

**A Groundwater Modelling Application  
for a Groundwater Flow Problem  
for A Shallow Unconfined Aquifer In  
Borno State, Nigeria**

**By**

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**A Report**

**Submitted to The Department of Civil and Geological Engineering  
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Degree of Master in Engineering**

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Executive Summary

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## EXECUTIVE SUMMARY

This Study is undertaken to demonstrate a basic understanding and working knowledge of the principles of groundwater modelling studied at the master's level in engineering. The task of developing and calibrating a model is not completely fulfilled. However, the author has gained valuable experience in the methodology of modelling through conceptualization, discretization, parameter estimation, calibration and documenting the exercise. The model could not be calibrated sufficiently well enough to permit transient simulations as limited data is available for establishing input parameters and for calibration. An increase in the number of elements, and a finer discretization in critical areas of the model domain are expected to reduce errors caused by large element aspect ratios and vertical flow gradients. A vertical-profile model or unsaturated-saturated flow model is recommended as an alternative to the 2-dimensional areal model utilized in this study. The difficulty in calibrating the model illustrates the requirement for more detailed field investigations to determine aquifer parameters and the spatial variability across the basin.

## **Disclaimer**

This work is outside the Terms of Reference for the work undertaken by the author in Nigeria for the Borno State Agricultural Development Project (BOSADP), and is strictly on a personal interest basis. Therefore, the accuracy and usefulness of this information to any interested parties is neither implied nor guaranteed.

## 1.0 PREFACE

As partial requirements for the fulfillment of the degree of Masters of Engineering, the student is required to demonstrate, through practical application, a working knowledge of the theory and concepts studied at an advanced level. This report details work undertaken by the author in the field of hydrogeology in response to this requirement.

This report outlines the field work undertaken, the formulation of the conceptual and mathematical models, calibration and sensitivity analysis, and finally the conclusions and recommendations drawn from the Study.

## 2.0 INTRODUCTION AND SCOPE

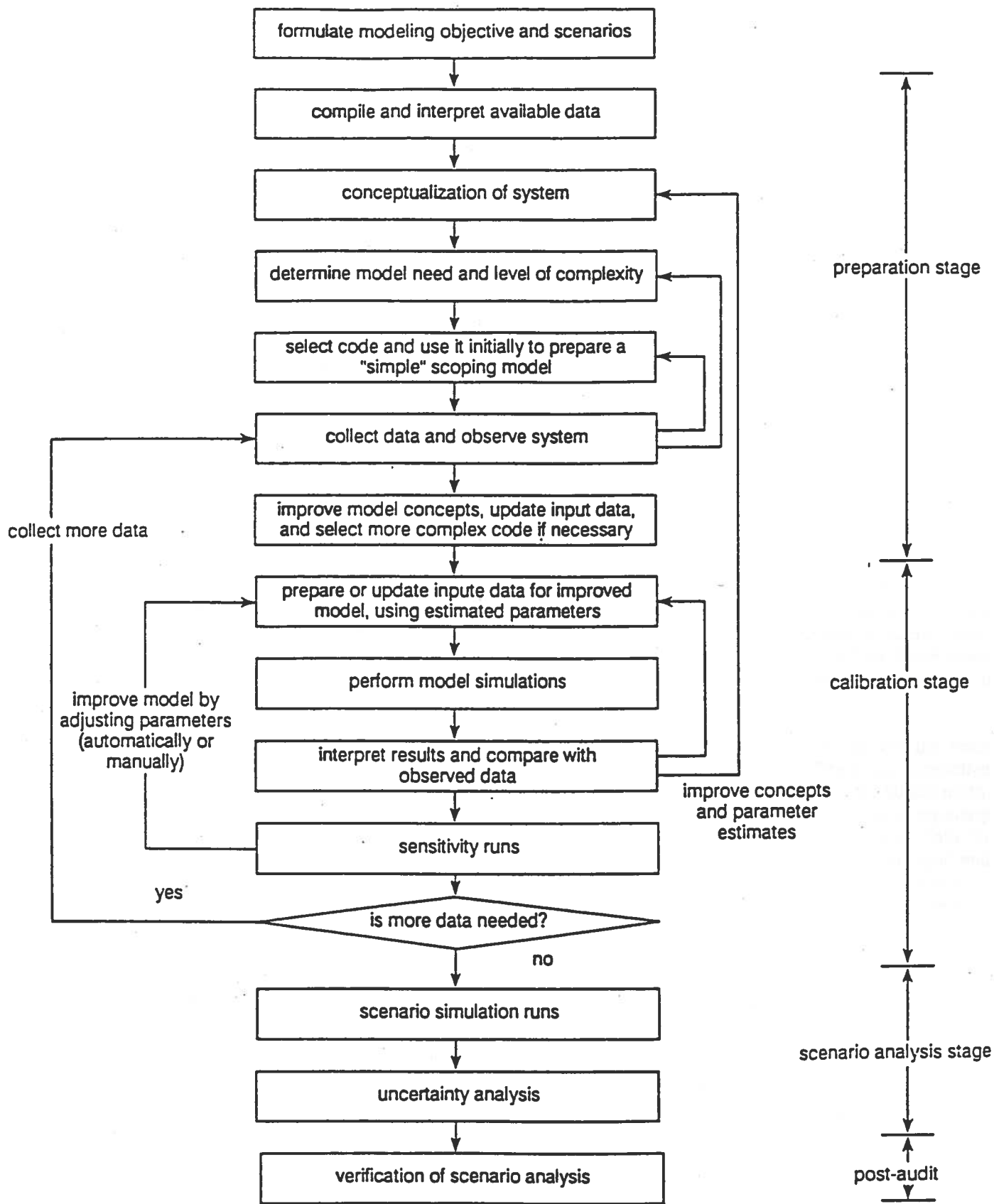
The purpose of this work is to develop a working groundwater flow model of the Wushi River Basin, Nigeria, and in turn to evaluate the potential impact of hydrologic stresses on the lower reaches of the basin. Such stresses to be evaluated include upstream abstraction, reduced precipitation and recharge, and excessive well development (well interference) in the middle reaches of the basin where large scale banana and mango plantations are proposed for development.

Due to limited field resources and poor climatic records, calibration and verification of the model are only partially successful for this modelling exercise. It was not possible to conduct transient simulations to investigate the potential impacts of stresses on the basin. Nonetheless the development of the conceptual and mathematical models for steady state flow is now presented.

Due to the complexity of the aquifer domain, analytical models are not capable of realistically representing the complex boundary conditions and heterogeneity of the aquifer. Numerical computer modelling is chosen and the United States Geological Survey's, Modular Finite Difference Flow Model (MODFLOW) was initially selected to solve the problem. Due to the irregular aquifer boundary and the inability of MODFLOW to handle such irregular domains, AQUIFEM-1 is the code finally utilized to solve the problem.

The modelling methodology and protocol as outlined in Anderson and Woessner (1992) is utilized for this Study. The methodology is graphically illustrated in Figure 1, with a summary of the critical modelling steps as follows:

1. The initial step is to define the purpose of the modelling effort and to determine the best method to obtain the desired results. (ie: analytical/numerical modelling of field testing);
2. The next step is to define the conceptual model based on hydrogeological and physical properties such as stratigraphy, physical boundaries, aquifer properties, and other site characteristics such as river flow, precipitation etc. Some of this information can be obtained from previous reports, historical data or field investigations;
3. Based on the conceptual model, the governing equation and suitable computer code are selected to solve the problem;
4. The mathematical model is then constructed by discretizing the aquifer domain into elements and assigning initial parameter values to the elements and boundary and/or initial conditions;
5. The mathematical model is then calibrated by adjusting the selected parameters until the model approximates observed field conditions;



6. A sensitivity analysis is then undertaken to assess the sensitivity of the model to variation in the input parameters;
7. The model is then verified by assessing the ability of the model to reproduce a new set of data from the aquifer.
8. Following the verification process, the model is used to predict the impacts of various stresses or external conditions imposed on the aquifer.
9. The results of the stress impacts (scenarios) are then compiled and compared and conclusions drawn from the results, and;
10. A postaudit is then conducted to compare the model results with actual field results from pumping tests, etc.

### 3.0 PHYSICAL SETTING

The Study basin is located in the north east corner of Nigeria, Africa, along the Wushi River at nominal latitude 10°15' north and longitude 12°30' east (See Figures 2 and 3). The basin is comprised of the Wushi and Yangari river floodplains which flow in a westerly direction to join with the much larger Jawi River. Flow is predominantly controlled by bedrock topography as elevation ranges from over 2500 m in the upper reaches of the basin to 750 m where the Wushi River converges with the Jawi River. The drainage basin covers a total area of 416.4 km<sup>2</sup>. The topographic map of the Study basin in Figure 4 shows the development in the area is minimal with only sparsely located villages. There are some hand dug wells used for potable water supply and 5 shallow (less than 8 m deep) PVC tubewells used for small scale agricultural farming. Other water use in the basin is by residual moisture farming of rice, cowpea, corn and millet following the rainy season.

Climatic information from the City of Maiduguri which is located 300 km to the north, as are the most representative data for the Wushi River Basin. This data is presented in Table 1. The total cumulative annual precipitation is 646 mm. Some precipitation records for the town of Biu, located only 50 km north, are available but are not considered statistically valid due to the absence of data for a number of reporting years and extreme inconsistency in the data for years which are available. A comparison of data for Maiduguri and Biu from 1982 through 1984 indicate that rainfall increases to the south from Maiduguri and is 15 percent greater in the area of the Wushi River Basin. Particular note, however, is given to the uneven distribution of rainfall which consists of no precipitation from November through March and over 50 percent of the yearly total occurring in the 2 months of July and August.

Streamflow records for the Wushi, Yangari and Jawi rivers do not exist. Accounts from interviews with the local farmers and field observations indicate that none of the rivers are considered perennial. Maximum peak flows occur during flood stages in the rainy season in late August or early September and last only a few days. For example at the town of Wushi along the middle reach of the Wushi River the peak during 1991 was 2.4 m and lasted from August 23 to September 2.

### 4.0 GEOLOGY AND HYDROGEOLOGY

Geology and hydrogeological information for the basin have been summarized in the 1992 report by Wardrop Engineering of Winnipeg, Canada for the Borno State Agricultural Development Project (BOSADP). The report was based on both an office study and a field program directed by the author. A brief summary is given in the following section.

# State Map of Nigeria

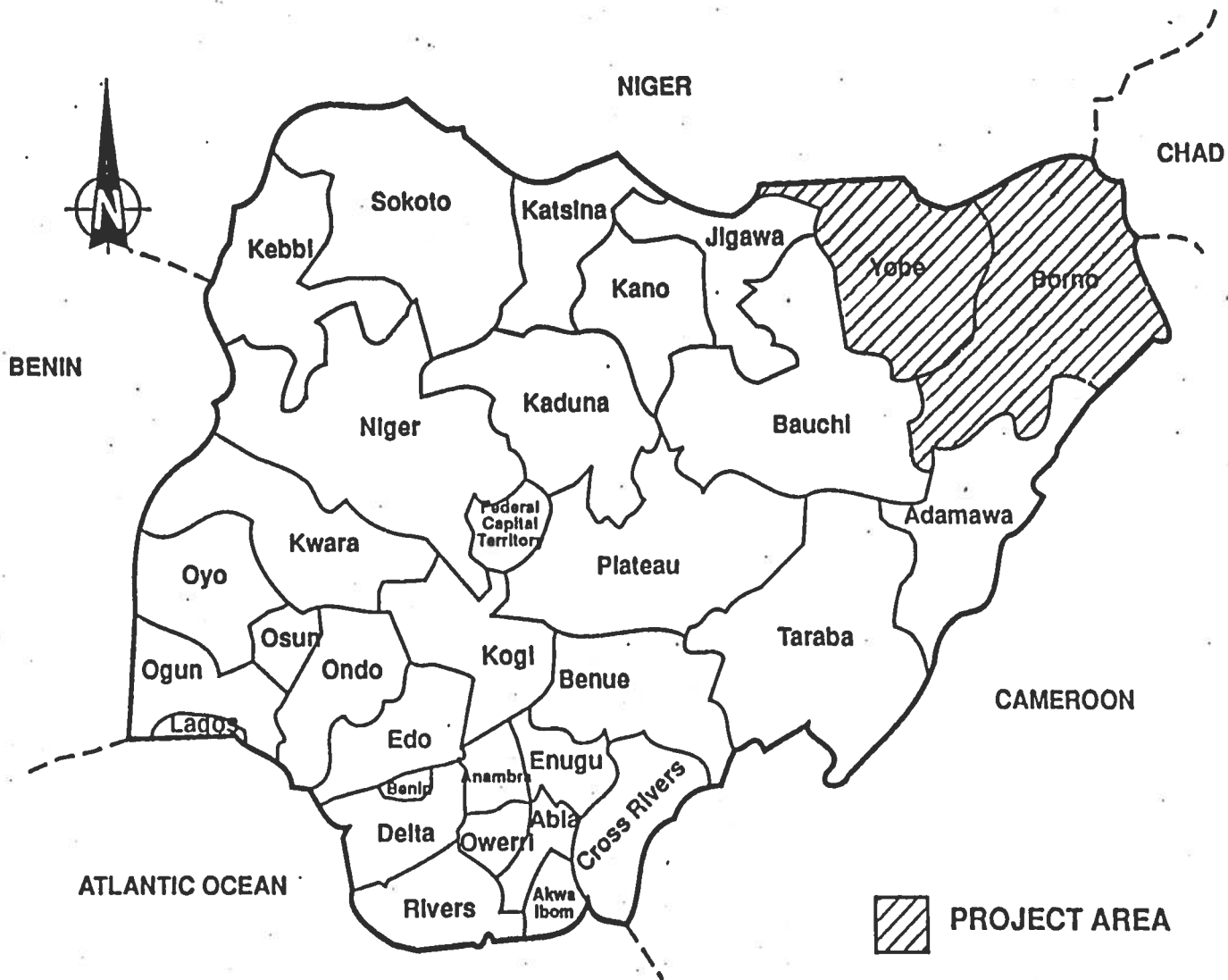
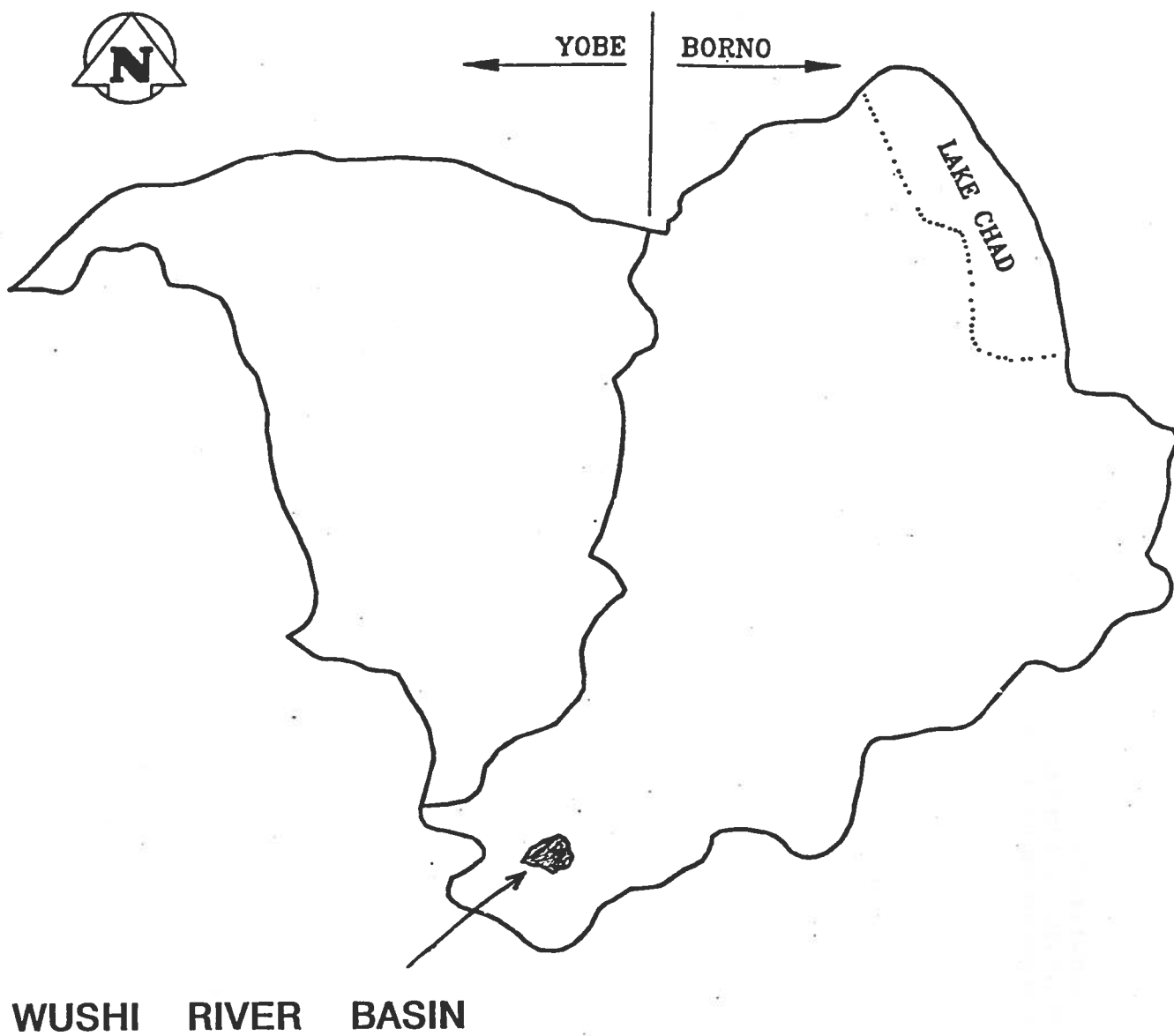


