6_done j6_done
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Is        IPROFv "ALL STRUCTURES WRT TARGET LEVEL"
HYPOTHESIS : floodp1_done
ACTIONS :
  Do        1      IPROF
  Do        j5_done j5_done
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Yes        floodp2_done
HYPOTHESIS : floodp_done
ACTIONS :
  Show       "/home/agyare/txt/floodp.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Do         floodp1_done floodp1_done
  Do         test2 test2
              INFERENCE PRIORITY :    1

```

```

NAME :
CONDITIONS :
  No      floodp2_done
HYPOTHESIS : floodp_done
ACTIONS :
  Do      0      IPROF
  Do      0      PROELV
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  =      1      1
HYPOTHESIS : gosid
ACTIONS :
  Show    "/home/agyare/txt/gosidl.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Execute "echo @V(NODF) @V(NODC) @V(NODR) @V(AGG) > sJ2" @TYPE=EXE;
  Execute "sidgo" @TYPE=EXE;@WAIT=TRUE;
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  =      1      1
HYPOTHESIS : grass
ACTIONS :
  Execute "/home/agyare/GRASS.src/go &" @TYPE=EXE;
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show    "/home/agyare/txt/j3.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name    NJPOL NJPOL
  Execute "echo @V(NJPOL) > sJ3" @TYPE=EXE;
  Name    1      counter6
  Yes     loop6
HYPOTHESIS : j3_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show    "/home/agyare/txt/j5.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name    NJPRF NJPRF
  Execute "echo @V(NJPRF) > sJ5" @TYPE=EXE;
  Name    1      counter8
  Yes     loop8
HYPOTHESIS : j5_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show    "/home/agyare/txt/j6.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Execute "echo @V(NJPRF) > sJ6" @TYPE=EXE;
  Name    1      counter9
  Yes     loop9
HYPOTHESIS : j6_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show    "/home/agyare/txt/j8.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name    NJEVAC NJEVAC
  Execute "echo @V(NJEVAC) > sJ8" @TYPE=EXE;
  Name    1      counter10
  Yes     loop10
HYPOTHESIS : j8_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Show    "/home/agyare/txt/ja.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Execute "echo @V(NJPOL) > sJA" @TYPE=EXE;
  Name    1      counter7
  Yes     loop7
HYPOTHESIS : ja_done

```

```

        INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
    <=          (counter10-NJEVAC)      0
    Name        JEVAC   JEVAC
HYPOTHESIS :   loop10
ACTIONS :
    Execute     "echo @V(JEVAC) >> sJ8" @TYPE=EXE;
    Do          counter10+1   counter10
    Reset       JEVAC
    Reset       loop10
        INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
    >          (counter10-NJEVAC)      0
HYPOTHESIS :   loop10
        INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
    <=          (counter11-NSTAG)      0
    Name        SSAGE   SSAGE
HYPOTHESIS :   loop11
ACTIONS :
    Execute     "echo @V(SSAGE) >> sDP" @TYPE=EXE;
    Do          counter11+1   counter11
    Reset       SSAGE
    Reset       loop11
        INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
    >          (counter11-NSTAG)      0
HYPOTHESIS :   loop11
        INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
    <=          (counter12-NSTAG)      0
    Name        PERCENTPP   PERCENTPP
HYPOTHESIS :   loop12
ACTIONS :
    Execute     "echo @V(PERCENTPP) >> sPC" @TYPE=EXE;
    Do          counter12+1   counter12
    Reset       PERCENTPP
    Reset       loop12
        INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
    >          (counter12-NSTAG)      0
HYPOTHESIS :   loop12
        INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
    <=          (counter13-NSTAG)      0
    Name        PERCENTD   PERCENTD
HYPOTHESIS :   loop13
ACTIONS :
    Execute     "echo @V(PERCENTD) >> sDD" @TYPE=EXE;
    Do          counter13+1   counter13
    Reset       PERCENTD
    Reset       loop13
        INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
    >          (counter13-NSTAG)      0
HYPOTHESIS :   loop13
        INFERENCE PRIORITY :    1
NAME :

```

```

CONDITIONS :
  <=      (counter3-NODF) 0
  Yes     df_done
  Name    1      counter11
  Yes     loop11
  Yes     pcdd_done
HYPOTHESIS :  loop3
ACTIONS :
  Do      counter3+1      counter3
  Reset   IT
  Reset   NSTAG
  Reset   df_done
  Reset   pcdd
  Reset   pcdd_done
  Reset   loop11
  Reset   loop3
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  >      (counter3-NODF) 0
HYPOTHESIS :  loop3
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  <=      (counter4-NODC) 0
  Name    JDCT      JDCT
  Name    TITDC     TITDC
  Name    POLMAX    POLMAX
  Name    PRFMAX    PRFMAX
HYPOTHESIS :  loop4
ACTIONS :
  Execute "echo @V(JDCT) @V(TITDC) @V(POLMAX) @V(PRFMAX) >> sDC" @TYPE=EXE;
  Do      counter4+1      counter4
  Reset   JDCT
  Reset   TITDC
  Reset   POLMAX
  Reset   PRFMAX
  Reset   loop4
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  >      (counter4-NODC) 0
HYPOTHESIS :  loop4
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  <=      (counter5-NODR) 0
  Yes     drt_done
HYPOTHESIS :  loop5
ACTIONS :
  Do      counter5+1      counter5
  Reset   JDR
  Reset   DTITLE
  Reset   REFFLD
  Reset   POELV
  Reset   PROELV
  Reset   EVCELV
  Reset   test1
  Reset   test2
  Reset   test3
  Reset   drt_done
  Reset   loop5
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  >      (counter5-NODR) 0

```



```

HYPOTHESIS :   loop5
      INFERENCE PRIORITY :   1
NAME :
CONDITIONS :
  <=      (counter6-NJPOL)      0
      Name      JPOL      JPOL
HYPOTHESIS :   loop6
ACTIONS :
  Execute  "echo @V(JPOL) >> sJ3" @TYPE=EXE;
  Do       counter6+1      counter6
  Reset    JPOL
  Reset    loop6
      INFERENCE PRIORITY :   1
NAME :
CONDITIONS :
  >      (counter6-NJPOL)      0
HYPOTHESIS :   loop6
      INFERENCE PRIORITY :   1
NAME :
CONDITIONS :
  <=      (counter7-NJPOL)      0
      Name      DPOL      DPOL
HYPOTHESIS :   loop7
ACTIONS :
  Execute  "echo @V(DPOL) >> sJA" @TYPE=EXE;
  Do       counter7+1      counter7
  Reset    DPOL
  Reset    loop7
      INFERENCE PRIORITY :   1
NAME :
CONDITIONS :
  >      (counter7-NJPOL)      0
HYPOTHESIS :   loop7
      INFERENCE PRIORITY :   1
NAME :
CONDITIONS :
  <=      (counter8-NJPRF)      0
      Name      JPRF      JPRF
HYPOTHESIS :   loop8
ACTIONS :
  Execute  "echo @V(JPRF) >> sJ5" @TYPE=EXE;
  Do       counter8+1      counter8
  Reset    JPRF
  Reset    loop8
      INFERENCE PRIORITY :   1
NAME :
CONDITIONS :
  >      (counter8-NJPRF)      0
HYPOTHESIS :   loop8
      INFERENCE PRIORITY :   1
NAME :
CONDITIONS :
  <=      (counter9-NJPRF)      0
      Name      DPRF      DPRF
HYPOTHESIS :   loop9
ACTIONS :
  Execute  "echo @V(DPRF) >> sJ6" @TYPE=EXE;
  Do       counter9+1      counter9
  Reset    DPRF
  Reset    loop9
      INFERENCE PRIORITY :   1
NAME :
CONDITIONS :
  >      (counter9-NJPRF)      0
HYPOTHESIS :   loop9
      INFERENCE PRIORITY :   1

```

```

NAME :
CONDITIONS :
  Is          pcdd    "DIRECT DAMAGE VALUES"
  Show        "/home/agyare/txt/damage.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name        1      IDF
  Execute     "echo @V(IDF) >> sdf" @TYPE=EXE;
  Name        1      counter13
  Yes         loop13
HYPOTHESIS : pcdd_done
              INFERENCE PRIORITY : 1

NAME :
CONDITIONS :
  Is          pcdd    "PERCENT DAMAGE VALUES"
  Show        "/home/agyare/txt/percent.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
  Name        0      IDF
  Execute     "echo @V(IDF) >> sdf" @TYPE=EXE;
  Name        1      counter12
  Yes         loop12
HYPOTHESIS : pcdd_done
              INFERENCE PRIORITY : 1

NAME :
CONDITIONS :
  Is          IPRNTv "SUPPRESS DAMREACH/ DAMFN PRINTOUT"
HYPOTHESIS : printout1_done
ACTIONS :
  Do          4      IPRNT
              INFERENCE PRIORITY : 1

NAME :
CONDITIONS :
  Is          IPRNTv "NORMAL PRINTOUT FOR ALL DAMREACHES"
HYPOTHESIS : printout1_done
ACTIONS :
  Do          0      IPRNT
              INFERENCE PRIORITY : 1

NAME :
CONDITIONS :
  Is          IPRNTv "SUPPRESS STRUCTURE PRINTOUT"
HYPOTHESIS : printout1_done
ACTIONS :
  Do          1      IPRNT
              INFERENCE PRIORITY : 1

NAME :
CONDITIONS :
  Is          IPRNTv "SUPPRESS DAMFUNCTION PRINTOUT"
HYPOTHESIS : printout1_done
ACTIONS :
  Do          2      IPRNT
              INFERENCE PRIORITY : 1

NAME :
CONDITIONS :
  Is          IPRNTv "SUPPRESS DAMFUNCTION & STRUCT PRINTOUT"
HYPOTHESIS : printout1_done
ACTIONS :
  Do          3      IPRNT
              INFERENCE PRIORITY : 1

NAME :
CONDITIONS :
  Yes         printout1_done
HYPOTHESIS : printout1_done
ACTIONS :
  Show        "/home/agyare/txt/printout.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,255;
              INFERENCE PRIORITY : 1

NAME :
CONDITIONS :
  Is          IPOLv  "ALL STRUCTURES TO DESIG. FLOOD LEVEL"
HYPOTHESIS : r_t1_done

```

```

ACTIONS :
  Do      1      IPOL
  Do      j3_done j3_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Is      IPOLv  "ALL STRUCTURES WITHIN DAMCAT"
HYPOTHESIS : r_t1_done
ACTIONS :
  Do      3      IPOL
  Do      j3_done j3_done
  Do      ja_done ja_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Is      IPOLv  "NEW STRUCTS TO DESIG. FLOOD LEVEL"
HYPOTHESIS : r_t1_done
ACTIONS :
  Do      2      IPOL
  Do      j3_done j3_done
  Do      ja_done ja_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Is      IPOLv  "ONLY NEW STRUCTURES WITHIN DAMCAT"
HYPOTHESIS : r_t1_done
ACTIONS :
  Do      4      IPOL
  Do      j3_done j3_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Yes     r_t_done
HYPOTHESIS : r_t_t_done
ACTIONS :
  Show    "/home/agyare/txt/r_t1_done.txt"      @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,
  Do      r_t1_done      r_t1_done
  Do      test1 test1
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  No      r_t_done
HYPOTHESIS : r_t_t_done
ACTIONS :
  Do      0      IPOL
  Do      0      POLELV
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Yes     grass
  Yes     title_done
  Yes     analysis_done
  Yes     dmgnfs_done
  Yes     dss_done
  Yes     gosid
HYPOTHESIS : sid_done
ACTIONS :
  UnloadKB "/home/agyare/new/sid.ckb"      @LEVEL=WIPEDOUT;
  LoadKB   "/home/agyare/new/ead.ckb"      @LEVEL=ENABLE;
  Do      ead_done      ead_done
          INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Is      IEVACv "ALL STRUCTS WITH ZERO.ELEV BELOW SPEC"
HYPOTHESIS : str_relocl_done
ACTIONS :

```

```

Do          3          IEVAC
Do          j8_done j8_done
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Is          IEVACv  "NEW STRUCTS WITH REF.ELEV BELOW SPEC"
HYPOTHESIS :   str_reloc1_done
ACTIONS :
  Do          2          IEVAC
  Do          j8_done j8_done
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Is          IEVACv  "ALL STRUCTS WITH REF.ELEV BELOW SPEC."
HYPOTHESIS :   str_reloc1_done
ACTIONS :
  Do          1          IEVAC
  Do          j8_done j8_done
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Is          IEVACv  "NEW STRUCTS WITH ZERO.ELEV BELOW SPEC."
HYPOTHESIS :   str_reloc1_done
ACTIONS :
  Do          4          IEVAC
  Do          j8_done j8_done
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Yes         str_reloc2_done
HYPOTHESIS :   str_reloc_done
ACTIONS :
  Show        "/home/agyare/txt/str_reloc_done.txt"  @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,
  Do          str_reloc1_done str_reloc1_done
  Do          test3  test3
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  No          str_reloc2_done
HYPOTHESIS :   str_reloc_done
ACTIONS :
  Do          0          IEVAC
  Do          0          EVCELV
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  =           IPOL      3
HYPOTHESIS :   test1
ACTIONS :
  Do          0          POLELV
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  =           IPOL      4
HYPOTHESIS :   test1
ACTIONS :
  Do          0          POLELV
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  =           IPOL      2
HYPOTHESIS :   test1
ACTIONS :
  Do          POLELV POLELV
      INFERENCE PRIORITY :    1
NAME :

```

```

CONDITIONS :
=          IPOL      1
HYPOTHESIS : test1
ACTIONS :
  Do          POELV  POELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IPOL      0
HYPOTHESIS : test1
ACTIONS :
  Do          0          POELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IPROF     0
HYPOTHESIS : test2
ACTIONS :
  Do          0          PROELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IPROF     3
HYPOTHESIS : test2
ACTIONS :
  Do          0          PROELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IPROF     2
HYPOTHESIS : test2
ACTIONS :
  Do          PROELV  PROELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IPROF     1
HYPOTHESIS : test2
ACTIONS :
  Do          PROELV  PROELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IPROF     4
HYPOTHESIS : test2
ACTIONS :
  Do          0          PROELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IEVAC     0
HYPOTHESIS : test3
ACTIONS :
  Do          0          EVCELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IEVAC     4
HYPOTHESIS : test3
ACTIONS :
  Do          EVCELV  EVCELV
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
=          IEVAC     3
HYPOTHESIS : test3

```

```
ACTIONS :
  Do          EVCELV EVCELV
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  =          IEVAC  2
HYPOTHESIS : test3
ACTIONS :
  Do          EVCELV EVCELV
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  =          IEVAC  1
HYPOTHESIS : test3
ACTIONS :
  Do          EVCELV EVCELV
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Show       "/home/agyare/txt/sid100.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,455;
  Name       TITLE TITLE
HYPOTHESIS : title_done
ACTIONS :
  Execute    "rm s??" @TYPE=EXE;
  Execute    "echo 'TT '@V(TITLE) > sTT" @TYPE=EXE;
              INFERENCE PRIORITY :    1
NAME :
```

APPENDIX B2:

RULES FOR EAD CONSULTATION.