FIGURE 2

SOURCE:

WARDROP ENGINEERING INC., 1992, STUDY OF IRRIGATION POTENTIAL OF SHALLOW GROUNDWATER IN FADAMA AREAS OF YOBE AND BORNO STATES, A REPORT TO BORNO STATE AGRICULTURAL DEVELOPMENT PROJECT





**TABLE 1 CLIMATIC PARAMETERS FOR MAIDUGURI**

|  | Jan   | Feb   | Mar   | Apr   | May   | June  | July  | Aug   | Sept  | Oct   | Nov   | Dec   |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Rainfall (mm)                                    | 0.0   | 0.0   | 0.0   | 8.4   | 36.5  | 75.7  | 172.6 | 227.1 | 107.0 | 18.6  | 0.0   | 0.0   |
| Average Daily Temperature (centigrade)           | 27.5  | 32.1  | 32.1  | 33.1  | 33.0  | 31.9  | 30.9  | 27.2  | 28.6  | 30.8  | 30.9  | 26.7  |
| Relative Humidity (percent)                      | 21.9  | 15.9  | 13.9  | 20.3  | 30.7  | 37.8  | 59.2  | 68.3  | 59.1  | 35.6  | 22.0  | 21.2  |
| Sunshine Hours (average monthly)                 | 373   | 273   | 270   | 251   | 269   | 244   | 246   | 177   | 229   | 285   | 282   | 210   |
| Sunshine Mean Daily Hours                        | 10.4  | 4.7   | 8.7   | 8.4   | 8.7   | 8.1   | 7.9   | 5.7   | 7.6   | 9.2   | 9.4   | 6.8   |
| Potential Evapotranspiration (average in mm/day) | 144.5 | 159.0 | 201.0 | 209.0 | 208.0 | 172.0 | 135.0 | 113.0 | 130.0 | 156.0 | 149.0 | 132.0 |
| Potential Evaporation (average in mm/day)        | 4.7   | 5.7   | 6.5   | 6.9   | 6.7   | 5.7   | 4.3   | 3.6   | 4.3   | 5.0   | 4.0   | 4.3   |

SOURCE:

WARDROP ENGINEERING INC., 1992, STUDY OF IRRIGATION POTENTIAL OF SHALLOW GROUNDWATER IN PADAMA AREAS OF YOBE AND BORNO STATES, A REPORT TO BORNO STATE AGRICULTURAL DEVELOPMENT PROJECT



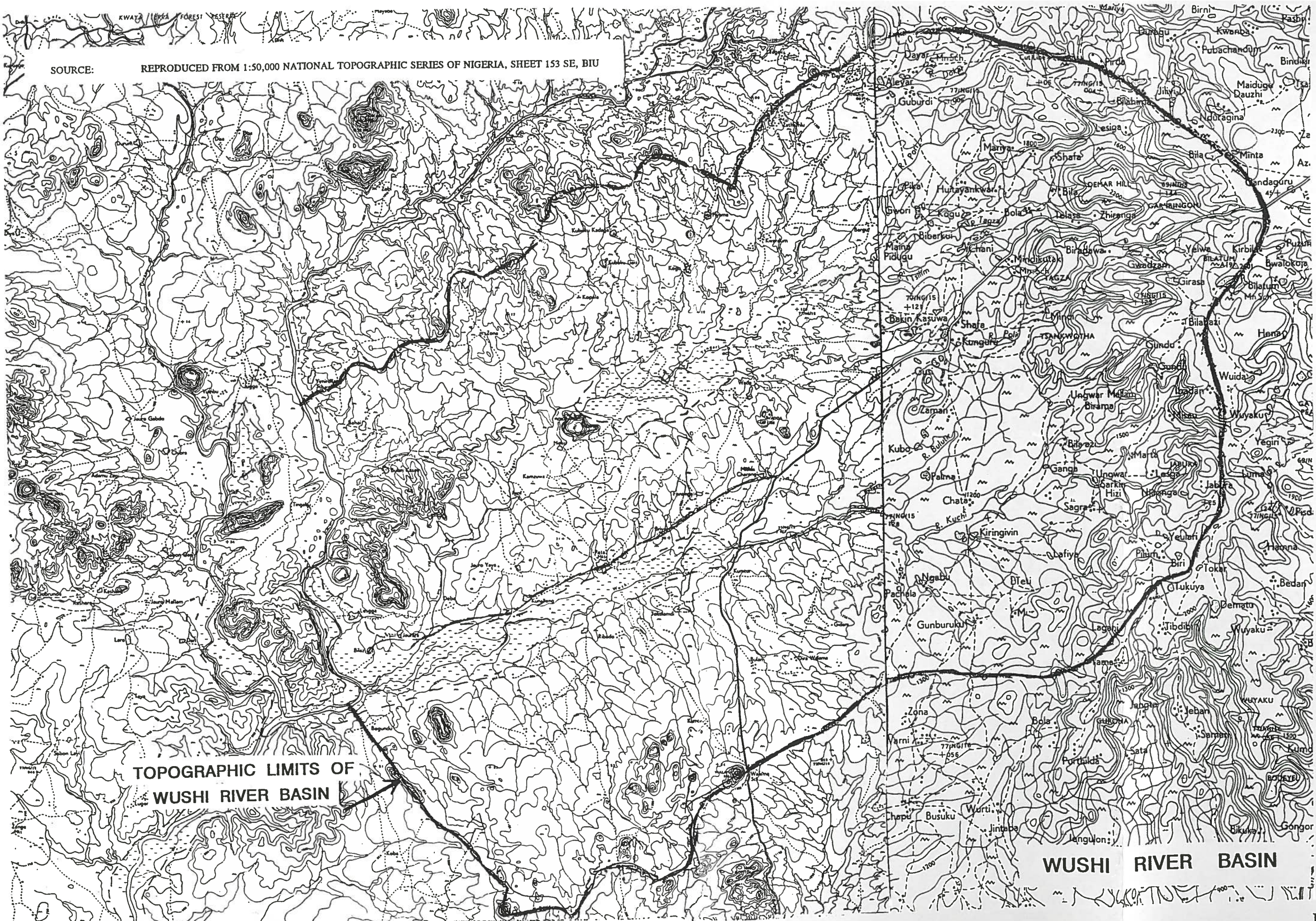


FIGURE 4



#### 4.1 HISTORICAL INFORMATION

Reports on the geology of the area had been compiled by The Geological Survey of Nigeria (1963), and the United States Geological Survey (1965). These reports describe the extensive plateaus of the Tertiary age Biu-Longida Basalts, which cover large areas of the Kerri-Kerri formation and the Crystalline-Basement complex. The edges of the plateau and exposed areas of basement complex are deeply dissected and filled with thin sequences (less than 10 m) of recent alluvium. Surface water runoff is reported to be rapid and streams are non-perennial.

More specifically, the Wushi River Basin is dominated by Moku Hill and Bogundu Hill which are both volcanic basalt pillars. The upper reach of the basin is characterized by granitic rock outcrop with little or no overburden.

#### 4.2 FIELD PROGRAM

To augment the topographical and climatic information, a field program was undertaken to determine suitable input parameters for the formulation of an aquifer model. The program included testhole drilling, shallow well construction, pumping tests on existing and new wells and static water level measurements throughout the basin. Detailed testhole logs and pumping test plots are presented in Appendix A. A summary of the field program is given in Table 2. All information is referenced to a Cartesian coordinate system established for the modelling Study.

Testholes and wells were constructed using the hand bailer/auger method and completed with 100 mm diameter PVC casing. Pumping tests were conducted using a 2.5 hp centrifugal suction lift pump. All coordinates were determined using a satellite positioning instrument.

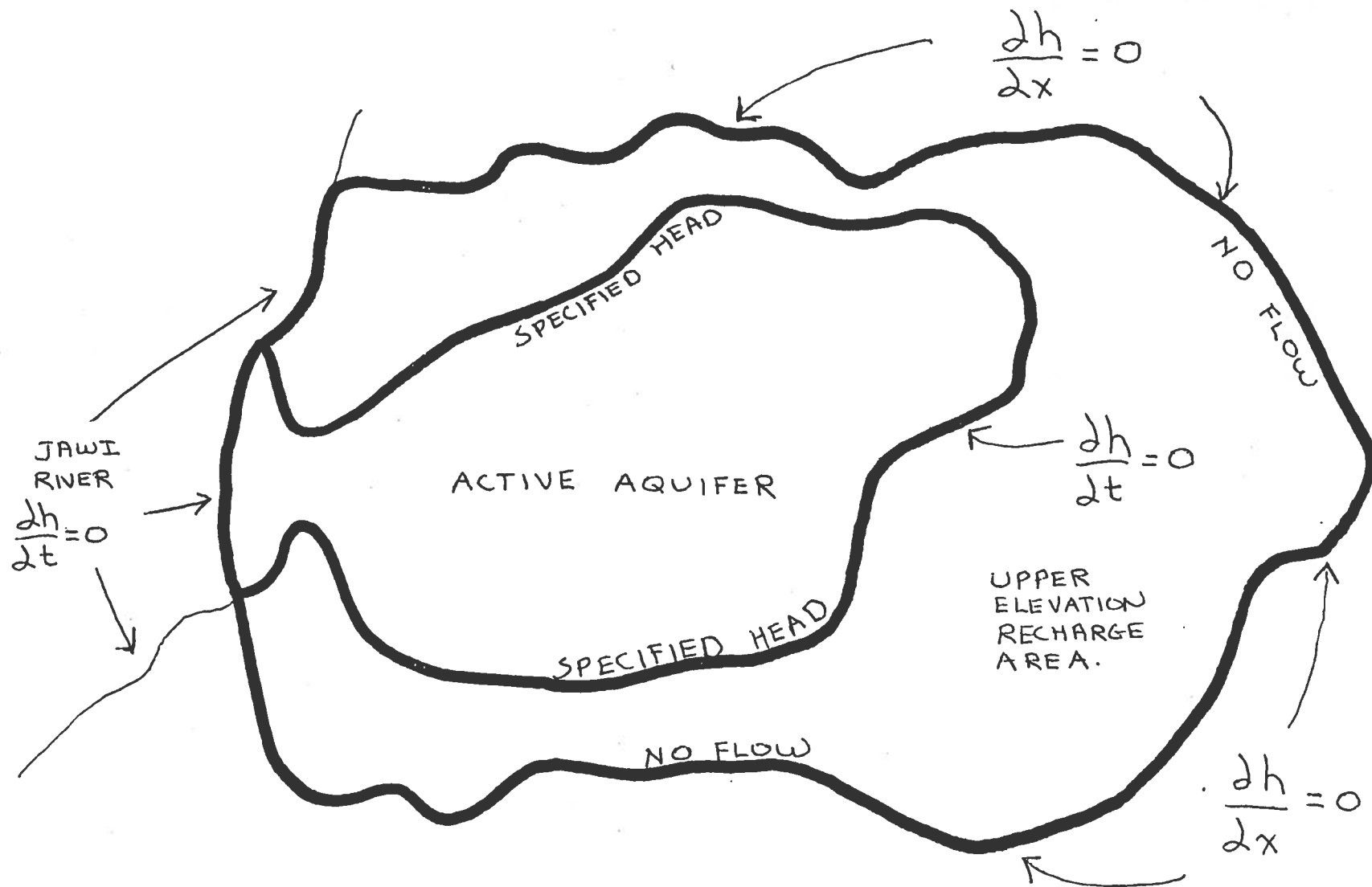
Based on the field program it is determined that the basin is typically comprised of an unconfined aquifer, ranging up to 8 m thickness. The aquifer thins out laterally away from the main river axes. Sediments are typically poorly graded and sub-rounded. Transmissivities calculated from pumping tests range from 80 m<sup>2</sup>/day to 200 m<sup>2</sup>/day. Hydraulic conductivities for testhole locations have been estimated based on sieve analysis and Hazen's Formula,  $k=d_{10}^2$ , where  $d_{10}$  represents the grain size diameter of 10 percent passing. Transmissivities have also been estimated using  $T=kb$ , where transmissivity (T), is calculated based on hydraulic conductivity (k) and saturated thickness (b). Aquifer properties and boundaries are irregular and non-homogeneous.

#### 5.0 CONCEPTUAL MODEL

The conceptual model of the aquifer is based on the geology and hydrogeology of the Study area. The model is defined by identifying physical features to the model such as hydrostratigraphic units, fluxes and boundaries to the aquifer domain. Aquifer properties and other input parameters for the conceptual model have been assigned based on the field program and on relevant climatic data.

The Study basin covers a total area of 416.38 km<sup>2</sup>, which comprises the entire drainage basin for the Wushi River as determined by topography. A Cartesian coordinate system is oriented with the x direction roughly parallel to the main axis of the Wushi River. The grid extends for 31 km in the x, and 21 km in the y direction. Approximately 251 km<sup>2</sup> (60 percent) of the total area is located in the higher elevation areas. These areas have limited thickness of alluvium and are designated as a recharge area. The two hills, Moku and Bogundu, are also considered non-active aquifer areas due to elevation and limited thickness of alluvium. At all locations throughout the model domain, the crystalline basement complex is the bottom unit and this unit is assumed to be non-conductive, based on a hydraulic conductivity several orders of magnitude less than alluvium.

6



CONCEPTUAL MODEL OF  
WUSHI RIVER BASIN

Groundwater flow throughout the area is topographically driven and occurs generally from the high elevation, eastern uplands towards the Jawi River. The main aquifer is situated along the two rivers (Wushi and Yangari). The flow is primarily horizontal throughout the basin even though the elevation difference from the upper to lower reaches of the basin is 1700 m. The large elevation changes occur in the uppermost portion of the basin, where the flow is primarily horizontal (5 percent gradient). Static water levels are generally within 3 m of the ground surface.

The ground water flow problem is reduced from a three dimensional problem to a two-dimensional problem by invoking the Dupuit assumptions. The Dupuit assumptions include; horizontal flow and vertical equipotentials; a horizontal gradient equal to the slope of the free surface; and the gradient to be invariant with depth (Freeze & Cherry, 1979). In the two-dimensional areal flow model, transmissivity is calculated based on spatial distribution of hydraulic conductivity and saturated thickness.

Surface water flow is present along the river channels of the Wushi and Yangari rivers for part of the rainy season in July and August. The Jawi River, which forms the western boundary to the model, is considered a perennial river for this application, despite the lack of flow data to support this assumption.

A sub-arid tropical climate for the area produces high evapotranspiration rates. Infiltration and recharge into the aquifer are estimated to be less than 40 percent of the total yearly precipitation. This assumption is consistent with evapotranspiration rates established for the area by The Federal Government of Nigeria, Ministry of Agriculture (1976), based on FAO guidelines (United Nations-Food and Agricultural Organization) .

In summary, the chosen conceptual model is a two-dimensional, unconfined, areal flow model incorporating the initial assumptions of a no flow boundary around the majority of the topographical limits of the drainage basin, with a constant head boundary along the Jawi River, where the flow collects and discharges into the river. Several zones are identified to account for regions of varying aquifer properties such as thickness, hydraulic conductivity, recharge rate, and storage coefficient. A sketch illustrating the main features of the conceptual model is shown in Figure 5. During calibration of the model, additional physical restrictions are added to account for rising ground water levels, seepage faces and lateral fluxes. These are described in Section 7.2.