```

CONDITIONS :
  Name      eNCAT  eNCAT
  Execute   "echo @V(eNCAT) > eCN" @TYPE=EXE;
  Name      1      count2
  Yes       lp2
HYPOTHESIS :  damcat_done
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Yes       title_done_ead
  Yes       period_done
  Yes       damcat_done
  Yes       plan_done
  Yes       reach_done
  Yes       eFR_done
  Yes       stagedam_done
  Yes       printout_done
  Yes       show_flood
HYPOTHESIS :  ead_done
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Is        eFR      "EXCEEDANCE-FREQUENCY VALUES"
HYPOTHESIS :  eFR_done
ACTIONS :
  Do        eNFRQ21 eNFRQ21
  Do        eNFRQ21 eNFRQ2
  Do        eNFRQ21 eNFRQ1
  Execute   "echo @V(eNFRQ1) > eFR" @TYPE=EXE;
  Do        1      count5
  Do        lp5     lp5
  Do        eFRDAM_done eFRDAM_done
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Is        eFR      "SINGLE FLOW VALUES"
HYPOTHESIS :  eFR_done
ACTIONS :
  Do        eNFRQ1  eNFRQ1
  Do        eNFRQ1  eNFRQ2
  Execute   "echo '-' @V(eNFRQ1) > eFR" @TYPE=EXE;
  Do        eFRDAM_done eFRDAM_done
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Is        eFRDAM1_done "FLOW VALUES"
HYPOTHESIS :  eFRDAM1_done
ACTIONS :
  Do        1      count6
  Do        lp6     lp6
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  Is        eFRDAM1_done "STAGE VALUES"
HYPOTHESIS :  eFRDAM1_done
ACTIONS :
  Do        1      count7
  Do        lp7     lp7
              INFERENCE PRIORITY : 1
NAME :
CONDITIONS :
  <=       (count1-eNHIS) 0
  Name     eIDYRS  eIDYRS
HYPOTHESIS :  lp1
ACTIONS :

```



```

Execute      "echo @V(eIDYRS) >> eDY"      @TYPE=EXE;
Do           count1+1      count1
Reset       eIDYRS
Reset       lp1
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
      >           (count1-eNHIS)  0
HYPOTHESIS :    lp1
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
      <=          (count2-eNCAT)  0
      Name       eNMCAT eNMCAT
HYPOTHESIS :    lp2
ACTIONS :
Execute      "echo @V(eNMCAT) >> eCN"      @TYPE=EXE;
Do           count2+1      count2
Reset       eNMCAT
Reset       lp2
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
      >           (count2-eNCAT)  0
HYPOTHESIS :    lp2
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
      <=          (count3-eIPLNN)  0
      Name       eNMPLN eNMPLN
HYPOTHESIS :    lp3
ACTIONS :
Execute      "echo @V(eNMPLN) >> ePN"      @TYPE=EXE;
Do           count3+1      count3
Reset       eNMPLN
Reset       lp3
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
      >           (count3-eIPLNN)  0
HYPOTHESIS :    lp3
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
      >           (count4-eIRCH)  0
HYPOTHESIS :    lp4
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
      <=          (count4-eIRCH)  0
      Name       eNMRCH eNMRCH
HYPOTHESIS :    lp4
ACTIONS :
Execute      "echo @V(eNMRCH) >> eRN"      @TYPE=EXE;
Do           count4+1      count4
Reset       eNMRCH
Reset       lp4
      INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
      <=          (count5-eFRQ2)  0
      Name       eFREQ2 eFREQ2
HYPOTHESIS :    lp5
ACTIONS :
Execute      "echo @V(eFREQ2) >> eFR"      @TYPE=EXE;
Do           count5+1      count5

```

```

Reset      eFREQ2
Reset      lp5
          INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
>          (count5-eNFRQ2) 0
HYPOTHESIS : lp5
          INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
<=        (count6-eNFRQ1) 0
Name      ePFRQ1 ePFRQ1
HYPOTHESIS : lp6
ACTIONS :
Execute   "echo @V(ePFRQ1) >> eQF"      @TYPE=EXE;
Do        count6+1      count6
Reset     ePFRQ1
Reset     lp6
          INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
>          (count6-eNFRQ1) 0
HYPOTHESIS : lp6
          INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
<=        (count7-eNFRQ2) 0
Name      ePFRQ2 ePFRQ2
HYPOTHESIS : lp7
ACTIONS :
Execute   "echo @V(ePFRQ2) >> eQF"      @TYPE=EXE;
Do        count7+1      count7
Reset     ePFRQ2
Reset     lp7
          INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
>          (count7-eNFRQ2) 0
HYPOTHESIS : lp7
          INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
Name      eIPOA  eIPOA
Name      eISTDYR eISTDYR
Name      eIBASYR eIBASYR
Name      eIDOLYR eIDOLYR
Yes       period3_done
Name      eRATE  eRATE
Name      eCPLI  eCPLI
HYPOTHESIS : period2_done
          INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
Name      eNHIS  eNHIS
Execute   "echo @V(eNHIS) > DY"      @TYPE=EXE;
Name      1      count1
Yes       lp1
HYPOTHESIS : period3_done
          INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
Yes       period1_done
HYPOTHESIS : period_done
ACTIONS :
Do        period2_done  period2_done
Execute   "echo @V(eIPOA) @V(eISTDYR) @V(eIBASYR) @V(eIDOLYR) @V(eNHIS) > eJ1"

```

```

Execute      "echo @V(eRATE) @V(eCPLI) > eJ2"          @TYPE=EXE;
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      No      period1_done
HYPOTHESIS :      period_done
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      Name      eIPLNN eIPLNN
      Execute   "echo @V(eIPLNN) > ePN" @TYPE=EXE;
      Name      1      count3
      Yes      lp3
HYPOTHESIS :      plan_done
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      Is      eJDGPRv "NO OUTPUT SUPPRESSED"
HYPOTHESIS :      printout_done
ACTIONS :
      Do      0      eJDGPR
      Execute "echo @V(eJDGPR) > ePP" @TYPE=EXE;
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      Is      eJDGPRv "SUPPRESS INPUT DATA PRINTOUT"
HYPOTHESIS :      printout_done
ACTIONS :
      Do      1      eJDGPR
      Execute "echo @V(eJDGPR) > ePP" @TYPE=EXE;
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      Is      eJDGPRv "SUPPRESS COMPUTED FLOW/STAGE PRINTOUT"
HYPOTHESIS :      printout_done
ACTIONS :
      Do      2      eJDGPR
      Execute "echo @V(eJDGPR) > ePP" @TYPE=EXE;
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      Is      eJDGPRv "SUPPRESS COMPUTED E.A.D. PRINTOUT"
HYPOTHESIS :      printout_done
ACTIONS :
      Do      4      eJDGPR
      Execute "echo @V(eJDGPR) > ePP" @TYPE=EXE;
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      Is      eJDGPRv "SUPPRESS SUMMARY BY REACH PRINTOUT"
HYPOTHESIS :      printout_done
ACTIONS :
      Do      16     eJDGPR
      Execute "echo @V(eJDGPR) > ePP" @TYPE=EXE;
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      Is      eJDGPRv "SUPPRESS GRAND SUMMARY BY REACH PRINTOUT"
HYPOTHESIS :      printout_done
ACTIONS :
      Do      32     eJDGPR
      Execute "echo @V(eJDGPR) > ePP" @TYPE=EXE;
      INFERENCE PRIORITY :      1
NAME :
CONDITIONS :
      Is      eJDGPRv "SUPPRESS ALL SUMMARY PRINTOUT"

```

```

HYPOTHESIS :    printout_done
ACTIONS :
  Do          64          eJDGPR
  Execute     "echo @V(eJDGPR) > ePP" @TYPE=EXE;
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Name       eIRCH    eIRCH
  Execute    "echo @V(eIRCH) > eRN" @TYPE=EXE;
  Name       1        count4
  Yes       lp4
HYPOTHESIS :    reach_done
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Execute    "/home/agyare/G/Gshow" @TYPE=EXE;
HYPOTHESIS :    show_flood
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  No        eSTGDAM
HYPOTHESIS :    stagedam_done
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Yes      eSTGDAM
HYPOTHESIS :    stagedam_done
ACTIONS :
  Show     "/home/agyare/txt/ead1.txt" @KEEP=FALSE;@WAIT=TRUE;@RECT=0,280,480,255;
  Execute  "cp /home/agyare/new/sSDDM /home/agyare/new/eSDDM" @TYPE=EXE;
  Execute  "textedit -Wp 0 660 -Ws 485 200 eSDDM" @TYPE=EXE;
              INFERENCE PRIORITY :    1
NAME :
CONDITIONS :
  Show     "/home/agyare/txt/ead100.txt" @KEEP=FALSE;@WAIT=FALSE;@RECT=0,280,480,400;
  Name     eTITLE eTITLE
HYPOTHESIS :    title_done_ead
ACTIONS :
  Execute  "rm e??" @TYPE=EXE;
  Execute  "echo 'TT' @V(eTITLE) > eTT " @TYPE=EXE;
              INFERENCE PRIORITY :    1
NAME :

```

APPENDIX C:

FORTRAN PROGRAMS

APPENDIX C1:

FORTRAN PROGRAMS FOR
FORMATTING SID FILES.

```

C
C
C
CHARACTER*6 JPOL
OPEN(1,FILE='file1')
OPEN(2,FILE='result10.s')
OPEN(3,FILE='sJ1')
OPEN(4,FILE='sJ2')
C
C for J1 required record
READ(3,*)IPOL,IPOF,IEVAC,IPRNT
WRITE(2,10)IPOL,IPOF,IEVAC,IPRNT
  10   FORMAT('J1',I6,I8,I8,8X,I8)
C
C for J2 required record
READ(4,*)NODF,NODC,NODR,AGG
WRITE(2,15)NODF,NODC,NODR,AGG
  15   FORMAT('J2',I6,I8,I8,F8.1)
  99  END

```

```

DIMENSION DPOL(10)
CHARACTER*10 LINE,PTER
OPEN(1,FILE='file1')
OPEN(2,FILE='result1.s')
OPEN(3,FILE='sJA')
PTER='sJA'
DO WHILE (LINE .NE. PTER)
  READ(1,*,END=30)LINE
  END DO
CLOSE(1)
  IF(LINE.EQ.PTER)THEN
    READ(3,*)NJPOL
    DO 20 I=1,NJPOL
      READ(3,*,END=30)DPOL(I)
    20  CONTINUE
    WRITE(2,40)(DPOL(I),I=1,NJPOL)
    40   FORMAT('JA',6X,6F8.1)
  ENDIF
  30  M=1
  99  END

```

```

DIMENSION JPRF(10)
CHARACTER*10 LINE,PTER
CHARACTER*7 JPRF
OPEN(1,FILE='file1')
OPEN(2,FILE='result2.s')
OPEN(3,FILE='sJ5')

```

```

PTER='sJ5'
DO WHILE (LINE .NE. PTER)
  READ(1,*,END=30)LINE
  END DO
CLOSE(1)
  IF(LINE.EQ.PTER)THEN
    READ(3,*)NJPRF
    DO 20 I=1,NJPRF
      READ(3,*,END=30)JPRF(I)
    20 CONTINUE
    WRITE(2,40)NJPRF,(JPRF(I),I=1,NJPRF)
    40 FORMAT('J5',I6,6A8)
  ENDIF
  30 M=1
  99 END

```

```

DIMENSION JPOL(10)
CHARACTER*10 LINE,PTER
CHARACTER*6 JPOL
OPEN(1,FILE='file1')
OPEN(2,FILE='result33.s')
OPEN(3,FILE='sJ3')
PTER='sJ3'
DO WHILE (LINE .NE. PTER)
  READ(1,*,END=30)LINE
  END DO
CLOSE(1)
  IF(LINE.EQ.PTER)THEN
    READ(3,*)NJPOL
    DO 20 I=1,NJPOL
      READ(3,*,END=30)JPOL(I)
    20 CONTINUE
    WRITE(2,40)NJPOL,(JPOL(I), I=1,NJPOL)
    40 FORMAT('J3',I6,6A8)
  ENDIF
  30 M=1
  99 END

```

```

DIMENSION DPRF(10)
CHARACTER*10 LINE,PTER
OPEN(1,FILE='file1')
OPEN(2,FILE='result3.s')
OPEN(3,FILE='sJ6')
PTER='sJ6'
DO WHILE (LINE .NE. PTER)
  READ(1,*,END=30)LINE

```



```

                END DO
CLOSE(1)
    IF(LINE.EQ.PTER)THEN
        READ(3,*)NJPRF
        DO 20 I=1,NJPRF
            READ(3,*,END=30)DPRF(I)
        20  CONTINUE
        WRITE(2,40)(DPRF(I),I=1,NJPRF)
        40     FORMAT('J6',6X,6F8.1)
    ENDIF
    30 M=1
    99  END

```

```

CHARACTER*10 ZW1,ZW2,ZW3
OPEN(1,FILE='sSDDM')
OPEN(2,FILE='result5.s')
READ(1,*,END=30)ZW1,ZW2,ZW3
WRITE(2,40)ZW1,ZW2,ZW3
    40     FORMAT('ZW',A14,A8,A16)
    30 M=1
    99  END

```

```

DIMENSION IT(100),NSTAG(100),IDF(100),ISAGE(200,200)
DIMENSION IPERCENT(200,200),IPERCENTX(200),ISAGEX(200)
DIMENSION IDAMAGE(200,200),IDAMAGEX(200)
OPEN(1,FILE='sJ2')
OPEN(2,FILE='result6.s')
OPEN(3,FILE='sDF')
OPEN(4,FILE='sDP')
OPEN(5,FILE='sPC')
OPEN(6,FILE='sDD')
C
READ(1,*)NODF
IF(NODF.EQ.1)THEN
GO TO 55
ENDIF
CLOSE(1)
    DO 20 I=1,NODF
        READ(3,*) IT(I)
        READ(3,*) NSTAG(I)
        READ(3,*) IDF(I)
        WRITE(2,30)IT(I),NSTAG(I),IDF(I)
    30     FORMAT('DF',3X,I3,I8,7X,I1)
        READ(4,*)(ISAGE(I,J),J=1,NSTAG(I))
        WRITE(2,31)(ISAGE(I,J),J=1,NSTAG(I))
    31     FORMAT('DP',I6,9(I8),/, 'DP',I6,9(I8))
    IF(IDF(I).EQ.0)THEN

```

```

        READ(5,*) (IPERCENT(I, J), J=1, NSTAG(I))
        WRITE(2, 32) (IPERCENT(I, J), J=1, NSTAG(I))
32      FORMAT('PC', I6, 9(I8), /, 'PC', I6, 9(I8))
    ELSE
        READ(6,*) (IDAMAGE(I, J), J=1, NSTAG(I))
        WRITE(2, 333) (IDAMAGE(I, J), J=1, NSTAG(I))
333    FORMAT('DD', I6, 9(I8), /, 'DD', I6, 9(I8))
    ENDIF
    20    CONTINUE
        GO TO 999
C
55    CLOSE(1)
        READ(3,*) ITX
        READ(3,*) NSTAGX
        READ(3,*) IDFX
        WRITE(2, 130) ITX, NSTAGX, IDFX
130    FORMAT('DF', 3X, I3, I8, 7X, I1)
        READ(4,*) (ISAGEX(J), J=1, NSTAGX)
        WRITE(2, 131) (ISAGEX(J), J=1, NSTAGX)
131    FORMAT('DP', I6, 9(I8), /, 'DP', I6, 9(I8))
        READ(3,*) CODE
        IF (IDFX.EQ.0) THEN
            READ(5,*) (IPERCENTX(J), J=1, NSTAGX)
            WRITE(2, 132) (IPERCENTX(J), J=1, NSTAGX)
132    FORMAT('PC', I6, 9(I8), /, 'PC', I6, 9(I8))
        ELSE
            READ(6,*) (IDAMAGEX(J), J=1, NSTAGX)
            WRITE(2, 444) (IDAMAGEX(J), J=1, NSTAGX)
444    FORMAT('DD', I6, 9(I8), /, 'DD', I6, 9(I8))
        ENDIF
999    END

```

```

DIMENSION JDCT(100), TITDC(100), POLMAX(100), PRFMAX(100)
CHARACTER*7 JDCT
CHARACTER*23 TITDC
OPEN(1, FILE='sDC')
OPEN(2, FILE='result7.s')
C
READ(1,*) NODC
write(*,*) 'hello'
    DO 20 I=1, NODC
        READ(1,*) JDCT(I), TITDC(I), POLMAX(I), PRFMAX(I)
        WRITE(2, 30) JDCT(I), POLMAX(I), PRFMAX(I), TITDC(I)
30    FORMAT('DC', 6X, A8, F8.1, F8.1, A32)
    20    CONTINUE
99    END

```

APPENDIX D:

INPUT AND OUTPUT FILES

APPENDIX D1:

**INPUT FILES FOR SID
CONSULTATION.**

TT	TEST 1 - EXISTING CONDITIONS									
J1	0	1	0		3					
J2	2	2	1	4.0			35			
J5	1 CAT2									
ZW	A=win		E=1992			F=plan1				
DF	HR1	20								
DP	0	1	2	3	4	5	6	7	8	
DP	9	10	11	12	13	14	15	16	17	
DP	18	19								
PC	0	1	8	14	18	22	25	28	29	
PC	30	32	36	41	45	48	51	54	57	
DP	60	63								
DF	HR2	20								
DP	0	1	2	3	4	5	6	7	8	
DP	9	10	11	12	13	14	15	16	17	
DP	18	19								
PC	0	4	23	32	38	45	50	53	55	
PC	55	55	58	63	65	72	77	82	87	
DP	100	100								
DC	CAT1					EAST_OF_DYKE				
DC	CAT2					WEST_OF_DYKE				
DR	1	705.4	0.0	787.4	0.0	705.0				
DT	DAMAGE_REACH_ONE									
SL	1	2	5500423	630950	705	787				2
SD	1	2	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	3	5500396	630949	705	787				2
SD	1	3	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	4	5500373	630949	705	784				2
SD	1	4	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	5	5500367	630973	705	784				2
SD	1	5	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	6	5500343	630946	705	787				2
SD	1	6	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	7	5500360	630921	705	784				2
SD	1	7	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	8	5500082	632415	705	784				2
SD	1	8	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	9	5500080	632448	705	787				2
SD	1	9	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	10	5500080	632463	705	784				2
SD	1	10	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	11	5500110	632500	705	787				2
SD	1	11	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	12	5500044	632494	705	787				2
SD	1	12	CAT1	HR2 50			EAST_OF_DYKE			

TT	TEST 2 - RAISING STRUCTURES TO A HEIGHT OF 3FT								
J1	3	1	0		3				
J2	2	2	1	4.0			35		
J3	1	CAT1							
JA		3							
J5	1	CAT2							
ZW	A=win	E=1992		F=plan2					
DF	HR1	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	1	8	14	18	22	25	28	29
PC	30	32	36	41	45	48	51	54	57
PC	60	63							
DF	HR2	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	4	23	32	38	45	50	53	55
PC	55	55	58	63	65	72	77	82	87
PC	100	100							
DC	CAT1		EAST_OF_DYKE						
DC	CAT2		WEST_OF_DYKE						
DR	1	705.4	0.0	787.4	0.0	705.0			
DT	DAMAGE_REACH_ONE								
SL	1	2	5500423	630950	705	787			2
SD	1	2	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	3	5500396	630949	705	787			2
SD	1	3	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	4	5500373	630949	705	784			2
SD	1	4	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	5	5500367	630973	705	784			2
SD	1	5	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	6	5500343	630946	705	787			2
SD	1	6	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	7	5500360	630921	705	784			2
SD	1	7	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	8	5500082	632415	705	784			2
SD	1	8	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	9	5500080	632448	705	787			2
SD	1	9	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	10	5500080	632463	705	784			2
SD	1	10	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	11	5500110	632500	705	787			2
SD	1	11	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	12	5500044	632494	705	787			2
SD	1	12	CAT1	HR2 50			EAST_OF_DYKE		

TT	TEST 3 - RAISING STRUCTURES TO A HEIGHT OF 5FT								
J1	3	1	0		3				
J2	2	2	1	4.0			35		
J3	1	CAT1							
JA		5							
J5	1	CAT2							
ZW	A=win	E=1992		F=plan3					
DF	HR1	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	1	8	14	18	22	25	28	29
PC	30	32	36	41	45	48	51	54	57
PC	60	63							
DF	HR2	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	4	23	32	38	45	50	53	55
PC	55	55	58	63	65	72	77	82	87
PC	100	100							
DC	CAT1					EAST_OF_DYKE			
DC	CAT2					WEST_OF_DYKE			
DR	1	705.4	0.0	787.4	0.0	705.0			
DT	DAMAGE_REACH_ONE								
SL	1	2	5500423	630950	705	787			2
SD	1	2	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	3	5500396	630949	705	787			2
SD	1	3	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	4	5500373	630949	705	784			2
SD	1	4	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	5	5500367	630973	705	784			2
SD	1	5	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	6	5500343	630946	705	787			2
SD	1	6	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	7	5500360	630921	705	784			2
SD	1	7	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	8	5500082	632415	705	784			2
SD	1	8	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	9	5500080	632448	705	787			2
SD	1	9	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	10	5500080	632463	705	784			2
SD	1	10	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	11	5500110	632500	705	787			2
SD	1	11	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	12	5500044	632494	705	787			2
SD	1	12	CAT1	HR2 50			EAST_OF_DYKE		

TEST 4 - FLOOD PROOFING OF STRUCTURES TO A HEIGHT OF 3FT

TT	0	3	0	3					
J1	2	2	1	4.0			35		
J2									
J5	1	CAT1							
J6		3							
ZW	A=win	E=1992		F=plan4					
DF	HR1	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	1	8	14	18	22	25	28	29
PC	30	32	36	41	45	48	51	54	57
PC	60	63							
DF	HR2	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	4	23	32	38	45	50	53	55
PC	55	55	58	63	65	72	77	82	87
PC	100	100							
DC		CAT1				EAST_OF_DYKE			
DC		CAT2				WEST_OF_DYKE			
DR	1	705.4	0.0	787.4	0.0	705.0			
DT		DAMAGE_REACH_ONE							
SL	1	2	5500423	630950	705	787			2
SD	1	2	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	3	5500396	630949	705	787			2
SD	1	3	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	4	5500373	630949	705	784			2
SD	1	4	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	5	5500367	630973	705	784			2
SD	1	5	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	6	5500343	630946	705	787			2
SD	1	6	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	7	5500360	630921	705	784			2
SD	1	7	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	8	5500082	632415	705	784			2
SD	1	8	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	9	5500080	632448	705	787			2
SD	1	9	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	10	5500080	632463	705	784			2
SD	1	10	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	11	5500110	632500	705	787			2
SD	1	11	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	12	5500044	632494	705	787			2
SD	1	12	CAT1	HR2 50			EAST_OF_DYKE		

TEST 5 - FLOOD PROOFING OF STRUCTURES TO A HEIGHT OF 5FT									
J1	0	3	0		3				
J2	2	2	1	4.0			35		
J5	1 CAT1								
J6		5							
ZW	A=win	E=1992		F=plan5					
DF	HR1	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	1	8	14	18	22	25	28	29
PC	30	32	36	41	45	48	51	54	55
PC	60	63							
DF	HR2	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	4	23	32	38	45	50	53	55
PC	55	55	58	63	65	72	77	82	87
PC	100	100							
DC	CAT1					EAST_OF_DYKE			
DC	CAT2					WEST_OF_DYKE			
DR	1	705.4	0.0	787.4	0.0	705.0			
DT	DAMAGE_REACH_ONE								
SL	1	2	5500423	630950	705	787			2
SD	1	2	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	3	5500396	630949	705	787			2
SD	1	3	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	4	5500373	630949	705	784			2
SD	1	4	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	5	5500367	630973	705	784			2
SD	1	5	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	6	5500343	630946	705	787			2
SD	1	6	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	7	5500360	630921	705	784			2
SD	1	7	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	8	5500082	632415	705	784			2
SD	1	8	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	9	5500080	632448	705	787			2
SD	1	9	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	10	5500080	632463	705	784			2
SD	1	10	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	11	5500110	632500	705	787			2
SD	1	11	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	12	5500044	632494	705	787			2
SD	1	12	CAT1	HR2 50			EAST_OF_DYKE		

TT	TEST 6 - RELOCATION OF STRUCTURES									
J1	0	1	3		3					
J2	2	2	1	4.0			35			
J5	1 CAT2									
J8	1 CAT1									
ZW	A=win		E=1992			F=plan6				
DF	HR1	20								
DP	0	1	2	3	4	5	6	7	8	
DP	9	10	11	12	13	14	15	16	17	
DP	18	19								
PC	0	1	8	14	18	22	25	28	29	
PC	30	32	36	41	45	48	51	54	57	
PC	60	63								
DF	HR2	20								
DP	0	1	2	3	4	5	6	7	8	
DP	9	10	11	12	13	14	15	16	17	
DP	18	19								
PC	0	4	23	32	38	45	50	53	55	
PC	55	55	58	63	65	72	77	82	87	
PC	100	100								
DC	CAT1					EAST_OF_DYKE				
DC	CAT2					WEST_OF_DYKE				
DR	1	705.4	0.0	787.4	754.0	705.0				
DT	DAMAGE_REACH_ONE									
SL	1	2	5500423	630950	705	787				2
SD	1	2	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	3	5500396	630949	705	787				2
SD	1	3	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	4	5500373	630949	705	784				2
SD	1	4	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	5	5500367	630973	705	784				2
SD	1	5	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	6	5500343	630946	705	787				2
SD	1	6	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	7	5500360	630921	705	784				2
SD	1	7	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	8	5500082	632415	705	784				2
SD	1	8	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	9	5500080	632448	705	787				2
SD	1	9	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	10	5500080	632463	705	784				2
SD	1	10	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	11	5500110	632500	705	787				2
SD	1	11	CAT1	HR2 50			EAST_OF_DYKE			
SL	1	12	5500044	632494	705	787				2
SD	1	12	CAT1	HR2 50			EAST_OF_DYKE			

TT	TEST 7 - DYKING THE RED RIVER TO A HEIGHT OF 20FT								
J1	0	1	0	3					
J2	2	2	1	4.0			35		
J5	1 CAT1								
ZW	A=win	E=1992	F=plan7						
DF	HR1	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	1	8	14	18	22	25	28	29
PC	30	32	36	41	45	48	51	54	57
PC	60	63							
DF	HR2	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	4	23	32	38	45	50	53	55
PC	55	55	58	63	65	72	77	82	87
PC	100	100							
DC	CAT1				EAST_OF_DYKE				
DC	CAT2				WEST_OF_DYKE				
DR	1	705.4	0.0	725.4	0.0	705.0			
DT	DAMAGE_REACH_ONE								
SL	1	2	5500423	630950	705	787			2
SD	1	2	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	3	5500396	630949	705	787			2
SD	1	3	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	4	5500373	630949	705	784			2
SD	1	4	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	5	5500367	630973	705	784			2
SD	1	5	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	6	5500343	630946	705	787			2
SD	1	6	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	7	5500360	630921	705	784			2
SD	1	7	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	8	5500082	632415	705	784			2
SD	1	8	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	9	5500080	632448	705	787			2
SD	1	9	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	10	5500080	632463	705	784			2
SD	1	10	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	11	5500110	632500	705	787			2
SD	1	11	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	12	5500044	632494	705	787			2
SD	1	12	CAT1	HR2 50			EAST_OF_DYKE		

TT	TEST 8 - DYKING THE RED RIVER TO A HEIGHT OF 40FT								
J1	0	1	0	3					
J2	2	2	1	4.0			35		
J5	1 CAT1								
ZW	A=win	E=1992	F=plan8						
DF	HR1	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	1	8	14	18	22	25	28	29
PC	30	32	36	41	45	48	51	54	57
PC	60	63							
DF	HR2	20							
DP	0	1	2	3	4	5	6	7	8
DP	9	10	11	12	13	14	15	16	17
DP	18	19							
PC	0	4	23	32	38	45	50	53	55
PC	55	55	58	63	65	72	77	82	87
PC	100	100							
DC	CAT1				EAST_OF_DYKE				
DC	CAT2				WEST_OF_DYKE				
DR	1	705.4	0.0	745.4	0.0	705.0			
DT	DAMAGE_REACH_ONE								
SL	1	2	5500423	630950	705	787			2
SD	1	2	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	3	5500396	630949	705	787			2
SD	1	3	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	4	5500373	630949	705	784			2
SD	1	4	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	5	5500367	630973	705	784			2
SD	1	5	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	6	5500343	630946	705	787			2
SD	1	6	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	7	5500360	630921	705	784			2
SD	1	7	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	8	5500082	632415	705	784			2
SD	1	8	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	9	5500080	632448	705	787			2
SD	1	9	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	10	5500080	632463	705	784			2
SD	1	10	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	11	5500110	632500	705	787			2
SD	1	11	CAT1	HR2 50			EAST_OF_DYKE		
SL	1	12	5500044	632494	705	787			2
SD	1	12	CAT1	HR2 50			EAST_OF_DYKE		

APPENDIX D2:

OUTPUT FILES FOR SID
CONSULTATION.