**TABLE 2**  
**SUMMARY OF FIELD INVESTIGATIONS**

| LOCATION                         | INFORMATION                               |
|----------------------------------|---|
| Node 628 (9.3,10.1) Peta         | Testhole, swl, sieve                      |
| Node 1018 (20.5,14.4) Wada       | Testhole, swl, sieve                      |
| Node 1102 (17.1,8.2)             | Testhole, swl, sieve                      |
| Node 683 (8.4,9.3) Ribado        | Testhole, swl, sieve                      |
| Node 384 (6.4,10.1) Kunalleng    | Testhole, swl, sieve                      |
| Node 49 (2.9,10.9) Bilazi        | Existing Well Pumping Test, swl, testhole |
| Node 815 (13.8,9.4) Kumtor       | Existing Well Pumping Test, swl, testhole |
| Node 111 (5.5,16.3) Bahai        | Testhole, swl, sieve                      |
| Node 831 (11.4,6.9) Kumtor/Bulam | Testhole, swl, sieve                      |
| Node 39 (3.1, 13.0) Lessga       | Existing Well, swl, testhole              |
| Node 567 (8.0,10.0) Kunalleng    | Existing Well Pumping Test, swl, testhole |
| Node 205 (6.6,16.3) Jauro Yaya   | Existing Well, swl, testhole              |

# WUSHI VALLEY AQUIFER

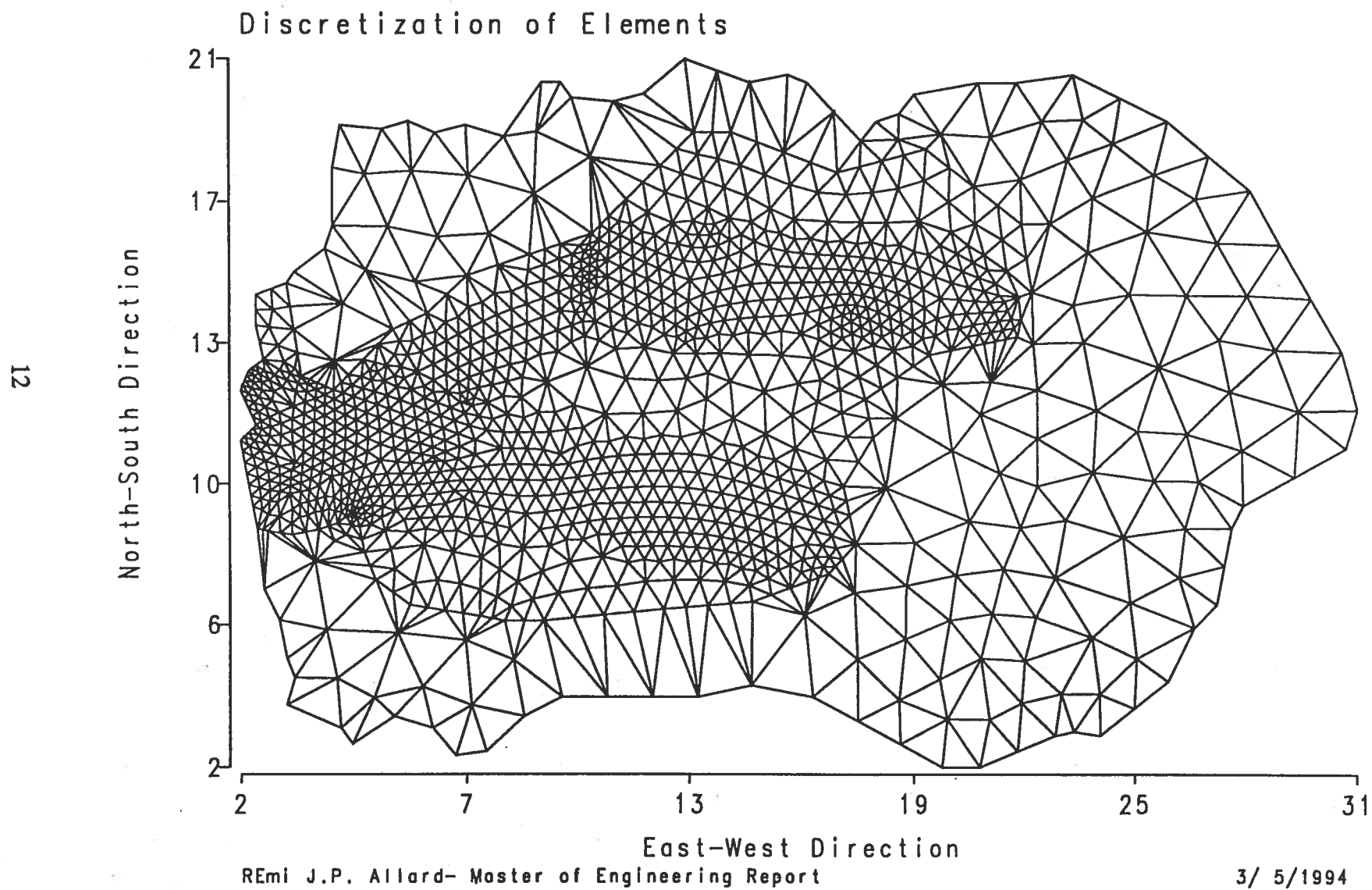


FIGURE 6



## 6.0 MATHEMATICAL MODEL

A complete overview of the method of finite elements is beyond the scope of this report. It is assumed the reader is familiar with the mathematics behind the formulation of the system of equations utilized for the solution of the groundwater flow problem. For completeness, however, a simplified description of the finite element method is presented. Good summaries of the finite difference method are presented by Anderson and Woessner (1992), Mercer and Faust (1981) and van der Heijde et al., (1988).

The response of an aquifer to pumping depends on the transmissivity and storage coefficient of the aquifer, the hydrologic and geologic boundary conditions, and the points at which water is being withdrawn or recharged within the system (Bachmat et al., 1980). For analytical solutions the variables of transmissivity and storage coefficient are assumed to be homogeneous, isotropic, and the aquifer to be thin, and infinite in areal extent. For more complex aquifer geometries with complex boundary conditions and heterogeneities, a mathematical framework or model comprised of a system of governing partial differential equations (PDE's) are used to describe the flow process. Boundary conditions refer hydraulic conditions at the boundary or limits of an aquifer system.

In the governing partial differential equation for groundwater flow, the aquifer characteristics and heads are depicted as continuously changing. In the finite element method, the continuous heads are replaced with discrete values that are defined at selected points or nodes within the aquifer system.

For a particular groundwater flow problem, the domain of the aquifer must be discretized or divided into elements and nodes. For each element or node, aquifer parameters must be input into the governing equation of flow and the system of equations formed for all the nodes within the aquifer domain forms the system of equations requiring solving.

The governing equation for two-dimensional, horizontal flow in a non-homogeneous, anisotropic aquifer is;

$$Q + S \frac{\delta h}{\delta t} = \frac{\delta}{\delta x} \left( T_{xx} \frac{\delta h}{\delta x} \right) + \frac{\delta}{\delta y} \left( T_{yy} \frac{\delta h}{\delta y} \right) + \frac{\delta}{\delta x} \left( T_{xy} \frac{\delta h}{\delta y} \right) + \frac{\delta}{\delta y} \left( T_{yx} \frac{\delta h}{\delta x} \right)$$

where;

|                 |  |
|-----------------|--|
| $S = S(x,y,t)$  | = aquifer storage coefficient [dimensionless];   |
| $h = h(x,y,t)$  | = depth averaged piezometric head [L];   |
| $T_{xx} = T(x)$ | = aquifer transmissivity in x direction [ $L^2/t$ ];   |
| $T_{yy} = T(y)$ | = aquifer transmissivity in y direction [ $L^2/t$ ];   |
| $K' = K'(x,y)$  | = vertical averaged permeability of the aquifer [ $L/t$ ];   |
| $Q = Q(x,y,t)$  | = net flux into aquifer from point or distributed sources [ $L/t$ ];                               |
| $B' = B'(x,y)$  | = thickness of saturated aquifer [L]   |
| $x, y$          | = Cartesian coordinates oriented along the principle axes of the hydraulic conductivity tensor [L] |
| $t$             | = time [t]   |

## **6.1 Description of Model Source Code**

AQUIFEM-1 is a Galerkin based finite-element computer program written in Fortran which utilizes linear interpolation functions and triangular elements. The code was developed to model two dimensional flow both in plan and in profile. Constant head (first type), constant flux (second type) and mixed (Cauchy or third type) boundary conditions are capable of being represented by this model. The source code is public-domain software.

An in depth summary of the code AQUIFEM-1 and further explanation of the mathematics and assumptions incorporated in the computer program development is beyond the scope of this report. For further reading the reader is referred to Townley et al, 1980. For completeness, example input and output files from AQUIFEM-1 are presented in Appendix B.

## **7.0 MODEL DESIGN AND INPUTS**

### **7.1 Mesh Generation**

Using the limits of the Wushi River drainage basin as determined from the topographic map and by overlaying the Cartesian coordinate system, the limits of the modelled area where assigned coordinates for plotting. For ease in assigning element properties at a later stage, the aquifer domain is divided into sub-regions. A triangular finite element mesh is then generated for the entire model domain using the University of Waterloo's, GRIDBUILDER program. Some areas of the mesh have smaller elements to allow for greater solution accuracy. In particular, areas where existing wells are present and where large elevation changes occur over short distances are discretized to a smaller scale. In total, 1187 nodes and 2272 elements are generated for the solution of the problem. The finite element mesh is shown in Figure 6 and the GRIDBUILDER data input file is presented in Appendix B.

### **7.2 Boundary Conditions**

The equation of flow is a general statement of fluid continuity within a region being modelled. However, the simulation has to account for the effects of conditions outside of the region. Boundary conditions are mathematical translations of physical conditions along the boundary of the aquifer domain. The boundary conditions for this model are dictated by the unique geology of the Wushi River Basin. They are summarized as follows:

- The outer limits of the basin (except where adjacent to the Jawi River) is a fixed no-flow boundary;
- The majority of the higher elevation areas, where aquifer thickness is less than 1 m, is designated as a non-active, transition area. This area is eliminated from the main model Study, as large elevation changes exist. These cause large vertical flow gradients and unsaturated conditions to develop. By setting the vertical recharge flux equal to zero for this area, and fixing the head along the interface between this area and the active model, the interface becomes a constant horizontal flux boundary (constant head boundary). This condition is also applied to the volcanic cone areas at Bogunda Hill and Moku Hill.
- The lower west-end of the aquifer domain along the Jawi River is designated as a fixed-head boundary controlled by the elevation of water in the river. It is assumed that the river is perennial, and fully penetrates the aquifer.

- Due to the irregular precipitation and flooding which occurs during the intense rainy season, it is anticipated that ground water levels would rise significantly above surface elevation during steady state simulation runs. To accomodate rising levels, ground water rising nodes (first-type rising water level nodes) are established along all stream axes.
- In addition to rising groundwater level nodes along streams, areas where seepage faces were possible are designated as first type rising water level nodes.
- The initial conditions included the initial estimate of the head distribution (static water level distribution) throughout the model domain. This distribution was taken as the surface elevation as determined from a topographic map of the area.

### 7.3 Parameter Estimation (Aquifer Properties)

Based on interpretation of the geology and hydrogeology of the area, the model is divided into 11 sub-regions, each with distinct aquifer properties. These properties are based primarily on assigned hydraulic conductivities. Initial estimates of hydraulic conductivity are based on testhole profiles, pumping test results, and seive analysis. Element and nodal elevations are calculated by kriging the original field elevation values taken from the topographic map. The properties are adjusted in value during calibration until predicted heads from simulation runs are in agreement with observed field values. The initial input parameters are shown in Figures 7 through 12. The best simulation results are obtained with the distribution of hydraulic conductivities as shown in Figure 13 and Table 3.

Zones 5,6,7, and 8 are the main aquifer zones along the axes of the Wushi and Yangari rivers. The hydraulic conductivity is based on pumping tests and saturated thicknesses observed in testhole drilling. The initially-assigned and final calibrated values for these sub-regions did not change significantly during calibration.

The general lower recharge area is slightly higher in elevation and dominated by finer grained sands and a reduced thickness of aquifer. This area is therefore assigned a slightly lower hydraulic conductivity. This value is estimated at 30 m/day, initially.

The upper recharge area is assigned a low hydraulic conductivity to allow significant accumulation of head behind the horizontal flux boundary. This value changed from an initial estimate of 2 m/day to 0.007 m/day.

All values are in general agreement with established values for similar geological materials except the upper recharge area. For reference, the reader is referred to Freeze & Cherry (1979).

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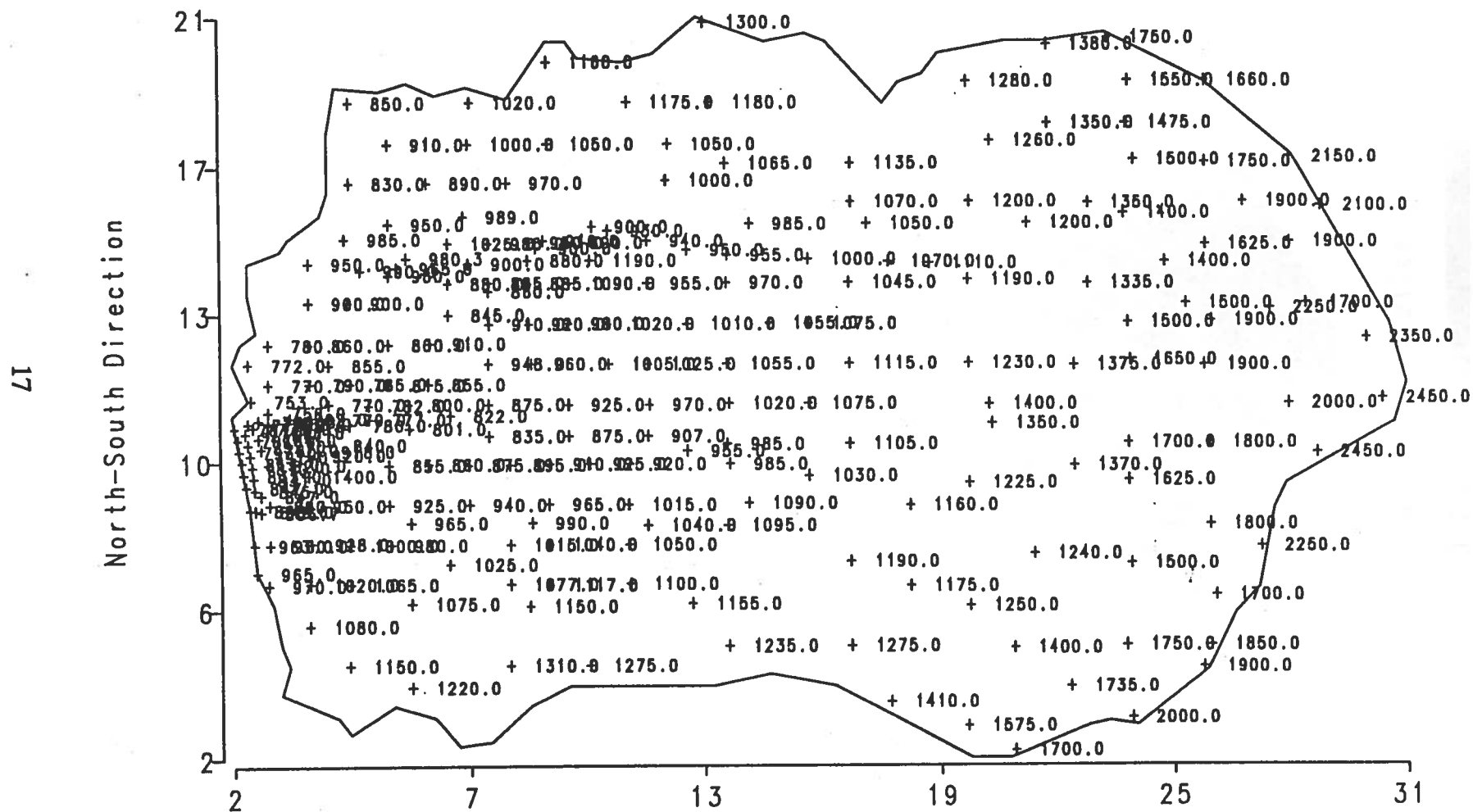
**TABLE 3**  
**HYDRAULIC CONDUCTIVITY DISTRIBUTION**  
**FOR BEST CALIBRATED RESULT**

| Aquifer Sub-Region         | Hydraulic Conductivity<br>(m/day) |
|----------------------------|-----------------------------------|
| 1- Upper Recharge Area     | 0.007                             |
| 2- Wushi South             | 35                                |
| 3- Bogundu Hill High       | 15                                |
| 4- Bogundu Hill Low        | 35                                |
| 5- Wushi Middle            | 75                                |
| 6- Wushi Low               | 100                               |
| 7- Yangari High            | 75                                |
| 8- Yangari Low             | 80                                |
| 9- Jawi South              | 60                                |
| 10- Lessga Rock Knob       | 35                                |
| 11- General Lower Recharge | 55                                |