```
*****
*      Structure Inventory for Damage Analysis      *
*      Users Manual (March 1989)                  *
*      Version 2.0.04; August 1991                *
*      Sun Unix Workstation                        *
*      Run date 09APR92   time 05:22:57          *
*****
```

```
SSSSSSSS  IIIIIIII  DDDDDDD
SS         II       DD   DD
SS         II       DD   DD
SSSSSSSS  II       DD   DD
         SS       II   DD   DD
         SS       II   DD   DD
SSSSSSSS  IIIIIIII  DDDDDDD
```

```
*****
* U.S. Army Corps of Engineers      *
* The Hydrologic Engineering Center *
* 609 Second Street, Suite B       *
* Davis, California 95616          *
* (916) 756-1104                   *
*****
```

TEST 1 - EXISTING CONDITIONS

DAMAGE_REACH_ONE
 (Damages are in \$1,000)

Damage Categories

```
*****
* Elevation* CAT1      * CAT2          * Total *
*-----*-----*-----*-----*
* 705.00 * 0.0 * 0.0 * 0.0 *
* 709.00 * 9.2 * 0.0 * 9.2 *
* 713.00 * 23.8 * 0.0 * 23.8 *
* 717.00 * 27.5 * 0.0 * 27.5 *
* 721.00 * 35.1 * 0.0 * 35.1 *
* 725.00 * 51.6 * 0.0 * 51.6 *
* 729.00 * 70.8 * 0.0 * 70.8 *
* 733.00 * 95.1 * 0.0 * 95.1 *
* 737.00 * 124.8 * 0.0 * 124.8 *
* 741.00 * 172.2 * 0.0 * 172.2 *
* 745.00 * 364.6 * 0.0 * 364.6 *
* 749.00 * 598.2 * 0.0 * 598.2 *
* 753.00 * 961.7 * 0.0 * 961.7 *
* 757.00 * 1435.3 * 0.0 * 1435.3 *
* 761.00 * 2787.4 * 0.0 * 2787.4 *
* 765.00 * 4487.8 * 0.0 * 4487.8 *
* 769.00 * 6649.8 * 0.0 * 6649.8 *
* 773.00 * 11374.9 * 0.0 * 11374.9 *
* 777.00 * 23062.6 * 0.0 * 23062.6 *
* 781.00 * 30688.3 * 0.0 * 30688.3 *
* 785.00 * 38032.6 * 0.0 * 38032.6 *
*-----*-----*-----*-----*
* 787.40 * 43313.6 * 0.0 * 43313.6 *
*-----*-----*-----*-----*
* 789.00 * 46591.5 * 4338.6 * 50930.1 *
* 793.00 * 52414.9 * 4732.4 * 57147.3 *
* 797.00 * 53588.9 * 4829.3 * 58418.2 *
* 801.00 * 54590.4 * 4912.5 * 59502.9 *
* 805.00 * 55411.4 * 4978.5 * 60389.8 *
* 809.00 * 55784.3 * 5008.1 * 60792.3 *
* 813.00 * 55787.1 * 5016.7 * 60803.8 *
* 817.00 * 55787.1 * 5017.2 * 60804.3 *
* 821.00 * 55787.1 * 5017.2 * 60804.3 *
* 825.00 * 55787.1 * 5017.2 * 60804.3 *
* 829.00 * 55787.1 * 5017.2 * 60804.3 *
* 833.00 * 55787.1 * 5017.2 * 60804.3 *
* 837.00 * 55787.1 * 5017.2 * 60804.3 *
* 841.00 * 55787.1 * 5017.2 * 60804.3 *
*****
```

PROELV

```
*****
Damage category CAT1 identified as EAST_OF_DYKE
Damage category CAT2 identified as WEST_OF_DYKE
Damage category OTHER identified as OTHER DAMAGE CATEGORIES
*****
```

TEST 2 - RAISING STRUCTURES TO A HEIGHT OF 3FT

DAMAGE_REACH_ONE
(Damages are in \$1,000)

Damage Categories

```
*****
* Elevation* CAT1      * CAT2      * Total *
*-----*-----*-----*-----*
* 705.00 * 0.0 * 0.0 * 0.0 *
* 709.00 * 0.0 * 0.0 * 0.0 *
* 713.00 * 13.7 * 0.0 * 13.7 *
* 717.00 * 25.7 * 0.0 * 25.7 *
* 721.00 * 28.7 * 0.0 * 28.7 *
* 725.00 * 37.5 * 0.0 * 37.5 *
* 729.00 * 59.2 * 0.0 * 59.2 *
* 733.00 * 73.8 * 0.0 * 73.8 *
* 737.00 * 103.1 * 0.0 * 103.1 *
* 741.00 * 130.2 * 0.0 * 130.2 *
* 745.00 * 222.3 * 0.0 * 222.3 *
* 749.00 * 410.2 * 0.0 * 410.2 *
* 753.00 * 662.2 * 0.0 * 662.2 *
* 757.00 * 1082.6 * 0.0 * 1082.6 *
* 761.00 * 1714.8 * 0.0 * 1714.8 *
* 765.00 * 3209.9 * 0.0 * 3209.9 *
* 769.00 * 4857.1 * 0.0 * 4857.1 *
* 773.00 * 7186.7 * 0.0 * 7186.7 *
* 777.00 * 14036.0 * 0.0 * 14036.0 *
* 781.00 * 25494.8 * 0.0 * 25494.8 *
* 785.00 * 32296.8 * 0.0 * 32296.8 *
*-----*-----*-----*-----*
* 787.40 * 36713.2 * 0.0 * 36713.2 *
*-----*-----*-----*-----*
* 789.00 * 40118.9 * 4338.6 * 44457.5 *
* 793.00 * 48532.3 * 4732.4 * 53264.7 *
* 797.00 * 52864.1 * 4829.3 * 57693.4 *
* 801.00 * 53851.7 * 4912.5 * 58764.2 *
* 805.00 * 54815.0 * 4978.5 * 59793.5 *
* 809.00 * 55552.5 * 5008.1 * 60560.6 *
* 813.00 * 55787.1 * 5016.7 * 60803.8 *
* 817.00 * 55787.1 * 5017.2 * 60804.3 *
* 821.00 * 55787.1 * 5017.2 * 60804.3 *
* 825.00 * 55787.1 * 5017.2 * 60804.3 *
* 829.00 * 55787.1 * 5017.2 * 60804.3 *
* 833.00 * 55787.1 * 5017.2 * 60804.3 *
* 837.00 * 55787.1 * 5017.2 * 60804.3 *
* 841.00 * 55787.1 * 5017.2 * 60804.3 *
*****
```

PROELV

```
*****
Damage category CAT1 identified as EAST_OF_DYKE
Damage category CAT2 identified as WEST_OF_DYKE
Damage category OTHER identified as OTHER DAMAGE CATEGORIES
*****
```


TEST 3 - RAISING STRUCTURES TO A HEIGHT OF 5FT

DAMAGE_REACH_ONE
 (Damages are in \$1,000)

Damage Categories

```
*****
* Elevation* CAT1   * CAT2       * Total *
*-----*-----*-----*
* 705.00 * 0.0 * 0.0 * 0.0 *
* 709.00 * 0.0 * 0.0 * 0.0 *
* 713.00 * 3.4 * 0.0 * 3.4 *
* 717.00 * 20.8 * 0.0 * 20.8 *
* 721.00 * 27.5 * 0.0 * 27.5 *
* 725.00 * 32.8 * 0.0 * 32.8 *
* 729.00 * 43.7 * 0.0 * 43.7 *
* 733.00 * 67.5 * 0.0 * 67.5 *
* 737.00 * 87.2 * 0.0 * 87.2 *
* 741.00 * 118.5 * 0.0 * 118.5 *
* 745.00 * 140.2 * 0.0 * 140.2 *
* 749.00 * 312.7 * 0.0 * 312.7 *
* 753.00 * 513.2 * 0.0 * 513.2 *
* 757.00 * 866.4 * 0.0 * 866.4 *
* 761.00 * 1337.3 * 0.0 * 1337.3 *
* 765.00 * 2401.1 * 0.0 * 2401.1 *
* 769.00 * 4007.1 * 0.0 * 4007.1 *
* 773.00 * 6030.2 * 0.0 * 6030.2 *
* 777.00 * 9957.3 * 0.0 * 9957.3 *
* 781.00 * 20333.5 * 0.0 * 20333.5 *
* 785.00 * 29029.4 * 0.0 * 29029.4 *
*-----*-----*-----*
* 787.40 * 32856.5 * 0.0 * 32856.5 *
*-----*-----*-----*
* 789.00 * 35706.6 * 4338.6 * 40045.2 *
* 793.00 * 44709.7 * 4732.4 * 49442.1 *
* 797.00 * 51796.8 * 4829.3 * 56626.2 *
* 801.00 * 53346.4 * 4912.5 * 58258.9 *
* 805.00 * 54295.7 * 4978.5 * 59274.1 *
* 809.00 * 55255.9 * 5008.1 * 60263.9 *
* 813.00 * 55777.0 * 5016.7 * 60793.8 *
* 817.00 * 55787.1 * 5017.2 * 60804.3 *
* 821.00 * 55787.1 * 5017.2 * 60804.3 *
* 825.00 * 55787.1 * 5017.2 * 60804.3 *
* 829.00 * 55787.1 * 5017.2 * 60804.3 *
* 833.00 * 55787.1 * 5017.2 * 60804.3 *
* 837.00 * 55787.1 * 5017.2 * 60804.3 *
* 841.00 * 55787.1 * 5017.2 * 60804.3 *
*****
```

PROELV

```
*****
Damage category CAT1 identified as EAST_OF_DYKE
Damage category CAT2 identified as WEST_OF_DYKE
Damage category OTHER identified as OTHER DAMAGE CATEGORIES
```

TEST 4 - FLOOD PROOFING OF STRUCTURES TO A HEIGHT OF 3FT

DAMAGE_REACH_ONE
 (Damages are in \$1,000)

Damage Categories

```

*****
* Elevation* CAT1      * CAT2      * Total *
*-----*-----*-----*-----*
* 705.00 * 0.0 * 0.0 * 0.0 *
* 709.00 * 0.0 * 0.0 * 0.0 *
* 713.00 * 23.8 * 0.0 * 23.8 *
* 717.00 * 27.5 * 0.0 * 27.5 *
* 721.00 * 35.1 * 0.0 * 35.1 *
* 725.00 * 48.2 * 0.0 * 48.2 *
* 729.00 * 70.8 * 0.0 * 70.8 *
* 733.00 * 77.5 * 0.0 * 77.5 *
* 737.00 * 124.8 * 0.0 * 124.8 *
* 741.00 * 149.2 * 3.4 * 152.7 *
* 745.00 * 331.9 * 20.8 * 352.7 *
* 749.00 * 497.0 * 41.8 * 538.8 *
* 753.00 * 837.9 * 75.8 * 913.4 *
* 757.00 * 1435.3 * 148.8 * 1584.2 *
* 761.00 * 2677.8 * 303.8 * 2981.6 *
* 765.00 * 4167.8 * 526.2 * 4694.0 *
* 769.00 * 5752.2 * 823.2 * 6575.4 *
* 773.00 * 8555.0 * 1402.4 * 9957.5 *
* 777.00 * 23001.2 * 2398.9 * 25400.2 *
* 781.00 * 30623.9 * 3059.3 * 33683.2 *
* 785.00 * 37783.1 * 3652.4 * 41435.5 *
*-----*-----*-----*-----*
* 787.40 * 43132.1 * 4071.5 * 47203.6 *
*-----*-----*-----*-----*
* 789.00 * 46146.0 * 4338.6 * 50484.6 *
* 793.00 * 52414.9 * 4732.4 * 57147.3 *
* 797.00 * 53588.9 * 4829.3 * 58418.2 *
* 801.00 * 54590.4 * 4912.5 * 59502.9 *
* 805.00 * 55411.4 * 4978.5 * 60389.8 *
* 809.00 * 55784.3 * 5008.1 * 60792.3 *
* 813.00 * 55787.1 * 5016.7 * 60803.8 *
* 817.00 * 55787.1 * 5017.2 * 60804.3 *
* 821.00 * 55787.1 * 5017.2 * 60804.3 *
* 825.00 * 55787.1 * 5017.2 * 60804.3 *
* 829.00 * 55787.1 * 5017.2 * 60804.3 *
* 833.00 * 55787.1 * 5017.2 * 60804.3 *
* 837.00 * 55787.1 * 5017.2 * 60804.3 *
* 841.00 * 55787.1 * 5017.2 * 60804.3 *
*****
    
```

PROELV

```

*****
Damage category CAT1 identified as EAST_OF_DYKE
Damage category CAT2 identified as WEST_OF_DYKE
Damage category OTHER identified as OTHER DAMAGE CATEGORIES
    
```

TEST 5 - FLOOD PROOFING OF STRUCTURES TO A HEIGHT OF 5FT

DAMAGE_REACH_ONE
 (Damages are in \$1,000)

Damage Categories

```
*****
* Elevation* CAT1      * CAT2      *   Total  *
*-----*-----*-----*-----*
* 705.00 *    0.0 *    0.0 *    0.0 *
* 709.00 *    0.0 *    0.0 *    0.0 *
* 713.00 *   23.8 *    0.0 *   23.8 *
* 717.00 *   27.5 *    0.0 *   27.5 *
* 721.00 *   35.1 *    0.0 *   35.1 *
* 725.00 *   48.2 *    0.0 *   48.2 *
* 729.00 *   50.0 *    0.0 *   50.0 *
* 733.00 *   77.5 *    0.0 *   77.5 *
* 737.00 *  124.8 *    0.0 *  124.8 *
* 741.00 *  149.2 *    3.4 *  152.7 *
* 745.00 *  179.7 *   20.8 *  200.5 *
* 749.00 *  497.0 *   41.8 *  538.8 *
* 753.00 *  837.9 *   75.5 *  913.4 *
* 757.00 * 1230.0 *  148.8 * 1378.9 *
* 761.00 * 1757.6 *  303.8 * 2061.4 *
* 765.00 * 3484.2 *  526.2 * 4010.4 *
* 769.00 * 5752.2 *  823.2 * 6575.4 *
* 773.00 * 8555.0 * 1402.4 * 9957.5 *
* 777.00 * 16018.7 * 2398.9 * 18417.6 *
* 781.00 * 30231.5 * 3059.3 * 33290.8 *
* 785.00 * 37381.3 * 3652.4 * 41033.7 *
*-----*-----*-----*-----*
* 787.40 * 42609.3 * 4071.5 * 46680.8 *
*-----*-----*-----*-----*
* 789.00 * 46146.0 * 4338.6 * 50484.6 *
* 793.00 * 51795.6 * 4732.4 * 56528.0 *
* 797.00 * 53588.9 * 4829.3 * 58418.2 *
* 801.00 * 54590.4 * 4912.5 * 59502.9 *
* 805.00 * 55411.4 * 4978.5 * 60389.8 *
* 809.00 * 55784.3 * 5008.1 * 60792.3 *
* 813.00 * 55787.1 * 5016.7 * 60803.8 *
* 817.00 * 55787.1 * 5017.2 * 60804.3 *
* 821.00 * 55787.1 * 5017.2 * 60804.3 *
* 825.00 * 55787.1 * 5017.2 * 60804.3 *
* 829.00 * 55787.1 * 5017.2 * 60804.3 *
* 833.00 * 55787.1 * 5017.2 * 60804.3 *
* 837.00 * 55787.1 * 5017.2 * 60804.3 *
* 841.00 * 55787.1 * 5017.2 * 60804.3 *
*****
```

PROELV

```
*****
Damage category CAT1 identified as EAST_OF_DYKE
Damage category CAT2 identified as WEST_OF_DYKE
Damage category OTHER identified as OTHER DAMAGE CATEGORIES
*****
```

TEST 6 - RELOCATION OF STRUCTURES

DAMAGE_REACH_ONE
 (Damages are in \$1,000)

Damage Categories