# WUSHI VALLEY AQUIFER

+ 1.0

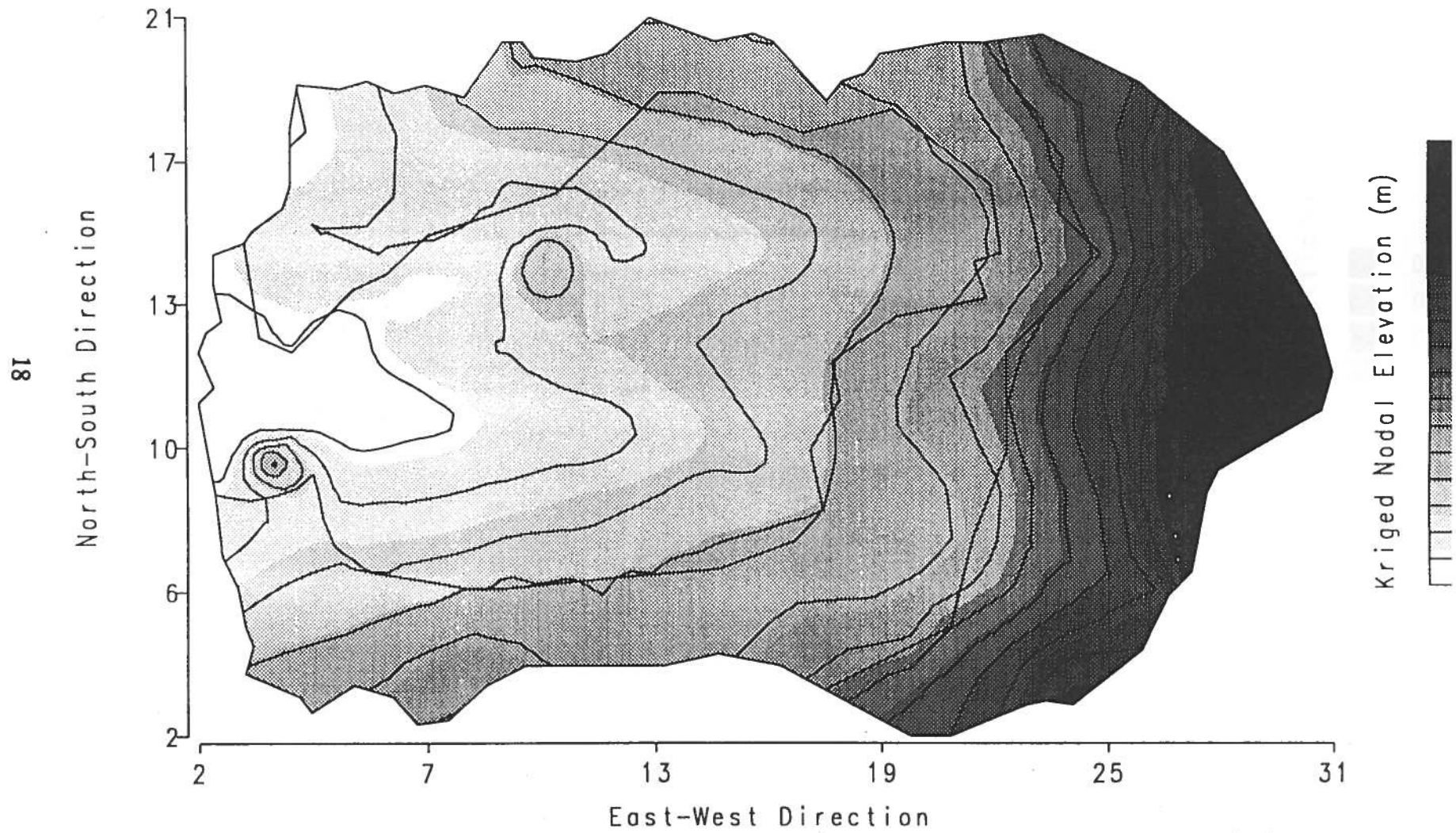
Elevation Data



Remi J.P. Allard- Master of Engineering Report

3/ 5/1994

# WUSHI VALLEY AQUIFER

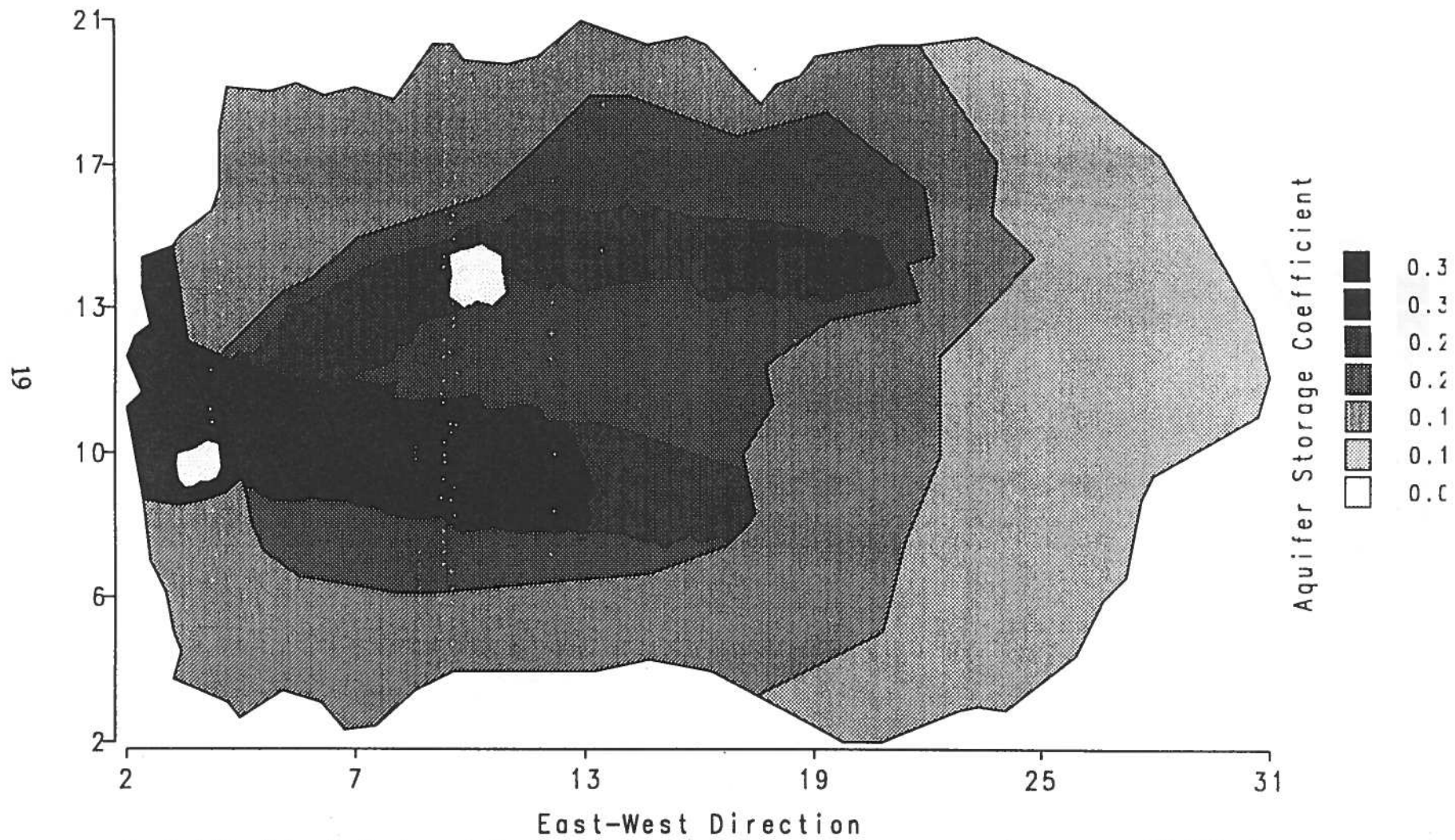


Remi J.P. Allard- Master of Engineering Report

3/ 5/1994

FIGURE 8

# WUSHI VALLEY AQUIFER

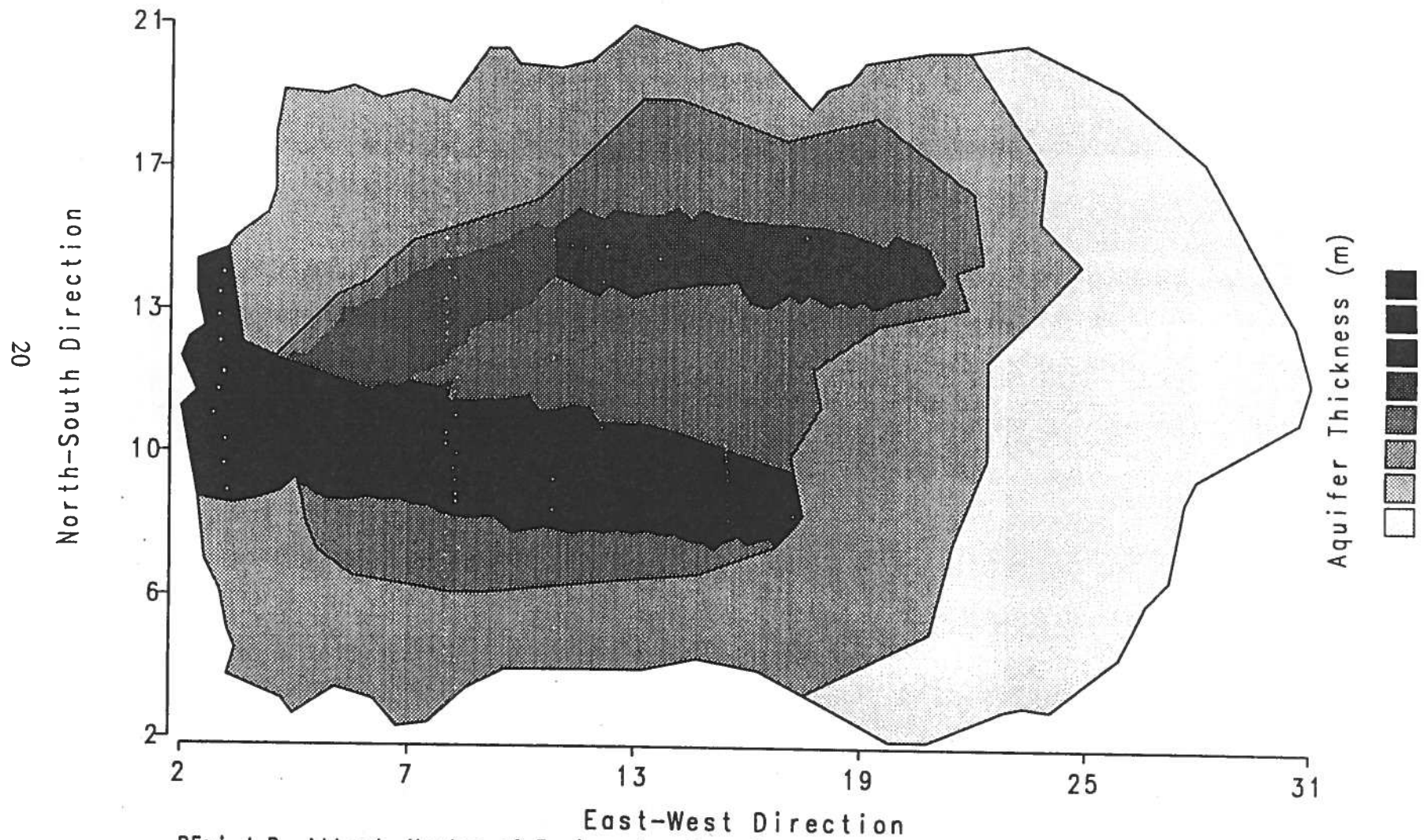


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# WUSHI VALLEY AQUIFER

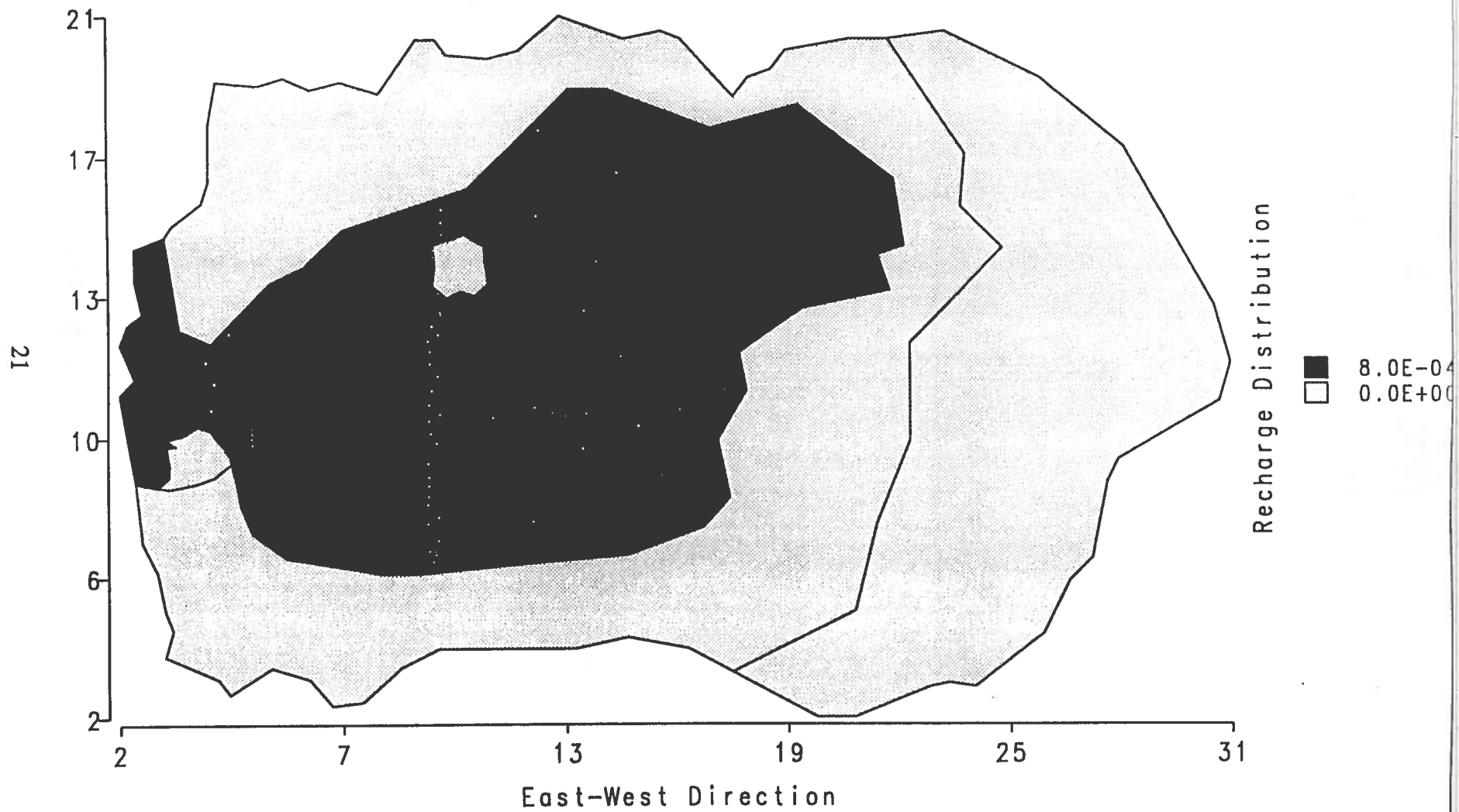


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FIGURE 10

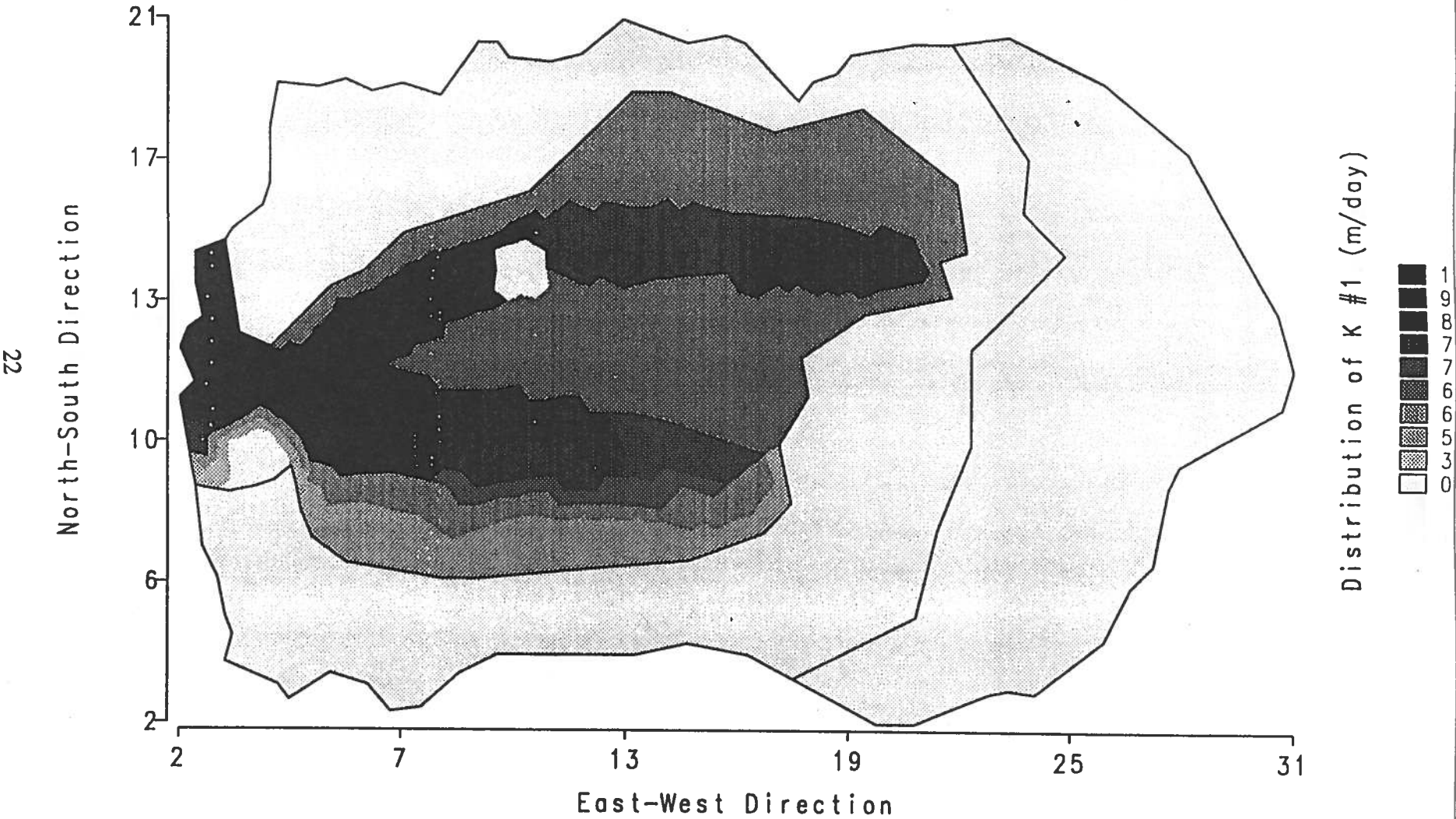
# WUSHI VALLEY AQUIFER



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WUSHI VALLEY AQUIFER

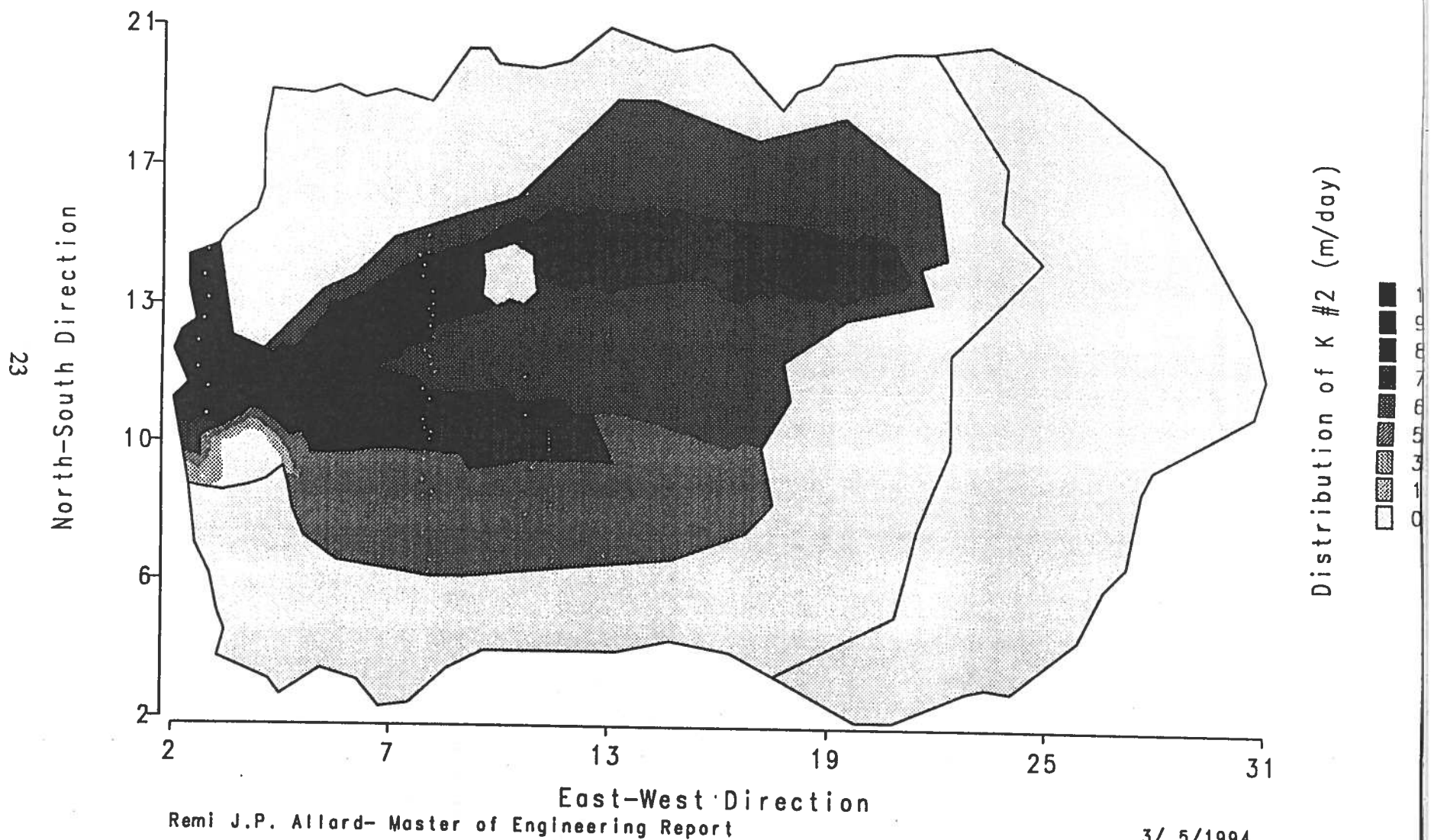


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FIGURE 12

# WUSHI VALLEY AQUIFER





## 8.0 CALIBRATION OF THE MODEL

Calibration of the model is desired based in this case on a steady state solution with both mass balance and iterative closure of predicted heads. The calibration is not successful.