```

*****
* Elevation * CAT1 * CAT2 * Total *
*-----*-----*-----*-----*
* 705.00 * 0.0 * 0.0 * 0.0 *
* 709.00 * 0.0 * 0.0 * 0.0 *
* 713.00 * 0.0 * 0.0 * 0.0 *
* 717.00 * 0.0 * 0.0 * 0.0 *
* 721.00 * 0.0 * 0.0 * 0.0 *
* 725.00 * 0.0 * 0.0 * 0.0 *
* 729.00 * 0.0 * 0.0 * 0.0 *
* 733.00 * 0.0 * 0.0 * 0.0 *
* 737.00 * 0.0 * 0.0 * 0.0 *
* 741.00 * 0.0 * 0.0 * 0.0 *
* 745.00 * 0.0 * 0.0 * 0.0 *
* 749.00 * 0.0 * 0.0 * 0.0 *
* 753.00 * 0.0 * 0.0 * 0.0 *
*-----*-----*-----*-----*
* 754.00 * 0.0 * 0.0 * 0.0 *
*-----*-----*-----*-----*
* 757.00 * 0.0 * 0.0 * 0.0 *
* 761.00 * 1029.8 * 0.0 * 1029.8 *
* 765.00 * 2448.6 * 0.0 * 2448.6 *
* 769.00 * 4365.1 * 0.0 * 4365.1 *
* 773.00 * 8972.5 * 0.0 * 8972.5 *
* 777.00 * 20659.7 * 0.0 * 20659.7 *
* 781.00 * 28285.5 * 0.0 * 28285.5 *
* 785.00 * 35629.8 * 0.0 * 35629.8 *
*-----*-----*-----*-----*
* 787.40 * 40910.8 * 0.0 * 40910.8 *
*-----*-----*-----*-----*
* 789.00 * 44188.8 * 4338.6 * 48527.4 *
* 793.00 * 50012.1 * 4732.4 * 54744.5 *
* 797.00 * 51186.1 * 4829.3 * 56015.4 *
* 801.00 * 52187.6 * 4912.5 * 57100.1 *
* 805.00 * 53008.6 * 4978.5 * 57987.0 *
* 809.00 * 53381.5 * 5008.1 * 58389.5 *
* 813.00 * 53384.3 * 5016.7 * 58401.0 *
* 817.00 * 53384.3 * 5017.2 * 58401.5 *
* 821.00 * 53384.3 * 5017.2 * 58401.5 *
* 825.00 * 53384.3 * 5017.2 * 58401.5 *
* 829.00 * 53384.3 * 5017.2 * 58401.5 *
* 833.00 * 53384.3 * 5017.2 * 58401.5 *
* 837.00 * 53384.3 * 5017.2 * 58401.5 *
* 841.00 * 53384.3 * 5017.2 * 58401.5 *
*****
    
```

EVCELV

PROELV

Damage category CAT1 identified as

EAST_OF_DYKE

TEST 7 - DYKING THE RED RIVER TO A HEIGHT OF 20FT

DAMAGE_REACH_ONE
(Damages are in \$1,000)

Damage Categories

```
*****
* Elevation* CAT1      * CAT2      * Total    *
*-----*-----*-----*-----*
* 705.00 * 0.0 * 0.0 * 0.0 *
* 709.00 * 0.0 * 0.0 * 0.0 *
* 713.00 * 0.0 * 0.0 * 0.0 *
* 717.00 * 0.0 * 0.0 * 0.0 *
* 721.00 * 0.0 * 0.0 * 0.0 *
* 725.00 * 0.0 * 0.0 * 0.0 *
*-----*-----*-----*-----*
* 725.40      0.0 * 0.0 * 0.0 *
*-----*-----*-----*-----*
* 729.00 * 70.8 * 0.0 * 70.8 *
* 733.00 * 95.1 * 0.0 * 95.1 *
* 737.00 * 124.8 * 0.0 * 124.8 *
* 741.00 * 172.2 * 3.4 * 175.7 *
* 745.00 * 364.6 * 20.8 * 385.4 *
* 749.00 * 598.2 * 41.8 * 640.0 *
* 753.00 * 961.7 * 75.5 * 1037.2 *
* 757.00 * 1435.3 * 148.8 * 1584.2 *
* 761.00 * 2787.4 * 303.8 * 3091.3 *
* 765.00 * 4487.8 * 526.2 * 5014.0 *
* 769.00 * 6649.8 * 823.2 * 7473.0 *
* 773.00 * 11374.9 * 1402.4 * 12777.3 *
* 777.00 * 23062.6 * 2398.9 * 25461.5 *
* 781.00 * 30688.3 * 3059.3 * 33747.6 *
* 785.00 * 38032.6 * 3652.4 * 41684.9 *
* 789.00 * 46591.5 * 4338.6 * 50930.1 *
* 793.00 * 52414.9 * 4732.4 * 57147.3 *
* 797.00 * 53588.9 * 4829.3 * 58418.2 *
* 801.00 * 54590.4 * 4912.5 * 59502.9 *
* 805.00 * 55411.4 * 4978.5 * 60389.8 *
* 809.00 * 55784.3 * 5008.1 * 60792.3 *
* 813.00 * 55787.1 * 5016.7 * 60803.8 *
* 817.00 * 55787.1 * 5017.2 * 60804.3 *
* 821.00 * 55787.1 * 5017.2 * 60804.3 *
* 825.00 * 55787.1 * 5017.2 * 60804.3 *
* 829.00 * 55787.1 * 5017.2 * 60804.3 *
* 833.00 * 55787.1 * 5017.2 * 60804.3 *
* 837.00 * 55787.1 * 5017.2 * 60804.3 *
* 841.00 * 55787.1 * 5017.2 * 60804.3 *
*****
```

PROELV

```
*****
Damage category CAT1 identified as EAST_OF_DYKE
Damage category CAT2 identified as WEST_OF_DYKE
Damage category OTHER identified as OTHER DAMAGE CATEGORIES
*****
```

TEST 8 - DYKING THE RED RIVER TO A HEIGHT OF 40FT

DAMAGE_REACH_ONE
(Damages are in \$1,000)

Damage Categories

```
*****
* Elevation* CAT1      * CAT2      * Total      *
*-----*-----*-----*-----*
* 705.00 * 0.0 * 0.0 * 0.0 *
* 709.00 * 0.0 * 0.0 * 0.0 *
* 713.00 * 0.0 * 0.0 * 0.0 *
* 717.00 * 0.0 * 0.0 * 0.0 *
* 721.00 * 0.0 * 0.0 * 0.0 *
* 725.00 * 0.0 * 0.0 * 0.0 *
* 729.00 * 0.0 * 0.0 * 0.0 *
* 733.00 * 0.0 * 0.0 * 0.0 *
* 737.00 * 0.0 * 0.0 * 0.0 *
* 741.00 * 0.0 * 3.4 * 3.4 *
* 745.00 * 0.0 * 20.8 * 20.8 *
*-----*-----*-----*-----*
* 745.40 * 0.0 * 22.0 * 22.0 *
*-----*-----*-----*-----*
* 749.00 * 598.2 * 41.8 * 640.0 *
* 753.00 * 961.7 * 75.5 * 1037.2 *
* 757.00 * 1435.3 * 148.8 * 1584.2 *
* 761.00 * 2787.4 * 303.8 * 3091.3 *
* 765.00 * 4487.8 * 526.2 * 5014.0 *
* 769.00 * 6649.8 * 823.2 * 7473.0 *
* 773.00 * 11374.9 * 1402.4 * 12777.3 *
* 777.00 * 23062.6 * 2398.9 * 25461.5 *
* 781.00 * 30688.3 * 3059.3 * 33747.6 *
* 785.00 * 38032.6 * 3652.4 * 41684.9 *
* 789.00 * 46591.5 * 4338.6 * 50930.1 *
* 793.00 * 52414.9 * 4732.4 * 57147.3 *
* 797.00 * 53588.9 * 4829.3 * 58418.2 *
* 801.00 * 54590.4 * 4912.5 * 59502.9 *
* 805.00 * 55411.4 * 4978.5 * 60389.8 *
* 809.00 * 55784.3 * 5008.1 * 60792.3 *
* 813.00 * 55787.1 * 5016.7 * 60803.8 *
* 817.00 * 55787.1 * 5017.2 * 60804.3 *
* 821.00 * 55787.1 * 5017.2 * 60804.3 *
* 825.00 * 55787.1 * 5017.2 * 60804.3 *
* 829.00 * 55787.1 * 5017.2 * 60804.3 *
* 833.00 * 55787.1 * 5017.2 * 60804.3 *
* 837.00 * 55787.1 * 5017.2 * 60804.3 *
* 841.00 * 55787.1 * 5017.2 * 60804.3 *
*****
```

PROELV

```
*****
Damage category CAT1 identified as EAST_OF_DYKE
Damage category CAT2 identified as WEST_OF_DYKE
Damage category OTHER identified as OTHER DAMAGE CATEGORIES
*****
```

APPENDIX D3:

**INPUT FILES FOR EAD
CONSULTATION.**

```

TT TEST 1 - DAMAGE FOR EXISTING CONDITIONS
J1 50 1992 1995 1992 3
J2 5
CN 2 CAT1 CAT2
PN 1 EXISTING CONDITIONS
DY 3 1950 1970 1974
RN 1 DAMAGE_REACH_ONE
FR 1 17 99 98 95 90 80 70 60
FR 50 40 30 20 10 5 2 1 0.5
FR 0.2
QF 1 5000 6000 8500 11200 15000 19000 23500
QF 28000 33000 40000 49000 62000 80000 100000 120000 140000
FR160000
SQ 1 16 708 712 716 720 724 728 732
SQ 736 740 744 748 752 756 760 764 768
QS 1 13000 15000 17000 19000 21000 24000 26000
QS 30000 35000 41000 50000 64000 80000 100000 140000 230000
ZR A=win B=1 C=DG E=1992 F=plan1
RC CAT1 1995 1.5
RC CAT2 1995 1.5
EJ 1

```



```

TT TEST 2 - DAMAGE FOR RAISING STRUCTURES 3FT
J1 50 1992 1995 1992 3
J2 5
CN 2 CAT1 CAT2
PN 1 RAISING STRUCTURES 3FT
DY 3 1950 1970 1974
RN 1 DAMAGE_REACH_ONE
FR 1 17 99 98 95 90 80 70 60
FR 50 40 30 20 10 5 2 1 0.5
FR 0.2
QF 1 5000 6000 8500 11200 15000 19000 23500
QF 28000 33000 40000 49000 62000 80000 100000 120000 140000
FR160000
SQ 1 16 708 712 716 720 724 728 732
SQ 736 740 744 748 752 756 760 764 768
QS 1 13000 15000 17000 19000 21000 24000 26000
QS 30000 35000 41000 50000 64000 80000 100000 140000 230000
ZR A=win B=1 C=DG E=1992 F=plan2
RC CAT1 1995 1.5
RC CAT2 1995 1.5
EJ 1

```

```

TT TEST 3 - DAMAGE FOR RAISING STRUCTURES 5FT
J1 50 1992 1995 1992 3
J2 5
CN 2 CAT1 CAT2
PN 1 RAISING STRUCTURES 5FT
DY 3 1950 1970 1974
RN 1 DAMAGE_REACH_ONE
FR 1 17 99 98 95 90 80 70 60
FR 50 40 30 20 10 5 2 1 0.5
FR 0.2
QF 1 5000 6000 8500 11200 15000 19000 23500
QF 28000 33000 40000 49000 62000 80000 100000 120000 140000
QF160000
SQ 1 16 708 712 716 720 724 728 732
SQ 736 740 744 748 752 756 760 764 768
QS 1 13000 15000 17000 19000 21000 24000 26000
QS 30000 35000 41000 50000 64000 80000 100000 140000 230000
ZR A=win B=1 C=DG E=1992 F=plan3
RC CAT1 1995 1.5
RC CAT2 1995 1.5
EJ 1

```

TT TEST 4 - FLOOD PROOFING TO A HEIGHT OF 3FT									
J1	50	1992	1995	1992	3				
J2	5								
CN	2	CAT1	CAT2						
PN	1	FLOOD PROOFING TO 3FT							
DY	3	1950	1970	1974					
RN	1	DAMAGE_REACH_ONE							
FR	1	17	99	98	95	90	80	70	60
FR	50	40	30	20	10	5	2	1	0.5
FR	0.2								
QF	1		5000	6000	8500	11200	15000	19000	23500
QF	28000	33000	40000	49000	62000	80000	100000	120000	140000
FR	160000								
SQ	1	16	708	712	716	720	724	728	732
SQ	736	740	744	748	752	756	760	764	768
QS	1		13000	15000	17000	19000	21000	24000	26000
QS	30000	35000	41000	50000	64000	80000	100000	140000	230000
SD	1	18	709	713	717	721	725	729	733
SD	737	741	745	749	753	757	761	765	769
SD	773	777							
DG	1		0	23.8	27.5	35.1	48.2	70.8	77.5
DG	124.5	149.2	331.9	497.0	837.9	1435.3	2677.8	4167.8	5752.2
DG	8555.0	23001.2							
RC		CAT1	1995	1.5					
RC		CAT2	1995	1.5					
EJ	1								

TT TEST 5 - FLOOD PROOFING TO A HEIGHT OF 5FT									
J1	50	1992	1995	1992	3				
J2	5								
CN	2	CAT1	CAT2						
PN	1	FLOOD PROOFING TO 5FT							
DY	3	1950	1970	1974					
RN	1	DAMAGE_REACH_ONE							
FR	1	17	99	98	95	90	80	70	60
FR	50	40	30	20	10	5	2	1	0.5
FR	0.2								
QF	1		5000	6000	8500	11200	15000	19000	23500
QF	28000	33000	40000	49000	62000	80000	100000	120000	140000
QF	160000								
SQ	1	16	708	712	716	720	724	728	732
SQ	736	740	744	748	752	756	760	764	768
QS	1		13000	15000	17000	19000	21000	24000	26000
QS	30000	35000	41000	50000	64000	80000	100000	140000	230000
SD	1	18	709	713	717	721	725	729	733
SD	737	741	745	749	753	757	761	765	769
SD	773	777							
DG	1		0	23.8	27.5	35.1	48.2	50.0	77.5
DG	128.4	149.2	179.7	497.0	837.9	1230.0	1757.6	3484.2	5752.2
DG	8555.0	16018.7							
RC		CAT1	1995	1.5					
RC		CAT2	1995	1.5					
EJ	1								