The best calibration run for the model is based on mass balance considerations and is in error by 10 %, with inflows exceeding outflows. This is due to the flux boundary along the interface between the upper recharge area and the lower active aquifer. The intent is to set the total amount of flux across the boundary equal to the total recharge which would have accumulated in the upper recharge area at the vertical flux rate assigned to the lower active area. Individual nodal heads are set at the lowest possible elevation without running dry. However, the flux could not be reduced sufficiently enough to provide a lower total flux across the boundary and still keep the upper recharge area saturated. A higher degree of discretization along this boundary may reduce this problem. The resulting distribution of heads is shown in Figure 15, and in general shows good agreement with observed heads. Large errors occur between calculated and predicted head ( $> 30$  m) around the base of Moku Hill and Bogunda Hill. Most head values are slightly above the upper level of the aquifer for this balance to occur. This suggests confined or semi-confined aquifer conditions exist at many locations throughout the aquifer.

Calibration of the model with respect to heads is not successful. The solution is based on a steady state vertical flux (recharge rate) averaged from the cumulative annual precipitation data for the area. This caused problems as, for the majority of the year, the recharge rate is much lower than the average calculated for the year. As the recharge rate is very difficult to determine, the assigned value is chosen on an arbitrary basis. The result in model runs is that high confined pressures are generated along the steeper slopes in the model domain. The AQUIFEM-1 code does not have the ability to recognize these areas as potential seepage faces. To release the pressure at these points, rising ground water level nodes are established. The identification of these areas seemed never ending and when most had been found and the appropriate ground levels set, the mass balance is in error and the resultant plot of predicted heads is not in good agreement with the observed heads. The best run based on distribution of heads had a maximum error of 5.8 m. The plot of head distribution based on iterative closure of heads is presented in Figure 16.

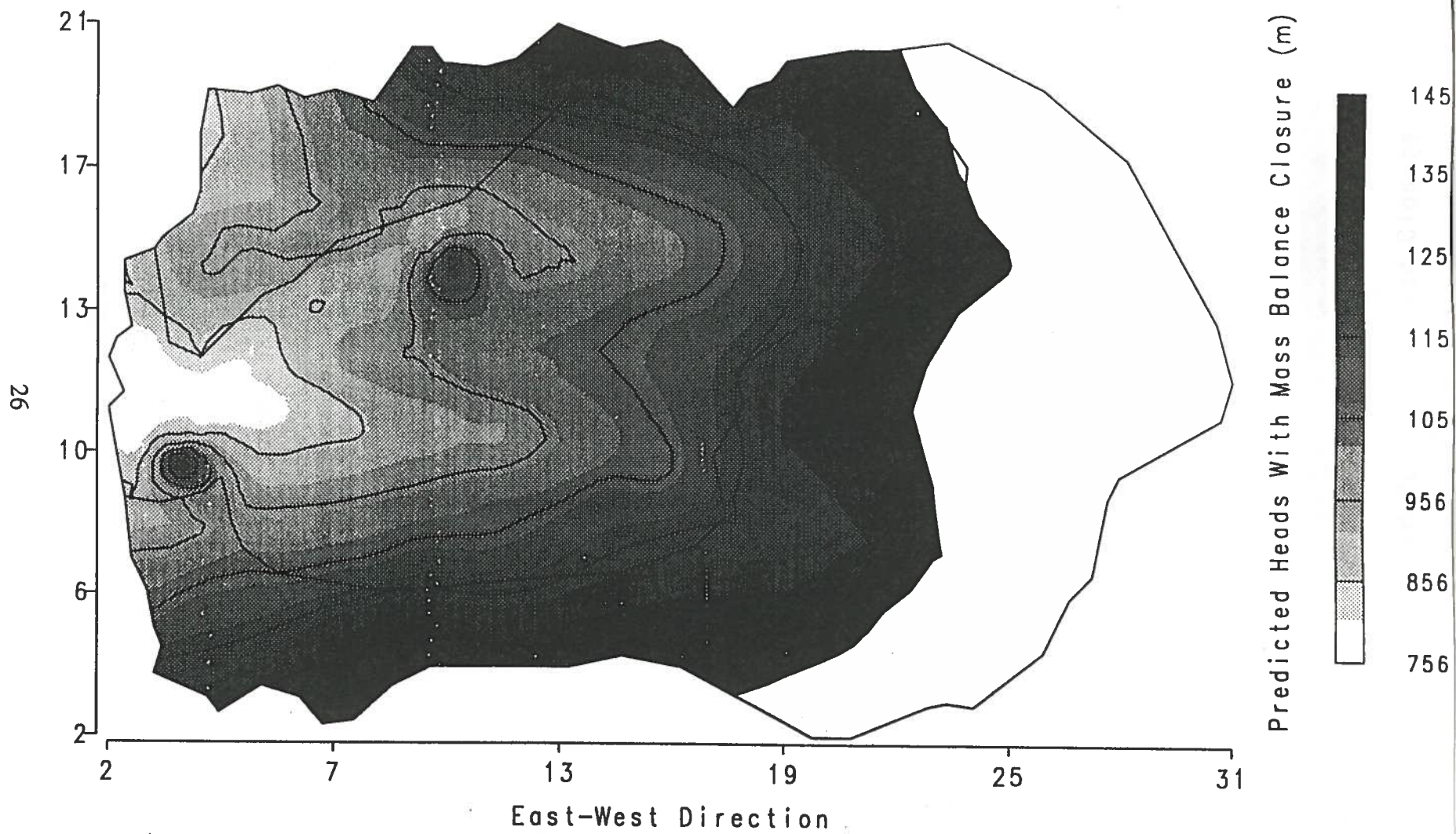
## 9.0 SENSITIVITY ANALYSIS

The model, although not calibrated sufficiently to permit verification, is tested to determine sensitivity to variations in input parameters. The parameters tested for sensitivity include hydraulic conductivity, boundary conditions, and recharge rate. The model is found to be most sensitive to changes in hydraulic conductivity, particularly changes in the lower reaches of the model domain (lower Wushi). Less sensitive are the fixed heads along the lower fixed head boundary along the Jawi River. The vertical recharge flux in the lower model area is still less sensitive and least sensitive is the horizontal flux across the interface between the upper recharge area and the lower active area. A summary of the sensitivity analysis is presented in Table 4.

**TABLE 4**  
**SUMMARY OF SENSITIVITY ANALYSIS**

| Scenario                                  | Head<br>Node 49<br>(m) | Head<br>Node 384<br>(m) | Head<br>Node 628<br>(m) | Head<br>Node 1018<br>(m) | Mass<br>Balance<br>(m <sup>3</sup> /day) |
|---|------------------------|-------------------------|-------------------------|--------------------------|--|
| Control Scenario                          | 791.0                  | 911.92                  | 962.2                   | 1227                     | 12419                                    |
| Lower Upper<br>Recharge Boundary<br>0.2 m | 790                    | 910                     | 953                     | 1221                     | 12870                                    |
| Lower Upper<br>Recharge Boundary<br>1.0 m | 790                    | 910                     | 953                     | 1221                     | 12973                                    |
| Set Upper Recharge<br>to K=0.007          | 790                    | 910                     | 953                     | 1221                     | 12972                                    |
| Set Vertical Recharge<br>to 0.00435       | 790                    | 910                     | 953                     | 1222                     | 6573                                     |
| Set Region 6 to K=<br>120                 | 793                    | 912                     | 960.7                   | 1227                     | 15320                                    |
| Set Region 7 to K=90                      | 791                    | 911.9                   | 962.2                   | 1224                     | 16652                                    |

# WUSHI VALLEY AQUIFER

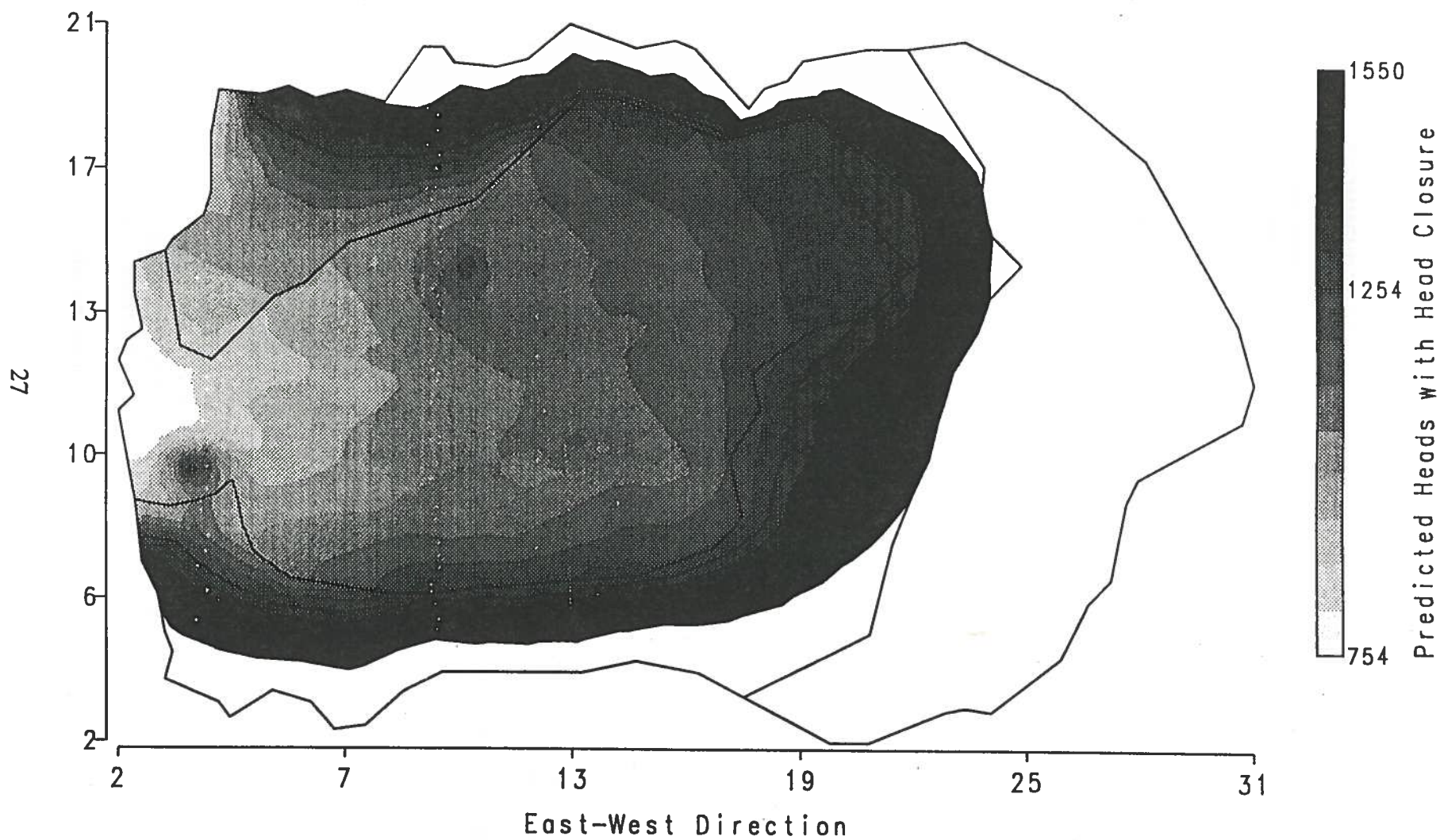


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## 10.0 CONCLUSIONS AND RECOMMENDATIONS

This Study is undertaken to demonstrate a basic understanding and working knowledge of the principles of groundwater modelling studied at the master's level in engineering. The task of developing and calibrating a model is not completely fulfilled. However, the author has gained valuable experience in the methodology of modelling through conceptualization, discretization, parameter estimation, calibration and documenting the exercise.

A simple summary of the effort is as follows:

- the model could not be calibrated sufficiently well enough to permit transient simulations;
- limited data is available for establishing input parameters and for calibration;
- large elevation differences across individual elements caused problems which could be overcome by a higher degree of discretization;
- the upper recharge area could have been eliminated from the model and represented by an exterior boundary condition. This was not realized until after calibration efforts commenced;
- the establishment of fixed head boundaries atop the volcanic cones does not appear to be conceptually correct. At locations where the topography becomes excessively high to rise above the top elevation of the aquifer, a 'hole' in the finite element mesh should appear, with a no flow condition fixed along the boundary;
- in the original conceptual model, no consideration is given to rising ground water level nodes along the rivers and for seepage faces. By graphically analyzing the model output with the assistance of GRIDBUILDER, it is easy to identify areas where heads accumulated anomalously and to investigate these areas in greater detail. In doing so, the modelling process is an exercise in the study of flow processes and understanding the hydrogeological regime of the basin;
- an increase in the number of elements, and a finer discretization in critical areas of the model, domain would reduce errors caused by large element aspect ratios and vertical flow gradients;
- a vertical-profile model or unsaturated-saturated flow model is recommended as an alternative to the 2-dimensional areal model utilized in this study;
- the difficulty in calibrating the model illustrates the requirement for more detailed field investigations to determine aquifer parameters and the spatial variability across the basin.
- additional information required to more accurately model the Wushi Basin includes:
  - many more (at least 10) static water level monitoring points, particularly in the upper reaches of the Yangari River and in the higher elevation areas .
  - 20 or 30 additional testholes to determine lithology and aquifer thickness.
  - hydraulic conductivity (or transmissivity) values from pumping tests, falling head tests and estimates from sieve analysis for 10 more locations; and
  - more detailed river flow and climatic data for the area.

## 11.0 ACKNOWLEDGEMENTS

Following completion of course work, the author accepted a position as managing hydrogeologist on a feasibility study for establishing the potential of utilizing shallow aquifers for irrigation in Borno State, Nigeria. Independent of the project, the author undertook field work on the Wushi River Basin within the state for personal interest. Upon returning to Canada, the idea of constructing and calibrating a model of the basin was proposed to the author's academic advisor, Dr. Al Woodbury, P.Eng., as a Master of Engineering project.

In undertaking this work the author has been assisted by many people with their valuable time, effort and patience. Most importantly gratitude is offered to Dr. Woodbury, who patiently waited for 3 years for completion of this work while the author was working overseas. Gratitude is also extended to fellow students, Dave Farrell and Steve Weicek who worked on other projects of similar scope and whose technical assistance was invaluable. Ingrid Trestrail from the Geological Engineering Department has also been very helpful. My thanks also go to my wife Pina and my employer, Wardrop Engineering, who have tolerated my alternating spells of hard work and laziness throughout this task.

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## **APPENDICES**

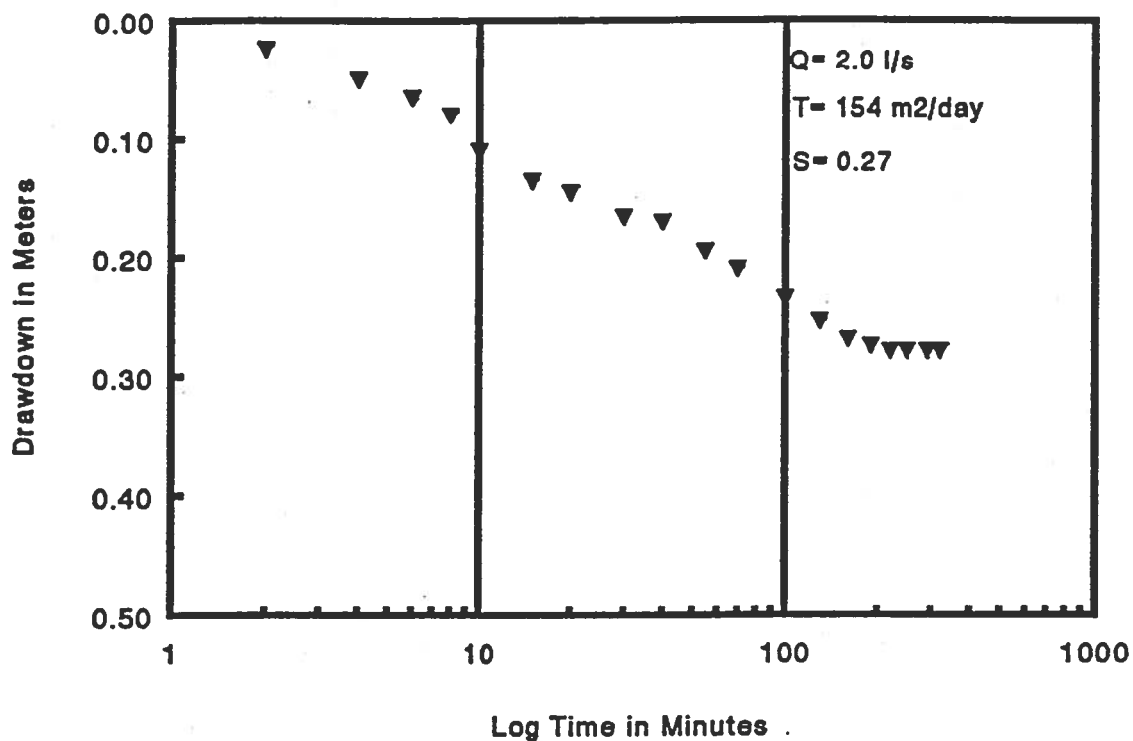
## **APPENDIX A**

# TESTHOLE LOG SUMMARY

| NODE                | NAME        | DEPTH   | UNIT                                     | DESCRIPTION   |
|---------------------|-------------|---|--|---|
| 628<br>(9.3,10.1)   | PETA        | 0.0 - 0.4<br>0.4 - 1.0<br>1.0 - 2.3<br>2.3 - 4.5<br>4.5 - 5.0 | CLAY<br>SAND<br>SAND<br>GRAVEL<br>GRAVEL | brown, firm, iron staining, some organics, damp<br>medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, loose, moist<br>well graded, brown to black, loose, wet<br>well graded, brown to black, occasional rock fragments, loose, wet |
| 1018<br>(20.5,14.4) | WADA        | 0.0 - 0.9<br>0.9 - 2.2<br>2.2 - 3.0                           | CLAY<br>SAND<br>SAND                     | brown, soft to firm , dry<br>medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, loose, wet  |
| 1102<br>(17.1,8.2)  | UNNAMED     | 0.0 - 0.75  | GRAVEL                                   | well graded, brown to black, occasional rock fragments, loose, wet  |
| 683<br>(8.4,9.3)    | RIBADO      | 0.0 - 0.4<br>0.4 - 0.8<br>0.8 - 2.0<br>2.3 - 3.8              | CLAY<br>SAND<br>SAND<br>GRAVEL           | brown, firm, iron staining, some organics, damp<br>medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, loose, moist<br>well graded, brown to black, loose, wet   |
| 384<br>(6.4,10.1)   | KUNALLENG   | 0.0 - 0.4<br>0.4 - 1.7<br>1.7 - 2.8<br>2.8 - 4.5<br>4.5 - 5.6 | CLAY<br>SAND<br>SAND<br>GRAVEL<br>GRAVEL | brown, firm, iron staining, some organics, damp<br>medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, loose, moist<br>well graded, brown to black, loose, wet<br>well graded, brown to black, occasional rock fragments, loose, wet |
| 49<br>(2.9,10.9)    | BILAZI      | 0.0 - 0.7<br>0.7 - 2.2<br>2.2 - 6.2                           | SAND<br>SAND<br>GRAVEL                   | medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, loose, moist<br>well graded, brown to black, loose, wet  |
| 815<br>(13.8,9.4)   | KUMTOR      | 0.0 - 0.8<br>0.8 - 1.2<br>1.2 - 2.0<br>2.0 - 4.5              | CLAY<br>SAND<br>SAND<br>GRAVEL           | brown, firm, iron staining, some organics, damp<br>medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, loose, moist<br>well graded, brown to black, loose, wet   |
| 111<br>(5.5,16.3)   | BAHAI       | 0.0 - 0.4<br>0.4 - 0.9<br>0.9 - 1.3<br>1.3 - 1.5              | CLAY<br>SAND<br>SAND<br>ROCK             | brown, firm, iron staining, some organics, damp<br>medium grained, well graded,brown, occasional rock fragments, loose, wet<br>medium grained, well graded,brown, loose, wet<br>black, weathered, hard  |
| 831<br>(11.4,6.9)   | KUMTOR/BULA | 0.0 - 0.3<br>0.3 - 1.9<br>1.9 - 4.8<br>4.8 - 4.9              | CLAY<br>SAND<br>SAND<br>ROCK             | brown, firm, iron staining, some organics, damp<br>medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, loose, moist<br>black, weathered, hard  |
| 39<br>(3.1,13.0)    | LESSGA      | 0.0 - 0.4<br>0.4 - 2.7<br>2.2 - 3.0<br>3.0 - 3.1              | SAND<br>SAND<br>SAND<br>ROCK             | medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, occasional rock fragments, loose, wet<br>medium grained, well graded,brown, loose, wet<br>black, weathered, hard   |
| 567<br>(8.0,10.0)   | KUNALLENG   | 0.0 - 0.4<br>0.4 - 1.7<br>1.7 - 2.8<br>2.8 - 4.5<br>4.5 - 5.6 | CLAY<br>SAND<br>SAND<br>GRAVEL<br>GRAVEL | brown, firm, iron staining, some organics, damp<br>medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, loose, moist<br>well graded, brown to black, loose, wet<br>well graded, brown to black, occasional rock fragments, loose, wet |
| 205<br>(6.6,16.3)   | JAURO YAYA  | 0.0 - 0.4<br>0.4 - 2.7<br>2.2 - 3.0<br>3.0 - 3.1              | SAND<br>SAND<br>ROCK                     | medium grained, well graded,brown, compact, damp<br>medium grained, well graded,brown, occasional rock fragments, loose, wet<br>black, weathered, hard  |

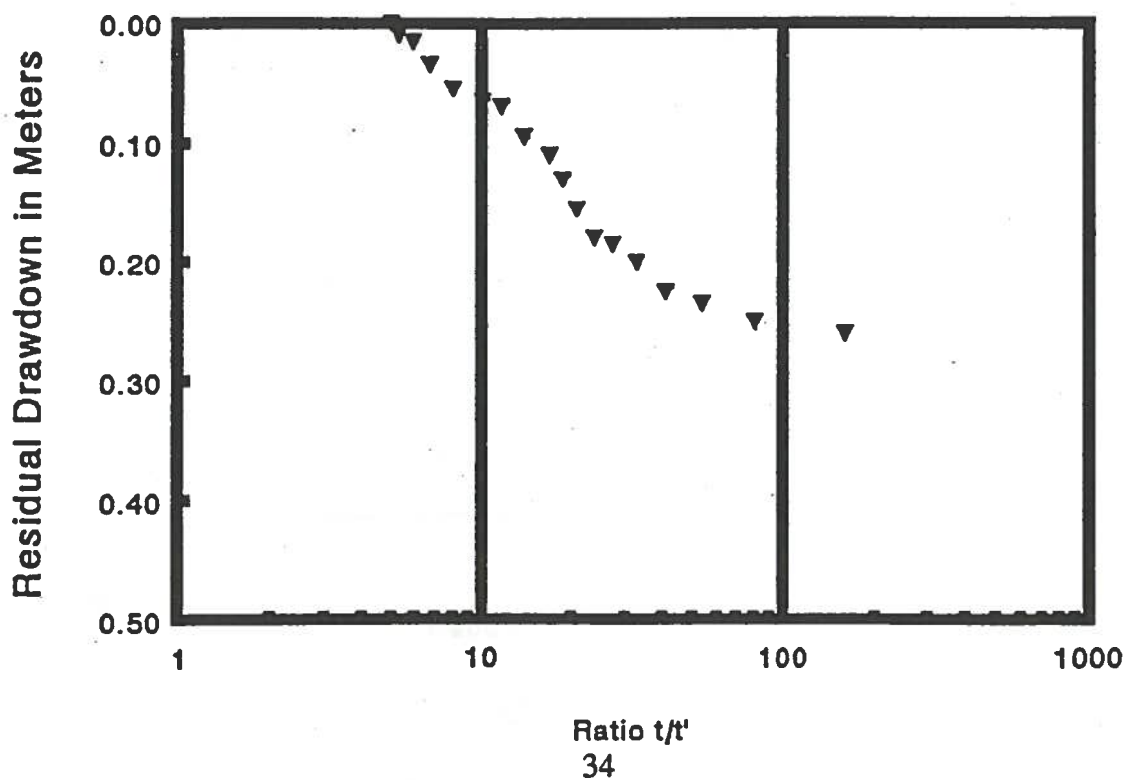
# WUSHI PUMPING TEST

## Observation Well Measurements, $r = 2\text{m}$



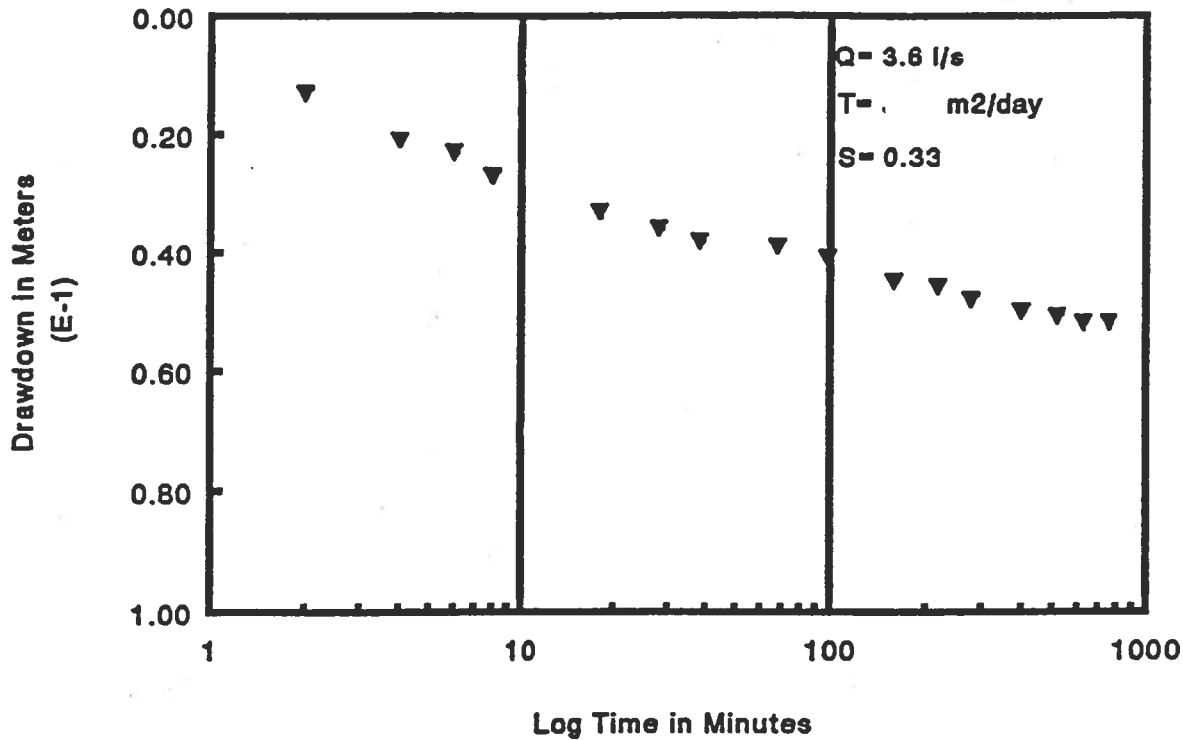
# WUSHI RECOVERY TEST

## Observation Well at $R = 2.0 \text{ m}$



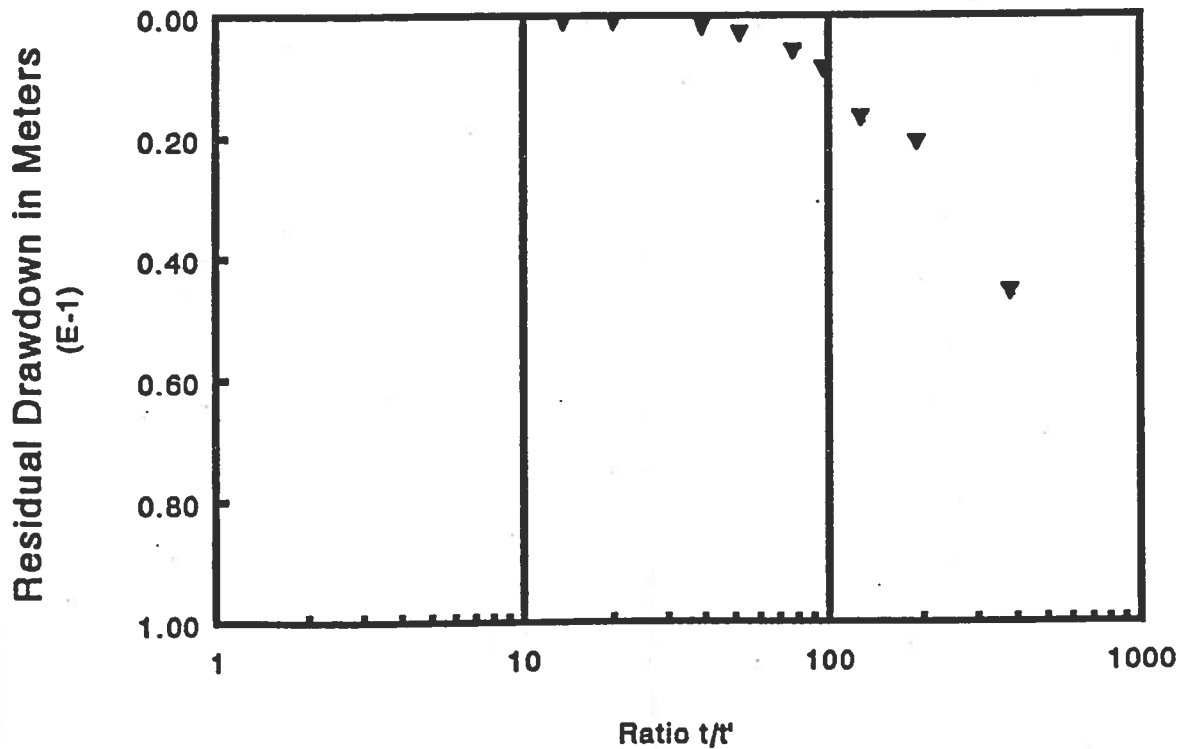
# BILAZI PUMPING TEST

Observation Well Measurements,  $r = 1.5\text{m}$



# BILAZI RECOVERY TEST

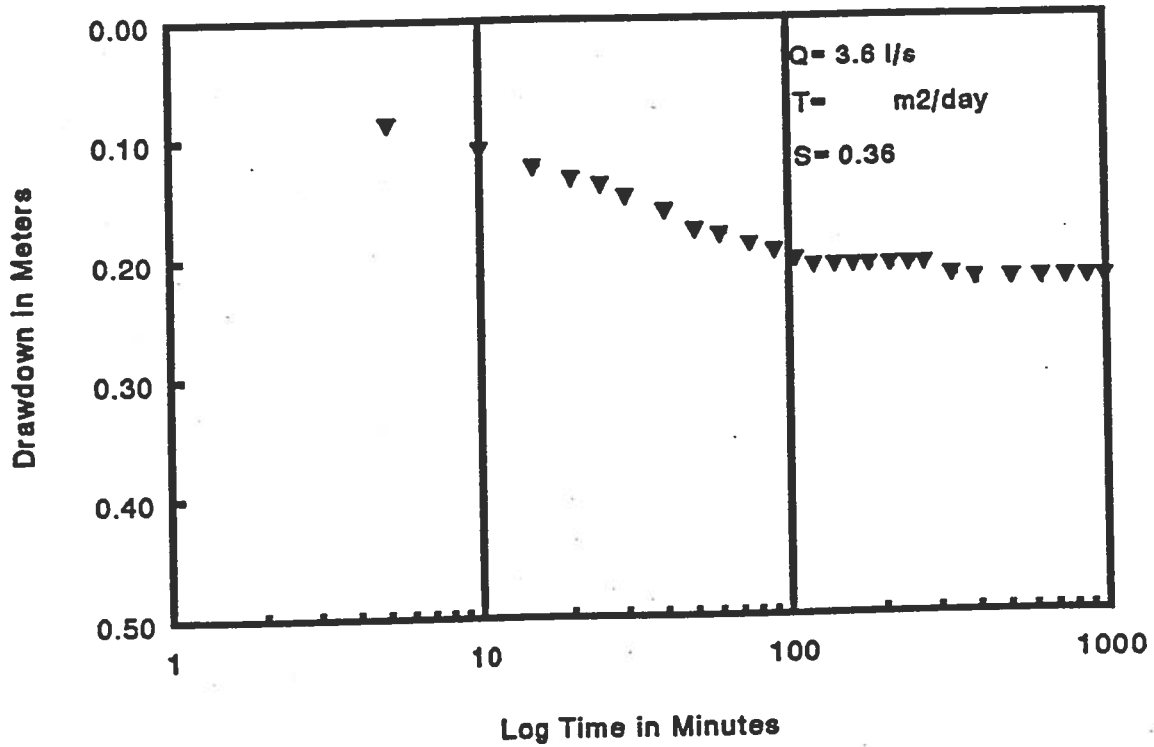
Observation Well at  $R = 1.5 \text{ m}$