```

TT TEST 6 - RELOCATION OF STRUCTURES ABOVE 754.0FT LEVEL
J1 50 1992 1995 1992 3
J2 5
CN 2 CAT1 CAT2
PN 1 RELOCATION OF STRUCTURES
DY 3 1950 1970 1974
RN 1 DAMAGE_REACH_ONE
FR 1 17 99 98 95 90 80 70 60
FR 50 40 30 20 10 5 2 1 0.5
FR 0.2
QF 1 5000 6000 8500 11200 15000 19000 23500
QF 28000 33000 40000 49000 62000 80000 100000 120000 140000
QF160000
SQ 1 16 708 712 716 720 724 728 732
SQ 736 740 744 748 752 756 760 764 768
QS 1 13000 15000 17000 19000 21000 24000 26000
QS 30000 35000 41000 50000 64000 80000 100000 140000 230000
ZR A=win B=1 C=DG E=1992 F=plan6
RC CAT1 1995 1.5
RC CAT2 1995 1.5
EJ 1

```

TT TEST 7 - DYKING THE RED RIVER TO A HEIGHT OF 20FT									
J1	50	1992	1995	1992	3				
J2	5								
CN	2	CAT1	CAT2						
PN	1	DYKING THE RED RIVER TO 725.4FT							
DY	3	1950	1970	1974					
RN	1	DAMAGE_REACH_ONE							
FR	1	17	99	98	95	90	80	70	60
FR	50	40	30	20	10	5	2	1	0.5
FR	0.2								
QF	1		5000	6000	8500	11200	15000	19000	23500
QF	28000	33000	40000	49000	62000	80000	100000	120000	140000
FR	160000								
SQ	1	16	708	712	716	720	724	728	732
SQ	736	740	744	748	752	756	760	764	768
QS	1		13000	15000	17000	19000	21000	24000	26000
QS	30000	35000	41000	50000	64000	80000	100000	140000	230000
SD	1	18	709	713	717	721	725	729	733
SD	737	741	745	749	753	757	761	765	769
SD	773	777							
DG	1		0	0	0	0	0	70.8	95.1
DG	124.8	172.2	364.6	598.2	961.7	1435.3	2787.4	4487.8	6649.8
DG	11374.	23062.6							
RC		CAT1	1995	1.5					
RC		CAT2	1995	1.5					
EJ	1								

APPENDIX D4:

**OUTPUT FILES FOR EAD
CONSULTATION.**

```

*****
*      Expected Annual Flood Damage Program      *
*      Users Manual (March 1989)                *
*      Version 2.0.01; June 1991                *
*      Sun Unix                                  *
*      Run date 14APR92   time 11:36:56         *
*****

```

```

EEEEEEEE      AA      DDDDDDDD
E              AA  AA  DD      DD
E              AA   AA  DD      DD
EEEEEE        AA      AA  DD      DD
E              AAAAAAAAAA DD      DD
E              AA      AA  DD      DD
EEEEEEEE      AA      AA  DDDDDDDD

```

```

*****
* U.S. Army Corps of Engineers *
* The Hydrologic Engineering Center *
* 609 Second Street, Suite B *
* Davis, California 95616 *
* (916) 756-1104 *
*****

```