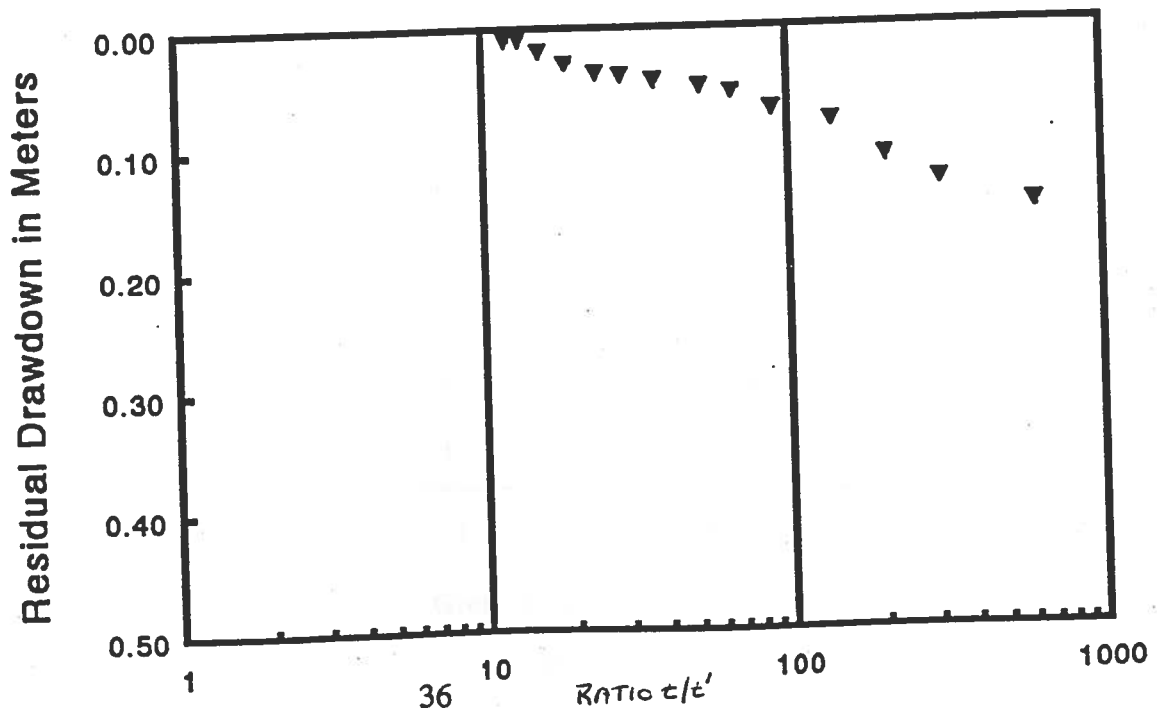
# PETA PUMPING TEST

Observation Well Measurements,  $r = 3\text{m}$

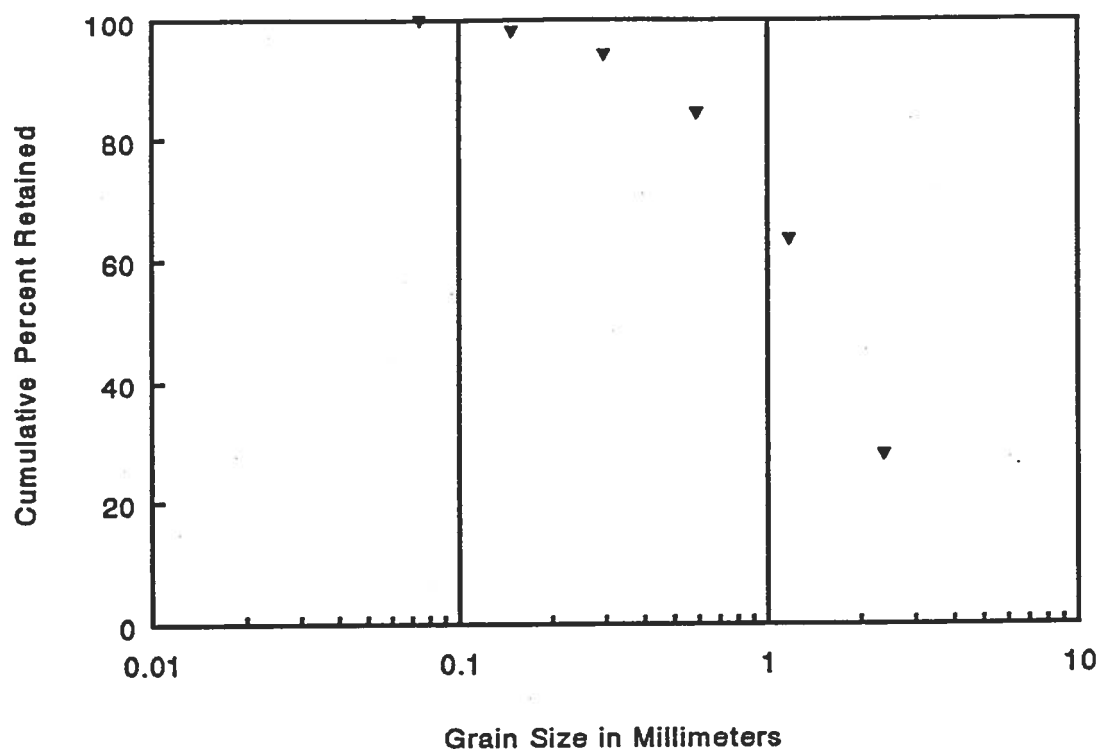


# PETA RECOVERY TEST

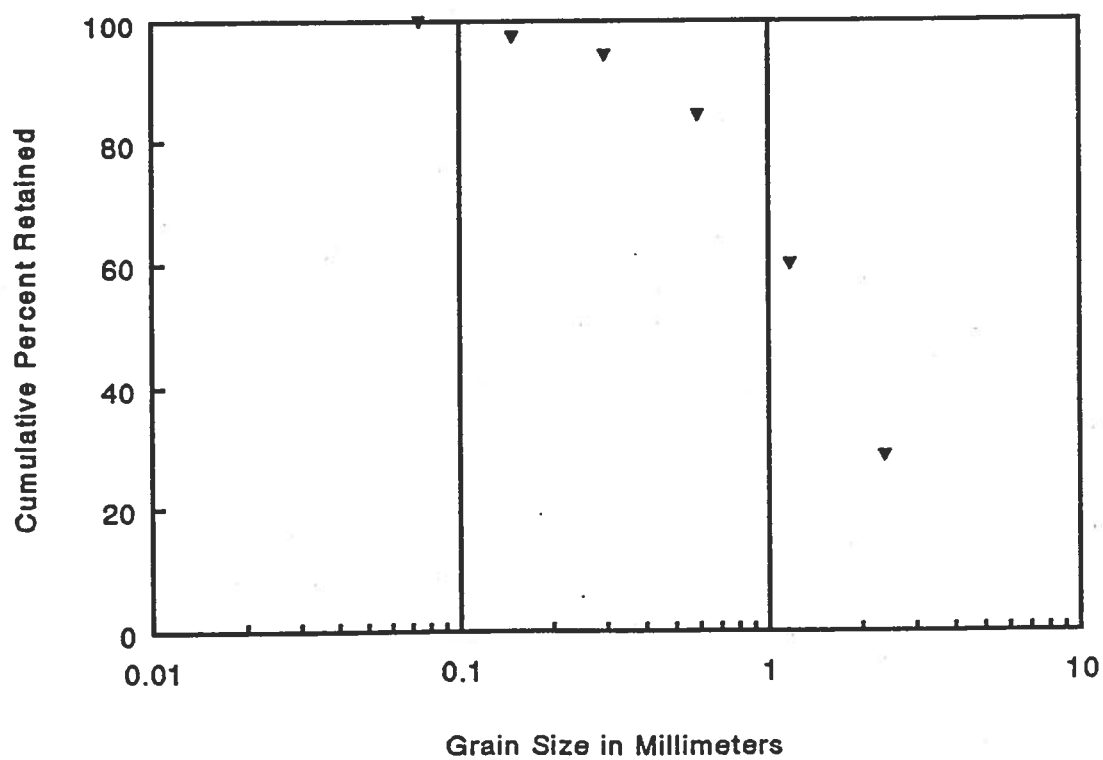
Observation Well at  $R = 3.0 \text{ m}$



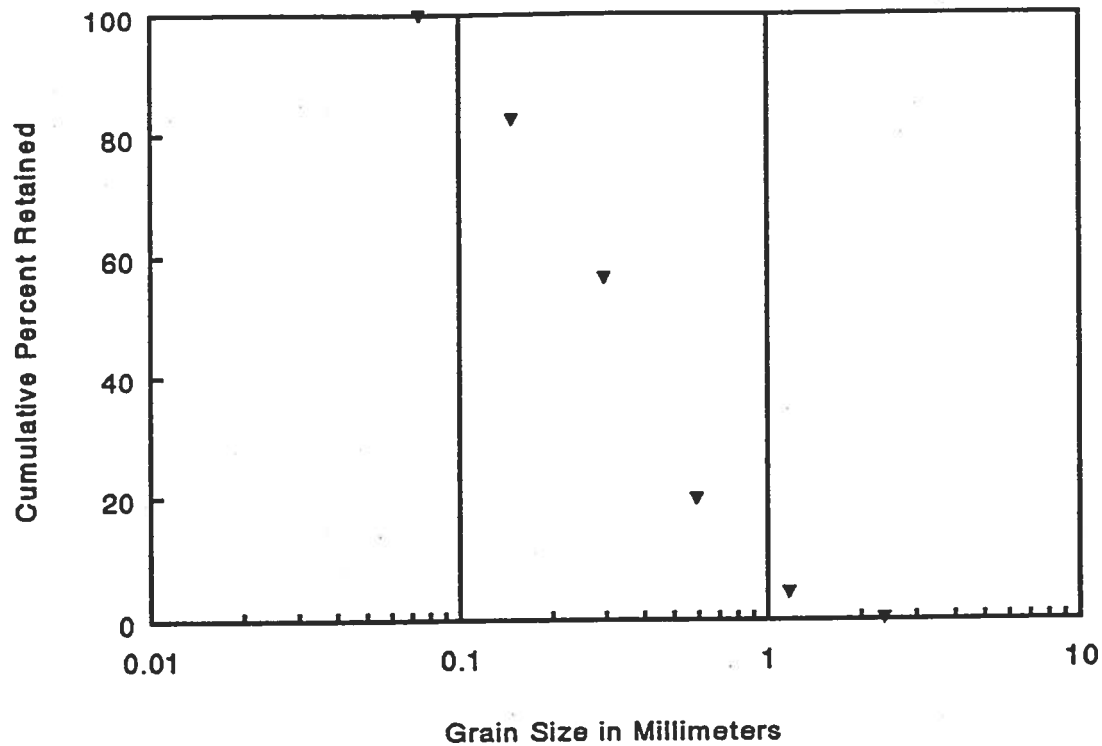
## PETA #1 SAMPLE SIEVE ANALYSIS



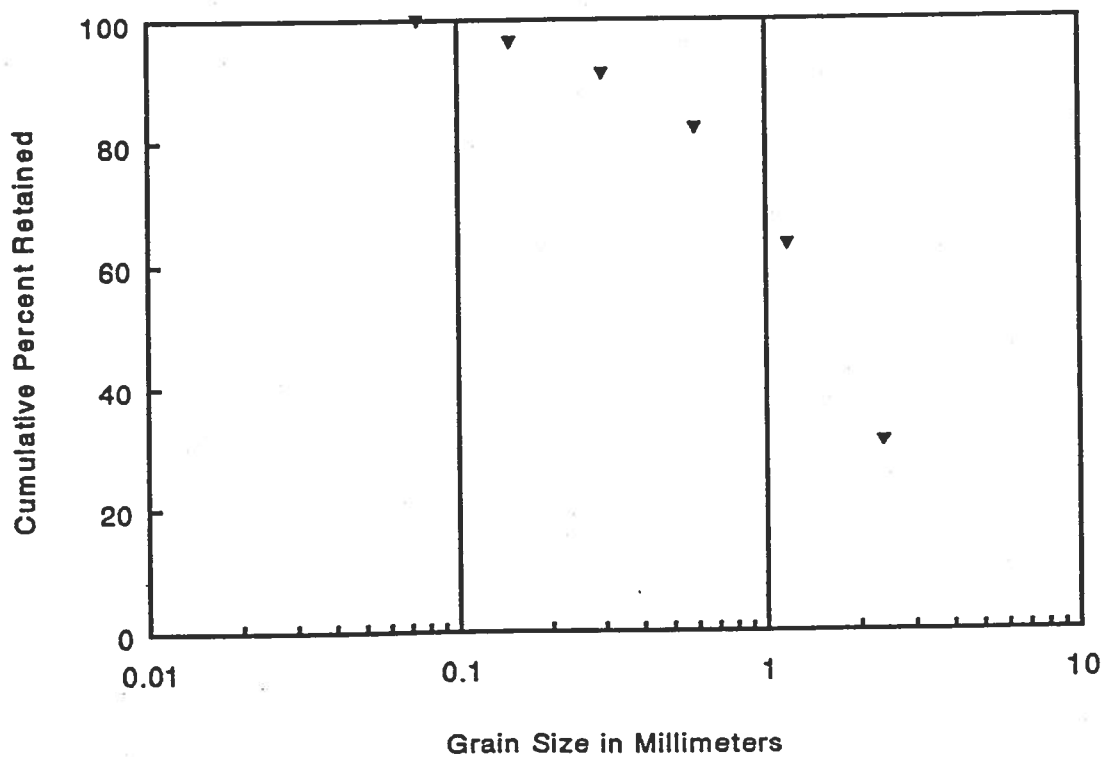
## PETA #2 SAMPLE SIEVE ANALYSIS



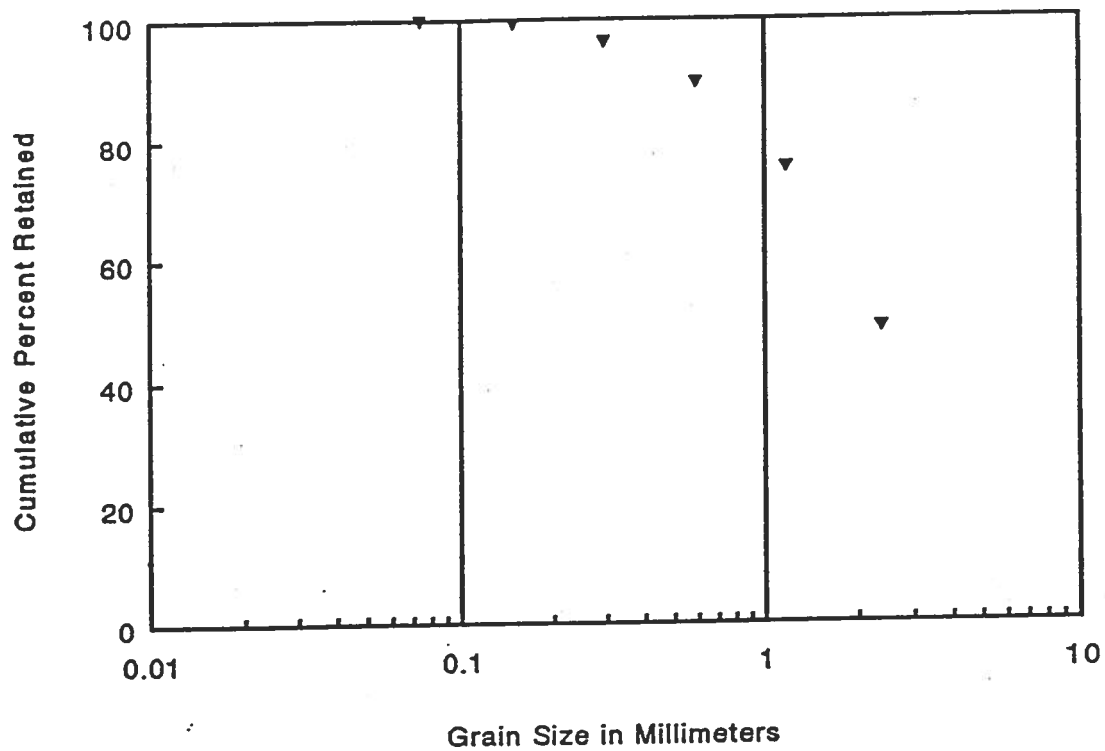
## BILAZI #1 SAMPLE SIEVE ANALYSIS



## BILAZI #2 SAMPLE SIEVE ANALYSIS



## BILAZI #3 SAMPLE SIEVE ANALYSIS



## APPENDIX B

# WUSHI VALLEY AQUIFER

## Discretization of Elements

Title block - line 3

| T            | I Plan-view/cross-section         |
|--------------|-----------------------------------|
| 1187         | I Number of nodes                 |
| 2272         | I Number of elements              |
| 65           | I Bandwidth                       |
| 3            | I Number of areas                 |
| 1.60000      | I Grid X minimum                  |
| 31.0000      | I Grid X maximum                  |
| 2.20000      | I Grid Y minimum                  |
| 20.6000      | I Grid X maximum                  |
| 1.60000      | I Screen X minimum                |
| 31.1632      | I screen X maximum                |
| 2.20000      | I screen Y minimum                |
| 21.6733      | I screen X maximum                |
| 12.9891      | I Screen-user x-scale             |
| 107.217      | I Screen-user x-translate         |
| 12.2732      | I Screen-user y-scale             |
| 68.9989      | I Screen-user y-translate         |
| 1.00000      | I Character size in x             |
| 0.800000     | I Character size in y             |
| 1.000000E-02 | I Mouse precision in x            |
| 1.000000E-02 | I Mouse precision in y            |
| 1.00000      | I Plotted output scale            |
| 0.000000E+00 | I Plotted output horizontal shift |
| 0.000000E+00 | I Plotted output vertical shift   |