```

+++++
+ Expected Annual Flood Damage Computation +
+ 761-X6-L7580 Sun Unix +
+ Version Date June 6, 1991 +
+++++

```


TEST 1 - DAMAGE FOR EXISTING CONDITIONS

** EXPECTED ANNUAL FLOOD DAMAGE **

** FOR REACH 1 = 1 DAMAGE_REACH_ONE

** WITH PLAN 1 = EXISTING CONDITIONS

** INPUT DATA YEARS = 1950 1970 1974

** PERIOD OF ANALYSIS = 50 YEARS

** DISCOUNT RATE = 5.0000 PERCENT

** DAMAGE BASE = 1992 DOLLARS

DAMAGE CATEGORIES	STUDY YEAR	BASE YEAR DECADE YEARS			
	1992	1995	10 2004	20 2014	30 2024	40 2034
1 CAT1	326.04	340.94	389.83	452.41	525.04	609.33
2 CAT2	0.00	0.00	0.00	0.00	0.00	0.00
TOTAL	326.04	340.94	389.83	452.41	525.04	609.33

.....	END OF PERIOD	EQUIVALENT ANNUAL DAMAGE HISTORIC EVENTS		
50 2044	2044		1950	1970	1974
707.15	707.15	435.63	172.86	233.87	
0.00	0.00	0.00	0.00	0.00	0.00
707.15	707.15	435.63	172.86	233.87	248.44

TEST 2 - DAMAGE FOR RAISING STRUCTURES 3FT

** EXPECTED ANNUAL FLOOD DAMAGE **
 ** FOR REACH 1 = 1 DAMAGE_REACH_ONE
 ** WITH PLAN 1 = RAISING STRUCTURES 3FT
 ** INPUT DATA YEARS = 1950 1970 1974
 ** PERIOD OF ANALYSIS = 50 YEARS
 ** DISCOUNT RATE = 5.0000 PERCENT
 ** DAMAGE BASE = 1992 DOLLARS

DAMAGE CATEGORIES	STUDY YEAR	BASE YEAR DECADE YEARS			
	1992	1995	10 2004	20 2014	30 2024	40 2034
1 CAT1	225.20	235.48	269.25	312.47	362.64	420.86
2 CAT2	0.00	0.00	0.00	0.00	0.00	0.00
TOTAL	225.20	235.48	269.25	312.47	362.64	420.86

.....	END OF PERIOD	EQUIVALENT ANNUAL DAMAGE HISTORIC EVENTS		
50 2044	2044		1950	1970	1974
488.42	488.42	300.88	119.39	161.53	171.60
0.00	0.00	0.00	0.00	0.00	0.00
488.42	488.42	300.88	119.39	161.53	171.60

TEST 3 - DAMAGE FOR RAISING STRUCTURES 5FT

** EXPECTED ANNUAL FLOOD DAMAGE **
 ** FOR REACH 1 = 1 DAMAGE_REACH_ONE
 ** WITH PLAN 1 = RAISING STRUCTURES 5FT
 ** INPUT DATA YEARS = 1950 1970 1974
 ** PERIOD OF ANALYSIS = 50 YEARS
 ** DISCOUNT RATE = 5.0000 PERCENT
 ** DAMAGE BASE = 1992 DOLLARS

DAMAGE CATEGORIES	STUDY YEAR	BASE YEAR DECADE YEARS			
	1992	1995	10 2004	20 2014	30 2024	40 2034
1 CAT1	174.32	182.28	208.42	241.88	280.71	325.77
2 CAT2	0.00	0.00	0.00	0.00	0.00	0.00
TOTAL	174.32	182.28	208.42	241.88	280.71	325.77

.....	END OF PERIOD	EQUIVALENT ANNUAL DAMAGE HISTORIC EVENTS		
50 2044	2044		1950	1970	1974
378.07	378.07	232.91	92.42	125.04	132.83
0.00	0.00	0.00	0.00	0.00	0.00
378.07	378.07	232.91	92.42	125.04	132.83

TEST 4 - FLOOD PROOFING TO A HEIGHT OF 3FT

** EXPECTED ANNUAL FLOOD DAMAGE **
 ** FOR REACH 1 = 1 DAMAGE_REACH_ONE
 ** WITH PLAN 1 = FLOOD PROOFING TO 3FT
 ** INPUT DATA YEARS = 1950 1970 1974
 ** PERIOD OF ANALYSIS = 50 YEARS
 ** DISCOUNT RATE = 5.0000 PERCENT
 ** DAMAGE BASE = 1992 DOLLARS

DAMAGE CATEGORIES	STUDY YEAR	BASE YEAR DECADE YEARS			
	1992	1995	10 2004	20 2014	30 2024	40 2034
1 CAT1	296.77	310.33	354.82	411.79	477.89	554.62
2 CAT2	0.00	0.00	0.00	0.00	0.00	0.00
TOTAL	296.77	310.33	354.82	411.79	477.89	554.62

.....	END OF PERIOD	EQUIVALENT ANNUAL DAMAGE HISTORIC EVENTS		
50 2044	2044		1950	1970	1974
643.65	643.65	396.51	157.34	212.87	226.14
0.00	0.00	0.00	0.00	0.00	0.00
643.65	643.65	396.51	157.34	212.87	226.14

TEST 5 - FLOOD PROOFING TO A HEIGHT OF 5FT

** EXPECTED ANNUAL FLOOD DAMAGE **
 ** FOR REACH 1 = 1 DAMAGE_REACH_ONE
 ** WITH PLAN 1 = FLOOD PROOFING TO 5FT
 ** INPUT DATA YEARS = 1950 1970 1974
 ** PERIOD OF ANALYSIS = 50 YEARS
 ** DISCOUNT RATE = 5.0000 PERCENT
 ** DAMAGE BASE = 1992 DOLLARS

DAMAGE CATEGORIES	STUDY YEAR	BASE YEAR DECADE YEARS			
	1992	1995	10 2004	20 2014	30 2024	40 2034
1 CAT1	252.05	263.56	301.35	349.73	405.87	471.03
2 CAT2	0.00	0.00	0.00	0.00	0.00	0.00
TOTAL	252.05	263.56	301.35	349.73	405.87	471.03

.....	END OF PERIOD	EQUIVALENT ANNUAL DAMAGE HISTORIC EVENTS		
50 2044	2044		1950	1970	1974
546.65	546.65	336.76	133.63	180.79	192.06
0.00	0.00	0.00	0.00	0.00	0.00
546.65	546.65	336.76	133.63	180.79	192.06

TEST 6 - RELOCATION OF STRUCTURES ABOVE 754.0FT LEVEL

** EXPECTED ANNUAL FLOOD DAMAGE **

** FOR REACH 1 = 1 DAMAGE_REACH_ONE

** WITH PLAN 1 = RELOCATION OF STRUCTURES

** INPUT DATA YEARS = 1950 1970 1974

** PERIOD OF ANALYSIS = 50 YEARS

** DISCOUNT RATE = 5.0000 PERCENT

** DAMAGE BASE = 1992 DOLLARS

DAMAGE CATEGORIES	STUDY YEAR	BASE YEAR DECADE YEARS			
	1992	1995	10 2004	20 2014	30 2024	40 2034
1 CAT1	37.39	39.10	44.70	51.88	60.21	69.87
2 CAT2	0.00	0.00	0.00	0.00	0.00	0.00
TOTAL	37.39	39.10	44.70	51.88	60.21	69.87

.....	END OF PERIOD	EQUIVALENT ANNUAL DAMAGE HISTORIC EVENTS		
50 2044	2044		1950	1970	1974
81.09	81.09	49.96	19.82	26.82	28.49
0.00	0.00	0.00	0.00	0.00	0.00
81.09	81.09	49.96	19.82	26.82	28.49

TEST 7 - DYKING THE RED RIVER TO A HEIGHT OF 20FT

** EXPECTED ANNUAL FLOOD DAMAGE **

** FOR REACH 1 = 1 DAMAGE_REACH_ONE

** WITH PLAN 1 = DYKING THE RED RIVER TO 725.4FT

** INPUT DATA YEARS = 1950 1970 1974

** PERIOD OF ANALYSIS = 50 YEARS

** DISCOUNT RATE = 5.0000 PERCENT

** DAMAGE BASE = 1992 DOLLARS

DAMAGE CATEGORIES	STUDY YEAR	BASE YEAR DECADE YEARS			
	1992	1995	10 2004	20 2014	30 2024	40 2034
1 CAT1	317.32	331.81	379.39	440.30	510.99	593.02
2 CAT2	0.00	0.00	0.00	0.00	0.00	0.00
TOTAL	317.32	331.81	379.39	440.30	510.99	593.02

.....	END OF PERIOD	EQUIVALENT ANNUAL DAMAGE HISTORIC EVENTS		
50 2044	2044		1950	1970	1974
688.23	688.23	423.97	168.24	227.61	241.79
0.00	0.00	0.00	0.00	0.00	0.00
688.23	688.23	423.97	168.24	227.61	241.79

TEST 8 - DYKING THE RED RIVER TO A HEIGHT OF 40FT

** EXPECTED ANNUAL FLOOD DAMAGE **

** FOR REACH 1 = 1 DAMAGE_REACH_ONE

** WITH PLAN 1 = DYKING THE RED RIVER TO 745.4FT

** INPUT DATA YEARS = 1950 1970 1974

** PERIOD OF ANALYSIS = 50 YEARS

** DISCOUNT RATE = 5.0000 PERCENT

** DAMAGE BASE = 1992 DOLLARS

DAMAGE CATEGORIES	STUDY YEAR	BASE YEAR	DECADE YEARS			
	1992	1995	10 2004	20 2014	30 2024	40 2034
1 CAT1	245.62	256.84	293.67	340.81	395.53	459.02
2 CAT2	0.00	0.00	0.00	0.00	0.00	0.00
TOTAL	245.62	256.84	293.67	340.81	395.53	459.02

END OF PERIOD	EQUIVALENT ANNUAL DAMAGE	HISTORIC EVENTS		
		1950	1970	1974
50 2044	532.72 328.17	130.22 0.00	176.18 0.00	187.16 0.00
532.72	532.72	130.22	176.18	187.16

APPENDIX E:

**STRUCTURE INVENTORY
LISTINGS**

KODE1	IDRCH	IBDLG	ROMN	COLG	ADJ	STOPO	DELTZ	KODE1	IDRCH	IBDLG	ROMN	COLG	ADJ	STOPO	DELTZ
SL	1	104	5502147	634747	771	771	0	SL	1	155	5502944	636141	771	771	0
SL	1	105	5502180	635252	771	771	0	SL	1	156	5502639	636474	761	771	0
SL	1	106	5502252	635263	761	761	0	SL	1	157	5502651	636586	761	761	0
SL	1	107	5502252	635312	761	761	0	SL	1	158	5502713	636575	755	755	0
SL	1	108	5502186	635334	768	771	0	SL	1	159	5502752	636530	755	755	0
SL	1	109	5502098	635279	771	771	0	SL	1	160	5502803	636541	755	755	0
SL	1	110	5502104	635312	771	771	0	SL	1	161	5502848	636519	755	755	0
SL	1	111	5502093	635361	768	768	0	SL	1	162	5502899	636519	755	755	0
SL	1	112	5502542	634796	771	771	0	SL	1	163	5502950	636333	768	768	0
SL	1	113	5502257	635050	761	761	0	SL	1	164	5503034	636333	755	755	0
SL	1	114	5502312	636069	761	761	0	SL	1	165	5503034	636276	771	771	0
SL	1	115	5501643	635789	768	768	0	SL	1	166	5502989	636310	771	771	0
SL	1	116	5501835	636700	755	755	0	SL	1	167	5502978	636338	768	768	0
SL	1	117	5501884	636694	761	761	0	SL	1	168	5502775	636592	755	755	0
SL	1	118	5501418	636788	768	768	0	SL	1	169	5502938	636806	771	771	0
SL	1	119	5501401	636837	768	768	0	SL	1	170	5503029	636801	768	768	0
SL	1	120	5501451	636815	768	768	0	SL	1	171	5503034	636699	758	758	0
SL	1	121	5501451	636864	764	764	0	SL	1	172	5503362	636192	768	768	0
SL	1	122	5501484	636881	761	761	0	SL	1	173	5503401	636186	771	771	0
SL	1	123	5501555	636892	771	771	0	SL	1	174	5503452	636175	771	771	0
SL	1	124	5502378	636437	764	764	0	SL	1	175	5503345	636310	768	768	0
SL	1	125	5502345	636420	764	764	0	SL	1	176	5503395	636299	768	768	0
SL	1	126	5502290	636420	764	764	0	SL	1	177	5503390	636338	768	768	0
SL	1	127	5502328	636557	758	758	0	SL	1	178	5503446	636293	771	771	0
SL	1	128	5502252	636541	758	758	0	SL	1	179	5503412	636304	768	768	0
SL	1	129	5502246	636612	755	755	0	SL	1	180	5503474	636270	768	768	0
SL	1	130	5502482	636601	761	761	0	SL	1	181	5503497	636259	768	768	0
SL	1	131	5502433	636678	758	758	0	SL	1	182	5503542	636248	768	768	0
SL	1	132	5502477	636689	755	755	0	SL	1	183	5503531	636180	768	768	0
SL	1	133	5502449	636760	755	755	0	SL	1	184	5503570	636180	768	768	0
SL	1	134	5502317	636738	758	758	0	SL	1	185	5503627	636158	768	768	0
SL	1	135	5502317	636799	758	758	0	SL	1	186	5503723	635988	751	751	0
SL	1	136	5502285	636782	761	761	0	SL	1	187	5503260	635926	771	771	0
SL	1	137	5502169	636875	761	761	0	SL	1	188	5504066	635390	768	768	0
SL	1	138	5502093	636882	755	755	0	SL	1	189	5504087	635419	771	771	0
SL	1	139	5502093	636882	755	755	0	SL	1	190	5504124	635415	771	771	0
SL	1	140	5500655	636885	758	758	0	SL	1	191	5504179	635441	768	768	0
SL	1	141	5502583	635176	764	764	0	SL	1	192	5504211	635532	771	771	0
SL	1	142	5502668	635170	755	755	0	SL	1	193	5504324	635342	771	771	0
SL	1	143	5502724	635182	748	748	0	SL	1	194	5504343	635386	768	768	0
SL	1	144	5502769	635176	748	748	0	SL	1	195	5504357	635357	771	771	0
SL	1	145	5502758	635119	764	764	0	SL	1	196	5504390	635357	768	768	0
SL	1	146	5502826	635114	768	768	0	SL	1	197	5504554	635353	768	768	0
SL	1	147	5503469	634967	768	768	0	SL	1	198	5504601	635342	768	768	0
SL	1	148	5503395	634984	771	771	0	SL	1	199	5504529	635707	774	774	0
SL	1	149	5503362	635283	771	771	0	SL	1	200	5504539	635736	778	778	0
SL	1	150	5503418	635263	764	764	0	SL	1	201	5504558	635780	781	781	0
SL	1	151	5503333	635257	768	768	0	SL	1	202	5504554	635849	778	778	0
SL	1	152	5503102	635229	768	768	0	SL	1	203	5504477	635944	771	771	0
SL	1	153	5503023	636118	768	768	0	SL	1	204	5504543	635951	771	771	0
SL	1	154	5502944	636101	771	771	0	SL	1	205	5504539	635969	771	771	0
SL	1	155	5502944	636101	771	771	0	SL	1	206	5504532	635995	771	771	0
SL	1	156	5502944	636101	771	771	0	SL	1	207	5504423	635966	764	764	0
SL	1	157	5502944	636101	771	771	0	SL	1	208	5504434	635988	764	764	0

SL	1	209	5504441	636924	771	771	0	SL	1	260	5503661	636370	771	771	0	
KODE1	IDRCH	1	IDBLG	ROWN	COLG	ADJ	STOPO	DELTZ	SL	1	261	5503679	636370	771	771	0
SL	1	210	5504401	636057	771	771	0	SL	1	263	5503664	636372	771	771	0	
SL	1	211	5504284	636020	771	764	0	SL	1	264	5503657	636454	764	764	0	
SL	1	212	5504284	636050	771	764	0	SL	1	265	5503639	636509	764	764	0	
SL	1	213	5504259	636057	771	764	0	SL	1	266	5503668	636516	768	768	0	
SL	1	214	5504248	636086	768	768	0	SL	1	267	5503708	636472	768	768	0	
SL	1	215	5503931	636035	741	741	0	SL	1	268	5503701	636516	768	768	0	
SL	1	216	5503854	635962	728	728	0	SL	1	269	5503734	636465	768	768	0	
SL	1	217	5503821	635973	728	728	0	SL	1	270	5503759	636465	768	768	0	
SL	1	218	5503836	636174	768	768	0	SL	1	271	5503726	636385	771	771	0	
SL	1	219	5503995	636177	771	771	0	SL	1	272	5503752	636396	771	771	0	
SL	1	220	5503562	636308	771	771	0	SL	1	273	5503774	636385	771	771	0	
KODE1	IDRCH	1	IDBLG	ROWN	COLG	ADJ	STOPO	DELTZ	SL	1	274	5503810	636392	771	771	0
SL	1	221	5503533	636334	771	771	0	SL	1	275	5503836	636392	768	768	0	
SL	1	222	5503530	636359	768	768	0	SL	1	276	5503854	636345	768	768	0	
SL	1	223	5503519	636385	768	768	0	SL	1	277	5503858	636403	771	771	0	
SL	1	224	5503515	636407	764	764	0	SL	1	278	5503880	636410	771	771	0	
SL	1	225	5503519	636432	764	764	0	SL	1	279	5503810	636462	768	768	0	
SL	1	226	5503541	636454	764	764	0	SL	1	280	5503832	636462	768	768	0	
SL	1	227	5503588	636494	764	764	0	SL	1	281	5503858	636454	771	771	0	
SL	1	228	5503610	636505	764	764	0	SL	1	282	5503883	636454	771	771	0	
SL	1	229	5503592	636425	764	764	0	SL	1	283	5503814	636505	771	771	0	
SL	1	230	5503577	636407	764	764	0	SL	1	284	5503839	636513	768	768	0	
SL	1	231	5503584	636374	768	768	0	SL	1	285	5503887	636516	771	771	0	
KODE1	IDRCH	1	IDBLG	ROWN	COLG	ADJ	STOPO	DELTZ	SL	1	286	5503912	636290	771	771	0
SL	1	232	5503610	636367	768	768	0	SL	1	287	5503887	636225	768	768	0	
SL	1	233	5503639	636367	771	771	0	SL	1	288	5503912	636225	771	771	0	
SL	1	234	5503621	636305	771	771	0	SL	1	289	5503938	636217	771	771	0	
SL	1	235	5503617	636250	771	771	0	SL	1	290	5503956	636228	768	768	0	
SL	1	236	5503580	636312	771	771	0	SL	1	291	5503974	636228	768	768	0	
SL	1	237	5503683	636319	768	768	0	SL	1	292	5504011	636228	771	771	0	
SL	1	238	5503646	636254	771	771	0	SL	1	293	5503971	636312	768	768	0	
SL	1	239	5503679	636254	771	771	0	SL	1	294	5503916	636359	768	768	0	
SL	1	240	5503661	636199	771	771	0	SL	1	295	5503923	636389	768	768	0	
SL	1	241	5503679	636188	771	771	0	SL	1	296	5503931	636414	771	771	0	
SL	1	242	5503705	636199	771	771	0	SL	1	297	5503923	636454	768	768	0	
KODE1	IDRCH	1	IDBLG	ROWN	COLG	ADJ	STOPO	DELTZ	SL	1	298	5503923	636472	771	771	0
SL	1	243	5503726	636210	768	768	0	SL	1	299	5503923	636498	768	768	0	
SL	1	244	5503745	636206	768	768	0	SL	1	300	5503752	636556	764	764	0	
SL	1	245	5503770	636195	768	768	0	SL	1	301	5503865	636542	768	768	0	
SL	1	246	5503792	636206	771	771	0	SL	1	302	5503883	636549	771	771	0	
SL	1	247	5503778	636272	768	768	0	SL	1	303	5503920	636545	771	771	0	
SL	1	248	5503818	636214	771	771	0	SL	1	304	5503949	636542	771	771	0	
SL	1	249	5503843	636221	771	771	0	SL	1	305	5503920	636520	768	768	0	
SL	1	250	5503869	636214	771	771	0	SL	1	306	5503931	636593	768	768	0	
SL	1	251	5503814	636279	768	768	0	SL	1	307	5503887	636593	768	768	0	
SL	1	252	5503847	636279	771	771	0	SL	1	308	5503821	636560	771	771	0	
SL	1	253	5503825	636323	768	768	0	SL	1	309	5503825	636582	768	768	0	
KODE1	IDRCH	1	IDBLG	ROWN	COLG	ADJ	STOPO	DELTZ	SL	1	310	5503836	636604	768	768	0
SL	1	254	5503737	636330	768	768	0	SL	1	311	5503836	636604	768	768	0	
SL	1	255	5503763	636334	771	771	0	SL	1	312	5503836	636604	768	768	0	
SL	1	256	5503781	636341	771	771	0	SL	1	313	5503836	636604	768	768	0	
SL	1	257	5503708	636327	771	771	0	SL	1	314	5503836	636604	768	768	0	
SL	1	258	5503737	636254	768	768	0	SL	1	315	5503836	636604	768	768	0	
SL	1	259	5503712	636257	771	771	0	SL	1	316	5503836	636604	768	768	0	

SL	1	416	5504580	636527	771	771	0	SL	1	467	5504620	636276	771	771	0
SL	1	417	5504605	636520	768	768	0	SL	1	468	5504609	636254	771	771	0
SL	1	418	5504623	636509	768	768	0	SL	1	469	5504605	636225	771	771	0
KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ	SL	1	470	5504550	636567	768	768	0
SL	1	419	5504445	636458	768	768	0	SL	1	471	5504580	636582	771	771	0
SL	1	420	5504463	636458	771	771	0	SL	1	472	5504605	636571	768	768	0
SL	1	421	5504492	636462	771	771	0	SL	1	473	5504638	636589	771	771	0
SL	1	422	5504532	636458	771	771	0	KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	1	423	5504569	636462	771	771	0	SL	1	474	5504616	636702	771	771	0
SL	1	424	5504587	636454	768	768	0	SL	1	475	5504652	636720	768	768	0
SL	1	425	5504612	636462	768	768	0	SL	1	476	5504609	635940	771	771	0
SL	1	426	5504481	636035	771	771	0	SL	1	477	5504638	635962	771	771	0
SL	1	427	5504488	636071	768	768	0	SL	1	478	5504656	636002	768	768	0
SL	1	428	5504467	636075	771	771	0	SL	1	479	5504663	635966	771	771	0
SL	1	429	5504459	636141	771	771	0	SL	1	480	5504663	635940	771	771	0
KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ	SL	1	481	5504663	636082	768	768	0
SL	1	430	5504459	636188	771	771	0	SL	1	482	5504663	636115	768	768	0
SL	1	431	5504477	636221	771	771	0	SL	1	483	5504663	636133	771	771	0
SL	1	432	5504485	636250	771	771	0	SL	1	484	5504656	636159	771	771	0
SL	1	433	5504503	636272	771	771	0	KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	1	434	5504503	636297	771	771	0	SL	1	485	5504656	636210	768	768	0
SL	1	435	5504503	636319	768	768	0	SL	1	486	5504663	636243	768	768	0
SL	1	436	5504518	636400	768	768	0	SL	1	487	5504671	636290	771	771	0
SL	1	437	5504507	636144	771	771	0	SL	1	488	5504663	636316	771	771	0
SL	1	438	5504525	636126	768	768	0	SL	1	489	5504663	636334	771	771	0
SL	1	439	5504532	636024	768	768	0	SL	1	490	5504663	636356	771	771	0
SL	1	440	5504536	636046	771	771	0	SL	1	491	5504667	636385	771	771	0
KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ	SL	1	492	5504663	636429	768	768	0
SL	1	441	5504565	636031	768	768	0	SL	1	493	5504671	636451	771	771	0
SL	1	442	5504587	636031	768	768	0	SL	1	494	5504671	636472	771	771	0
SL	1	443	5504598	636097	771	771	0	SL	1	495	5504667	636498	771	771	0
SL	1	444	5504565	636112	768	768	0	KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	1	445	5504507	636199	771	771	0	SL	1	496	5504667	636516	768	768	0
SL	1	446	5504525	636188	768	768	0	SL	1	497	5504663	636545	771	771	0
SL	1	447	5504543	636170	771	771	0	SL	1	498	5504693	636578	771	771	0
SL	1	448	5504565	636174	771	771	0	SL	1	499	5504689	636133	768	768	0
SL	1	449	5504587	636166	771	771	0	SL	1	500	5504689	636177	768	768	0
SL	1	450	5504612	636163	771	771	0	SL	1	501	5504747	636108	768	768	0
SL	1	451	5504547	636232	771	771	0	SL	1	502	5504773	636115	764	764	0
KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ	SL	1	503	5504773	636082	764	764	0
SL	1	452	5504554	636254	771	771	0	SL	1	504	5504784	636060	761	761	0
SL	1	453	5504550	636279	768	768	0	SL	1	505	5504827	636837	771	771	0
SL	1	454	5504558	636305	771	771	0	SL	1	506	5504911	636115	751	751	0
SL	1	455	5504576	636319	771	771	0	KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	1	456	5504576	636294	771	771	0	SL	1	507	5504919	636071	751	751	0
SL	1	457	5504547	636327	771	771	0	SL	1	508	5504966	636101	755	755	0
SL	1	458	5504547	636356	771	771	0	SL	1	509	5505156	636148	771	771	0
SL	1	459	5504561	636392	771	771	0	SL	1	510	5505181	636126	768	768	0
SL	1	460	5504565	636418	771	771	0	SL	1	511	5505188	636155	771	771	0
SL	1	461	5504594	636410	768	768	0	SL	1	512	5505516	636075	761	761	0
SL	1	462	5504612	636410	771	771	0	SL	1	513	5505473	636079	771	771	0
KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ	SL	1	514	5505393	636093	761	761	0
SL	1	463	5504620	636392	771	771	0	SL	1	515	5505349	636159	771	771	0
SL	1	464	5504620	636348	771	771	0	SL	1	516	5505356	636225	768	768	0
SL	1	465	5504620	636323	771	771	0	SL	1	517	5505389	636195	771	771	0
SL	1	466	5504620	636301	771	771	0	KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTZ

SL	I	518	5505389	636217	771	771	0
SL	I	519	5505575	636319	771	771	0
SL	I	520	5506956	634094	771	771	0
SL	I	521	5507000	634065	768	768	0
SL	I	522	5507020	634089	771	771	0
SL	I	523	5507029	634114	768	768	0
SL	I	524	5506981	634128	771	771	0
SL	I	525	5506835	634463	758	758	0
SL	I	526	5506874	634473	755	755	0
SL	I	527	5507102	634585	758	758	0
SL	I	528	5507146	634454	758	758	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	529	5507122	634473	755	755	0
SL	I	530	5507170	634488	755	755	0
SL	I	531	5507156	634517	755	755	0
SL	I	532	5507335	634434	771	771	0
SL	I	533	5507335	634483	768	768	0
SL	I	534	5507384	634536	771	771	0
SL	I	535	5507418	634556	768	768	0
SL	I	536	5507452	634575	768	768	0
SL	I	537	5507476	634458	771	771	0
SL	I	538	5507491	634488	771	771	0
SL	I	539	5507501	634420	771	771	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	540	5507622	634493	768	768	0
SL	I	541	5507219	634998	755	755	0
SL	I	542	5507267	635022	771	771	0
SL	I	543	5507326	635046	771	771	0
SL	I	544	5507233	635037	764	764	0
SL	I	545	5507253	635129	784	784	0
SL	I	546	5507190	635134	784	784	0
SL	I	547	5507156	635114	787	787	0
SL	I	548	5507097	635221	764	764	0
SL	I	549	5507068	635236	771	771	0
SL	I	550	5507034	635236	787	787	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	551	5506990	635309	778	778	0
SL	I	552	5506952	635343	781	781	0
SL	I	553	5506927	635382	787	787	0
SL	I	554	5506845	635187	778	778	0
SL	I	555	5506864	635474	771	771	0
SL	I	556	5506835	635537	768	768	0
SL	I	557	5506879	635523	768	768	0
SL	I	558	5506879	635542	768	768	0
SL	I	559	5506879	635586	768	768	0
SL	I	560	5506641	635955	768	768	0
SL	I	561	5506592	635960	771	771	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	562	5506558	636004	768	768	0
SL	I	563	5506485	636004	768	768	0
SL	I	564	5506495	636038	768	768	0
SL	I	565	5506471	636115	764	764	0
SL	I	566	5506660	636101	771	771	0
SL	I	567	5506854	636076	764	764	0
SL	I	568	5506893	636028	768	768	0
SL	I	569	5505844	636183	768	768	0
SL	I	570	5505941	636237	781	781	0
SL	I	571	5505960	636276	771	771	0

SL	I	572	5505912	636300	771	771	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	573	5505834	636227	768	768	0
SL	I	574	5505810	636290	771	771	0
SL	I	575	5505698	636329	771	771	0
SL	I	576	5505718	636358	771	771	0
SL	I	577	5505786	636382	768	768	0
SL	I	578	5505820	636412	768	768	0
SL	I	579	5505815	636450	771	771	0
SL	I	580	5505781	636441	771	771	0
SL	I	581	5505805	636504	768	768	0
SL	I	582	5505951	636533	771	771	0
SL	I	583	5506087	636514	768	768	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	584	5506145	636509	758	758	0
SL	I	585	5506145	636538	761	761	0
SL	I	586	5506203	636669	764	764	0
SL	I	587	5506213	636698	768	768	0
SL	I	588	5506140	636800	771	771	0
SL	I	589	5506135	636820	771	771	0
SL	I	590	5506169	636800	771	771	0
SL	I	591	5506203	636805	771	771	0
SL	I	592	5506354	636791	764	764	0
SL	I	593	5507000	636004	761	761	0
SL	I	594	5507000	636047	758	758	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	595	5506786	636723	738	738	0
SL	I	596	5506850	636791	745	745	0
SL	I	597	5506884	636805	745	745	0
SL	I	598	5506981	636810	745	745	0
SL	I	599	5507209	636504	761	761	0
SL	I	600	5507258	636504	764	764	0
SL	I	601	5507501	635231	768	768	0
SL	I	602	5507501	635032	764	764	0
SL	I	603	5507544	634939	768	768	0
SL	I	604	5507564	634993	778	778	0
SL	I	605	5507598	634978	778	778	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	606	5507617	635105	781	781	0
SL	I	607	5507646	635148	771	771	0
SL	I	608	5507676	635119	781	781	0
SL	I	609	5507690	635173	771	771	0
SL	I	610	5508322	636786	722	722	0
SL	I	611	5508356	636553	738	738	0
SL	I	612	5508331	636543	738	738	0
SL	I	613	5508200	636441	738	738	0
SL	I	614	5508113	636285	758	758	0
SL	I	615	5508089	636276	764	764	0
SL	I	616	5507909	636174	748	748	0
KODE1	IDRCH	IBDLG	ROWN	COLE	ADJ	STOPO	DELTZ
SL	I	617	5507923	636013	764	764	0
SL	I	618	5507855	635440	768	768	0
SL	I	619	5507855	635479	768	768	0
SL	I	620	5507923	635484	768	768	0
SL	I	621	5507729	635192	774	774	0
SL	I	622	5507739	635226	771	771	0

SL	1	830	5511642	635146	771	771	0
SL	1	831	5511654	635108	768	768	0
SL	1	832	5511824	635309	768	768	0
SL	1	833	5511974	635397	771	771	0
SL	1	834	5511635	634750	761	761	0
SL	1	835	5512068	635466	768	768	0
SL	1	836	5512081	635516	771	771	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
SL	1	837	5512125	635528	771	771	0
SL	1	838	5512156	635497	771	771	0
SL	1	839	5512326	635585	768	768	0
SL	1	840	5512301	635616	771	771	0
SL	1	841	5511447	634650	761	761	0
SL	1	842	5511478	634631	764	764	0
SL	1	843	5511491	634323	771	771	0
SL	1	844	5511548	634600	764	764	0
SL	1	845	5511541	634643	761	761	0
SL	1	846	5511617	634600	768	768	0
SL	1	847	5511591	634637	764	764	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
SL	1	848	5511667	634618	774	774	0
SL	1	849	5511673	634650	771	771	0
SL	1	850	5511730	634731	764	764	0
SL	1	851	5511755	634643	784	784	0
SL	1	852	5511780	634738	768	768	0
SL	1	853	5511805	634618	784	784	0
SL	1	854	5511836	634706	778	778	0
SL	1	855	5511868	634700	781	781	0
SL	1	856	5511843	634562	787	787	0
SL	1	857	5511899	634562	787	787	0
SL	1	858	5511974	634669	774	774	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
SL	1	859	5511811	633759	784	784	0
SL	1	860	5511773	633840	787	787	0
SL	1	861	5511799	633884	784	784	0
SL	1	862	5511698	633997	784	784	0
SL	1	863	5511635	633959	784	784	0
SL	1	864	5511623	634028	784	784	0
SL	1	865	5511585	633991	787	787	0
SL	1	866	5511912	634198	771	771	0
SL	1	867	5511962	634217	774	774	0
SL	1	868	5512012	634204	784	784	0
SL	1	869	5512062	634323	784	784	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
SL	1	870	5511999	634480	787	787	0
SL	1	871	5512062	634625	771	771	0
SL	1	872	5512119	634606	774	774	0
SL	1	873	5512125	634562	784	784	0
SL	1	874	5512207	634562	771	771	0
SL	1	875	5512200	634468	787	787	0
SL	1	876	5512514	635710	771	771	0
SL	1	877	5512533	635798	768	768	0
SL	1	878	5512564	635773	768	768	0
SL	1	879	5512589	635836	771	771	0
SL	1	880	5512627	635936	771	771	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
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SL	1	881	5512627	636005	768	768	0
SL	1	882	5512589	636037	771	771	0
SL	1	883	5512671	635805	768	768	0
SL	1	884	5512715	635798	771	771	0
SL	1	885	5512715	635861	768	768	0
SL	1	886	5512803	635817	768	768	0
SL	1	887	5512866	635861	771	771	0
SL	1	888	5501702	636940	761	761	0
SL	1	889	5501744	636950	764	764	0
SL	1	890	5502004	636961	755	755	0
SL	1	891	5502062	636929	758	758	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
SL	1	892	5502093	636935	758	758	0
SL	1	893	5501874	637929	771	771	0
SL	1	894	5501822	637961	771	771	0
SL	1	895	5500083	639695	768	768	0
SL	1	896	5500057	639721	771	771	0
SL	1	897	5501291	639898	771	771	0
SL	1	898	5502374	639861	771	771	0
SL	1	899	5502442	639898	771	771	0
SL	1	900	5503056	639913	771	771	0
SL	1	901	5503108	639919	771	771	0
SL	1	902	5504855	636961	771	771	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
SL	1	903	5504810	636990	771	771	0
SL	1	904	5504827	637075	771	771	0
SL	1	905	5504832	637120	768	768	0
SL	1	906	5504849	637251	771	771	0
SL	1	907	5504821	637285	771	771	0
SL	1	908	5504685	637364	771	771	0
SL	1	909	5504651	637387	771	771	0
SL	1	910	5504781	637426	771	771	0
SL	1	911	5504793	637466	771	771	0
SL	1	912	5504793	637517	768	768	0
SL	1	913	5504656	637965	771	771	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
SL	1	914	5504696	637988	771	771	0
SL	1	915	5505104	637761	768	768	0
SL	1	916	5505155	637772	768	768	0
SL	1	917	5504135	638696	771	771	0
SL	1	918	5504169	638702	768	768	0
SL	1	919	5504044	639042	771	771	0
SL	1	920	5504135	639048	771	771	0
SL	1	921	5504186	639036	771	771	0
SL	1	922	5504203	638951	771	771	0
SL	1	923	5504231	639031	771	771	0
SL	1	924	5504328	639036	771	771	0

KODE1	IDRCH	IDDLG	ROWN	COLE	ADJ	STOPO	DELTA
SL	1	925	5504294	639201	771	771	0
SL	1	926	5504294	639263	771	771	0
SL	1	927	5504333	639257	771	771	0
SL	1	928	5504356	639201	768	768	0
SL	1	929	5504401	639070	771	771	0
SL	1	930	5504481	639025	771	771	0
SL	1	931	5504503	639053	771	771	0
SL	1	932	5504696	639138	771	771	0
SL	1	933	5504702	639053	768	768	0
SL	1	934	5504741	639048	771	771	0

KODE1	IDRCH	IBDLG	ROMN	COLF	ADJ	STOPO	DELTZ
SL	1	1142	5509659	631587	764	764	0
SL	1	1143	5509625	631417	758	764	0
SL	1	1144	5509732	631470	764	764	0
KODE1	IDRCH	IBDLG	ROMN	COLF	ADJ	STOPO	DELTZ
SL	1	1145	5509790	631558	771	771	0
SL	1	1146	5509770	631762	768	768	0
SL	1	1147	5509853	631179	768	768	0
SL	1	1148	5509897	631213	768	768	0
SL	1	1149	5510091	631256	771	771	0
SL	1	1150	5510130	631271	771	771	0
SL	1	1151	5509970	632199	768	768	0
SL	1	1152	5510135	631111	768	768	0
SL	1	1153	5510154	631159	768	768	0
SL	1	1154	5510353	631242	768	768	0
SL	1	1155	5510392	631213	771	771	0
KODE1	IDRCH	IBDLG	ROMN	COLF	ADJ	STOPO	DELTZ
SL	1	1156	5510732	631091	771	771	0
SL	1	1157	5510757	631047	771	771	0
SL	1	1158	5510815	631149	771	771	0
SL	1	1159	5510956	631140	771	771	0
SL	1	1160	5510776	631106	771	771	0
SL	1	1161	5510864	632660	758	758	0
SL	1	1162	5511014	632903	781	781	0
SL	1	1163	5510669	631033	771	771	0
SL	1	1164	5511346	631028	771	771	0
SL	1	1165	5511351	631083	771	771	0
SL	1	1166	5511366	631137	768	768	0
KODE1	IDRCH	IBDLG	ROMN	COLF	ADJ	STOPO	DELTZ
SL	1	1167	5512590	631058	771	771	0
SL	1	1168	5511924	633087	745	745	0
SL	1	1169	5511879	633082	755	755	0
SL	1	1170	5511218	632954	784	784	0
SL	1	1171	5511265	633250	787	787	0
SL	1	1172	5511340	633256	784	784	0
SL	1	1173	5511378	633325	768	768	0
SL	1	1174	5511504	633401	768	768	0
SL	1	1175	5511604	633495	771	771	0
SL	1	1176	5512194	633759	781	781	0
SL	1	1177	5512062	633332	761	761	0
KODE1	IDRCH	IBDLG	ROMN	COLF	ADJ	STOPO	DELTZ
SL	1	1178	5512326	633407	768	768	0
SL	1	1179	5512363	633451	768	768	0
SL	1	1180	5512414	633420	768	768	0
SL	1	1181	5512476	633539	768	768	0
SL	1	1182	5512464	633570	774	774	0
SL	1	1183	5512495	633639	774	774	0
SL	1	1184	5512533	633671	774	774	0
SL	1	1185	5512489	633702	774	774	0
SL	1	1186	5512407	633991	791	791	0
SL	1	1187	5512432	634079	787	787	0
SL	1	1188	5512464	634072	784	784	0
KODE1	IDRCH	IBDLG	ROMN	COLF	ADJ	STOPO	DELTZ
SL	1	1189	5512564	633376	758	758	0
SL	1	1190	5512696	633300	755	755	0
SL	1	1191	5512765	633520	768	768	0
SL	1	1192	5512803	633551	771	771	0

1213 rows selected.

IBDLG	IDCAT	ID1	VIFS	DELTG	IADDR
1166	CAT2	HR2	50	2	WEST_OF_DYKE
1167	CAT2	HR2	50	2	WEST_OF_DYKE
1168	CAT2	HR2	50	2	WEST_OF_DYKE
1169	CAT2	HR2	50	2	WEST_OF_DYKE
1170	CAT2	HR2	50	2	WEST_OF_DYKE
1171	CAT2	HR1	80	2	WEST_OF_DYKE
1172	CAT2	HR1	80	2	WEST_OF_DYKE
1173	CAT2	HR1	80	2	WEST_OF_DYKE
1174	CAT2	HR1	80	2	WEST_OF_DYKE
1175	CAT2	HR1	80	2	WEST_OF_DYKE
1176	CAT2	HR1	80	2	WEST_OF_DYKE
1177	CAT2	HR1	80	2	WEST_OF_DYKE
1178	CAT2	HR1	80	2	WEST_OF_DYKE
1179	CAT2	HR1	80	2	WEST_OF_DYKE
1180	CAT2	HR1	80	2	WEST_OF_DYKE
1181	CAT2	HR1	80	2	WEST_OF_DYKE
1182	CAT2	HR1	80	2	WEST_OF_DYKE
1183	CAT2	HR1	80	2	WEST_OF_DYKE
1184	CAT2	HR1	80	2	WEST_OF_DYKE
1185	CAT2	HR1	80	2	WEST_OF_DYKE
1186	CAT2	HR1	80	2	WEST_OF_DYKE
1187	CAT2	HR1	80	2	WEST_OF_DYKE
1188	CAT2	HR1	80	2	WEST_OF_DYKE
1189	CAT2	HR1	80	2	WEST_OF_DYKE
1190	CAT2	HR1	80	2	WEST_OF_DYKE
1191	CAT2	HR1	80	2	WEST_OF_DYKE
1192	CAT2	HR1	80	2	WEST_OF_DYKE
1193	CAT2	HR1	80	2	WEST_OF_DYKE
1194	CAT2	HR1	80	2	WEST_OF_DYKE
1195	CAT2	HR1	80	2	WEST_OF_DYKE
1196	CAT2	HR1	80	2	WEST_OF_DYKE
1197	CAT2	HR1	80	2	WEST_OF_DYKE
1198	CAT2	HR1	80	2	WEST_OF_DYKE
1199	CAT2	HR1	80	2	WEST_OF_DYKE
1200	CAT2	HR1	80	2	WEST_OF_DYKE
1201	CAT2	HR1	80	2	WEST_OF_DYKE
1202	CAT2	HR1	80	2	WEST_OF_DYKE
1203	CAT2	HR1	80	2	WEST_OF_DYKE
1204	CAT2	HR1	80	2	WEST_OF_DYKE
1205	CAT2	HR1	80	2	WEST_OF_DYKE
1206	CAT2	HR1	80	2	WEST_OF_DYKE
1207	CAT2	HR1	80	2	WEST_OF_DYKE
1208	CAT2	HR1	80	2	WEST_OF_DYKE
1209	CAT2	HR1	80	2	WEST_OF_DYKE
1210	CAT2	HR1	80	2	WEST_OF_DYKE
1211	CAT2	HR1	80	2	WEST_OF_DYKE
1212	CAT2	HR1	80	2	WEST_OF_DYKE
1213	CAT2	HR1	80	2	WEST_OF_DYKE

1213 rows selected.