(F10.1)

(F10.1)

|          |                                |
|----------|--------------------------------|
| 1.60000  | I X-axis start                 |
| 31.0000  | I X-axis end                   |
| 5.88000  | I X-axis increment             |
| 2.01600  | I X-axis y-placement           |
| 0.220800 | I X-axis tic length            |
| 1.28000  | I X-axis tic label y-placement |
| 0.800000 | I X-axis tic label size        |

(I10)

East-West Direction

|          |                                |
|----------|--------------------------------|
| 16.3000  | I X-axis label x-placement     |
| 0.176000 | I X-axis label y-placement     |
| 0.800000 | I X-axis label size            |
| 2.20000  | I Y-axis start                 |
| 20.6000  | I Y-axis end                   |
| 3.68000  | I Y-axis increment             |
| 1.30600  | I Y-axis x-placement           |
| 0.294000 | I Y-axis tic length            |
| 1.12960  | I Y-axis tic label x-placement |
| 0.800000 | I Y-axis tic label size        |

(I10)

North-South Direction

|          |                            |
|----------|----------------------------|
| -1.34000 | I Y-axis label x-placement |
| 11.4000  | I Y-axis label y-placement |
| 0.800000 | I Y-axis label size        |

|         |         |         |         |         |         |              |
|---------|---------|---------|---------|---------|---------|--------------|
| 1.60000 | 24.2800 | 1.60000 | 21.5200 | 1.60000 | 20.7840 | I X,Y titles |
|---------|---------|---------|---------|---------|---------|--------------|

|  |           |          |                                 |
|--|-----------|----------|---------------------------------|
| 1.00000  | 0.900000  | 0.900000 | ! X,Y title sizes               |
| REmi J.P. Allard- Master of Engineering Report |           |          |                                 |
| 1.60000  | -0.560000 | !        | Company name placement          |
| 0.600000                                       | !         |          | Company name size               |
| 27.4720  | -0.560000 | !        | Date placement                  |
| 0.600000                                       | !         |          | Date size                       |
| 1.60000  | 22.4400   | !        | Field name placement            |
| 0.800000                                       | !         |          | Field name size                 |
| 0.500000                                       | !         |          | Field labels size               |
| (F10.1)  |           |          |                                 |
| 1.60000  | 21.5200   | !        | Vector name placement           |
| 0.500000                                       | !         |          | Vector name size                |
| (1PE10.2)                                      |           |          |                                 |
| 1.60000  | 22.4400   | !        | Head name placement             |
| 1.60000  | 21.5200   | !        | Stream name placement           |
| 0.500000                                       | !         |          | Head, stream name size          |
| 35.4100  | 11.4000   | !        | Property name placement         |
| 0.800000                                       | !         |          | Property name size              |
| 90.0000  | !         |          | Property name angle             |
| (F10.2)  |           |          |                                 |
| (F10.2)  |           |          |                                 |
| 3.46020  | !         |          | colour legend xmin              |
| 9.04516  | !         |          | colour legend ymin              |
| 3.50100  | !         |          | colour legend xmax              |
| 9.68000  | !         |          | colour legend ymax              |
| 3.52140  | !         |          | colour legend label x placement |
| 0.700000                                       | !         |          | colour legend label size        |
| (I10)  |           |          |                                 |
| 3.46020  | !         |          | fill legend xmin                |
| 9.04516  | !         |          | fill legend ymin                |
| 3.50100  | !         |          | fill legend xmax                |
| 9.68000  | !         |          | fill legend ymax                |
| 3.52140  | !         |          | fill legend label x placement   |
| 0.700000                                       | !         |          | fill legend label size          |
| (I10)  |           |          |                                 |
| (F10.2)  |           |          |                                 |
| (1PE10.1)                                      |           |          |                                 |
| (F10.2)  |           |          |                                 |
| 0.800000                                       |           |          |                                 |
| 0.550000                                       |           |          |                                 |
| (F10.2)  |           |          |                                 |
| T  | !         |          | Plot outer boundary             |
| T  | !         |          | Plot area boundaries            |
| T  | !         |          | Plot elements                   |
| F  | !         |          | Plot element numbers            |
| F  | !         |          | Plot elements shrunken          |
| F  | !         |          | Plot nodes                      |
| F  | !         |          | Plot node numbers               |
| T  | T         | F        |                                 |
| T  | !         |          | Plot x-axis                     |
| T  | !         |          | Plot x-axis label               |
| T  | !         |          | Plot y-axis                     |
| T  | !         |          | Plot y-axis label               |
| T  | !         |          | Plot date                       |



T I Plot company name

Boundary data

22 first-type nodes

|     |         |
|-----|---------|
| 1   | 5.47717 |
| 3   | 5.51873 |
| 4   | 5.43241 |
| 8   | 5.56029 |
| 9   | 5.38765 |
| 15  | 5.64341 |
| 16  | 5.34288 |
| 25  | 5.79668 |
| 27  | 5.29812 |
| 36  | 5.21626 |
| 41  | 5.94994 |
| 53  | 5.13439 |
| 60  | 6.08294 |
| 73  | 5.05253 |
| 83  | 6.50000 |
| 87  | 6.35796 |
| 88  | 6.21593 |
| 100 | 4.97067 |
| 127 | 5.05000 |
| 157 | 5.09000 |
| 195 | 5.13000 |
| 233 | 5.22000 |

0 non-zero second-type nodes

0 third-type nodes

Boundary data

22 first-type nodes

|     |         |
|-----|---------|
| 1   | 5.47717 |
| 3   | 5.51873 |
| 4   | 5.43241 |
| 8   | 5.56029 |
| 9   | 5.38765 |
| 15  | 5.64341 |
| 16  | 5.34288 |
| 25  | 5.79668 |
| 27  | 5.29812 |
| 36  | 5.21626 |
| 41  | 5.94994 |
| 53  | 5.13439 |
| 60  | 6.08294 |
| 73  | 5.05253 |
| 83  | 6.50000 |
| 87  | 6.35796 |
| 88  | 6.21593 |
| 100 | 4.97067 |
| 127 | 5.05000 |
| 157 | 5.09000 |
| 195 | 5.13000 |
| 233 | 5.22000 |

0 non-zero second-type nodes

# AQUIFEM-1

TWO DIMENSIONAL FINITE ELEMENT MODEL  
OF GROUNDWATER FLOW WITH  
LINEAR TRIANGULAR ELEMENTS

DEPARTMENT OF CIVIL ENGINEERING  
MASSACHUSETTS INSTITUTE OF TECHNOLOGY  
CAMBRIDGE, MASSACHUSETTS, 02139

NOVEMBER 1979 VERSION

(w3in) - 60,70,80's and .02's, constant head 3e-4

## PROBLEM DESCRIPTION

TYPE OF AQUIFER.....LINEAR= .F.  
LINEAR=.T. LINEAR (CONFINED) OR LINEARIZED AQUIFER  
LINEAR=.F. NONLINEAR (UNCONFINED OR MIXED) AQUIFER

TYPE OF PROBLEM.....STEADY= .T.  
STEADY=.T. STEADY STATE PROBLEM  
STEADY=.F. UNSTEADY OR TRANSIENT PROBLEM

INITIAL CONDITIONS/GUESSES PARAMETER.....INITAL= .F.  
INITAL=.T. COMPUTE LINEAR SOLUTION AS A FIRST GUESS FOR A NONLINEAR PROBLEM  
AND/OR INITIAL STEADY STATE SOLUTION FOR AN UNSTEADY PROBLEM  
INITAL=.F. READ INITIAL CONDITIONS OR GUESSES

FINAL STEADY STATE SOLUTION PARAMETER.....FINAL= .F.  
FINAL=.T. COMPUTE FINAL STEADY STATE SOLUTION WITH BOUNDARY CONDITIONS AT TIME=ENDTIM  
FINAL=.F. DO NOT COMPUTE FINAL STEADY STATE SOLUTION

DATA CHECK PARAMETER.....CHECK= .F.  
CHECK=.T. CHECK DATA THEN STOP  
CHECK=.F. EXECUTE PROGRAM NORMALLY

## FINITE ELEMENT GRID PARAMETERS

NUMBER OF ELEMENTS.....NUMEL= 2272

NUMBER OF NODE POINTS.....NUMNP= 1187

FLAG FOR PRINTING GEOMETRIC DATA.....PRGEOM= .T.  
PRGEOM=.T. PRINT GEOMETRIC DATA  
PRGEOM=.F. DO NOT PRINT GEOMETRIC DATA

FLAG FOR PRINT-PLOTTING GEOMETRIC DATA.....PLGEOM= .T.  
PLGEOM=.T. PLOT GEOMETRIC DATA  
PLGEOM=.F. DO NOT PLOT GEOMETRIC DATA

SCALING FACTOR FOR X-COORDINATES.....XSCALE= 1000.000

SCALING FACTOR FOR Y-COORDINATES.....YSCALE= 1000.000

LARGEST ELEMENT IDENTIFICATION NUMBER.....MAXELT= 2272

LARGEST NODE IDENTIFICATION NUMBER.....MAXNOD= 1187

## AQUIFER PROPERTY PARAMETERS

NUMBER OF REGIONS WITH REGIONALLY DEFINED AQUIFER PROPERTIES.....NAQR= 0

NUMBER OF INDIVIDUAL ELEMENTS OR NODES WITH SPECIALLY DEFINED AQUIFER PROPERTIES.....NSPEC= 2272

METHOD BY WHICH AQUIFER PROPERTIES ARE GIVEN.....BYNODE= .F.  
BYNODE=.T. BY NODES  
BYNODE=.F. BY ELEMENTS

METHOD BY WHICH HYDRAULIC PROPERTIES ARE GIVEN.....PERM= .T.  
PERM=.T. PERMEABILITIES KXX,KYY ARE GIVEN  
PERM=.F. TRANSMISSIVITIES TXX,YY ARE GIVEN

```

1
BOUNDARY CONDITION PARAMETERS
=====
NUMBER OF PRESCRIBED BOUNDARY HEAD NODES.....NHNODE=      281
NUMBER OF TIMES WHEN PRESCRIBED HEAD BOUNDARY CONDITIONS ARE SET.....NTBH=      1
NUMBER OF NODES WHERE GROUND LEVELS ARE SPECIFIED.....NGRD=     190
NUMBER OF TIMES WHEN GROUND LEVELS ARE SET.....NTGRD=      1
NUMBER OF FLUX ELEMENTS.....NFLXE=    2272
NUMBER OF TIMES WHEN PRESCRIBED BOUNDARY FLUXES ARE SET.....NTFLXE=      1
NUMBER OF REGIONS WITH REGIONAL ELEMENT FLUX.....NEFR=       0
NUMBER OF FLUX SIDES.....NFLXS=       0
NUMBER OF TIMES WHEN PRESCRIBED SIDE FLUXES ARE SET.....NTFLXS=      0
NUMBER OF FLUX NODES.....NFLXN=       0
NUMBER OF TIMES WHEN PRESCRIBED NODE FLUXES ARE SET.....NTFLXN=      0

NUMBER OF 3RD-TYPE BOUNDARY SIDES.....NBC3=       0
NUMBER OF TIMES WHEN 3RD-TYPE BOUNDARY HEADS ARE SET.....NTBC3=      0
NUMBER OF NODES ON THE 3RD-TYPE BOUNDARY SIDES.....NNO03=      0
3RD-TYPE BOUNDARY PARAMETER.....BEDBC3=      .F.
  BEDBC3=.T.  USE RIVER BED LEVELS TO MODIFY 3RD-TYPE INFLOWS
  BEDBC3=.F.  DO NOT USE RIVER BED LEVELS

NUMBER OF NODES WHERE HEADS IN ADJACENT AQUIFER ARE GIVEN.....NHADJ=      0
NUMBER OF TIMES WHEN HEADS IN ADJACENT AQUIFER ARE SET.....NTHADJ=      0
ADJACENT AQUIFER PARAMETER.....ATTOP=      .F.
  ATTOP=.T.  ADJACENT AQUIFER IS ABOVE AQUIFER UNDER STUDY
  ATTOP=.F.  ADJACENT AQUIFER IS NOT AT TOP

METHOD OF SUPPLYING ADJACENT HEADS.....HAVARY=      .F.
  HAVARY=.T.  ADJACENT HEADS VARY IN SPACE
  HAVARY=.F.  ADJACENT HEADS ARE CONSTANT

TYPE OF INITIAL CONDITIONS/GUESSES IF INITIAL=.F.....ICVARY=      .T.
  ICVARY=.T.  INITIAL CONDITIONS VARY IN SPACE
  ICVARY=.F.  INITIAL CONDITIONS ARE CONSTANT

```

```

1
SOLUTION STRATEGY
=====
START TIME.....STRTIM=    0.0000
END TIME.....ENDTIM=    0.0000
TOLERANCE FOR CONVERGENCE.....TOL=    5.0000
INDICATOR FOR CONVERGENCE CRITERION.....ITOL=      1
  ITOL=0  ROOT MEAN SQUARE ERROR CRITERION
  ITOL=1  MAXIMUM ABSOLUTE ERROR CRITERION
MAXIMUM NUMBER OF ITERATIONS.....MAXIT=    30
TIME STEP.....DT=    0.00000
ALPHA PARAMETER FOR TIME INTEGRATION SCHEME.....ALPHA=    0.5000
TIME STEP PARAMETER.....DTPARM=    0.0000
INDICATOR FOR CHANGING TIME STEP.....IDT=      0
  IDT=0  NO CHANGE OF TIME STEP
  IDT=1  DT=DT*DTPARM AFTER NDT TIME STEPS
  IDT=2  DT=DT+DTPARM AFTER NDT TIME STEPS
NUMBER OF CONSTANT LENGTH TIME STEPS BEFORE CHANGING ACCORDING TO IDT.....NDT=      1
NUMBER OF ITERATIONS WITH SAME LEFT HAND SIDE SYSM MATRIX.....NSYS=      1
  NSYS=999  REFORM SYSM ONCE EACH TIME STEP

```

1  
OUTPUT CONTROL  
=====

FIRST TIME STEP FOR PRINTED OUTPUT.....ISTPRT= 0  
NUMBER OF TIME STEPS BETWEEN PRINTED OUTPUTS.....NDTPRT= 1  
NUMBER OF SPECIAL PRINTED OUTPUT TIMES.....NOUT= 0  
FIRST TIME STEP FOR PLOTTED OUTPUT.....ISTPLT= 1000000  
NUMBER OF TIME STEPS BETWEEN PLOTTED OUTPUTS.....NDTPLT= 1  
NUMBER OF SPECIAL PLOTTED OUTPUT TIMES.....NPLT= 0  
PLOT SCALING FACTOR.....PSCALE= 1000.00  
INCREMENT FOR LABELLING PLOT AXES.....PDELTA= 0.00  
ROTATION PARAMETER.....NRFLAG= 1  
NRFLAG=0 ROTATION OF PLOT IS ALLOWED  
NRFLAG=1 NO ROTATION IS ALLOWED, X-AXIS ACROSS THE PAGE  
NRFLAG=2 ROTATION IS FORCED, Y-AXIS ACROSS THE PAGE  
NUMBER OF ROWS/COLUMNS AROUND PLOT BOUNDARY.....NBOUND= 3  
NUMBER OF DECIMAL PLACES IN PLOTTED VALUES OF HEAD.....NDP= 1

NODE POINT COORDINATES  
=====

| NODE | X     | Y      | NODE | X     | Y      | NODE | X     | Y      | NODE | X     | Y      | NODE | X     | Y      |
|------|-------|--------|------|-------|--------|------|-------|--------|------|-------|--------|------|-------|--------|
| 1    | 1800. | 12500. | 2    | 1941. | 12384. | 3    | 1900. | 12575. | 4    | 1750. | 12375. | 5    | 2160. | 12212. |

ELEMENT ARRAY  
=====

| ELEMENT | I   | J   | K   | ELEMENT | I   | J   | K   | ELEMENT | I   | J   | K   | ELEMENT | I   | J   | K   |
|---------|-----|-----|-----|---------|-----|-----|-----|---------|-----|-----|-----|---------|-----|-----|-----|
| 1       | 556 | 506 | 505 | 2       | 556 | 557 | 506 | 3       | 557 | 558 | 506 | 4       | 557 | 611 | 558 |
|         |     |     |     |         |     |     |     |         |     |     |     | 5       | 611 | 612 | 558 |

NUMBER OF ELEMENTS (NK) IN SYMMETRIC COMPACTED MATRIX IS 58566  
BANDWIDTH OF MATRIX IN FULL FORM WOULD BE 131  
413406 WORDS OF STORAGE HAVE BEEN USED OUT OF A TOTAL ALLOCATION OF 800000  
CALCULATIONS ARE IN DOUBLEPRECISION

AQUIFER CHARACTERISTICS  
=====

| ELEMENT NO | BOTTOM ELEVATION | AQUIFER THICKNESS | KXX       | KYY       | STORATIVITY | SPECIFIC YIELD | CONF.LAYER K'/B' |
|------------|------------------|-------------------|-----------|-----------|-------------|----------------|------------------|
| 1          | 1149.00          | 0.75              | 2.000E-02 | 2.000E-02 | 0.000E+00   | 1.500E-01      | 0.000E+00        |
| 2          | 1182.00          | 0.75              | 2.000E-02 | 2.000E-02 | 0.000E+00   | 1.500E-01      | 0.000E+00        |
| 3          | 1191.00          | 0.75              | 2.000E-02 | 2.000E-02 | 0.000E+00   | 1.500E-01      | 0.000E+00        |

PRESCRIBED HEAD BOUNDARY DATA - SPECIFIED PIEZOMETRIC HEADS AND ASSOCIATED NODE NUMBERS  
=====

| TIMES..... |  |
|------------|--|
| 0.000      |  |
| NODE NO    | HEADS UP TO AND INCLUDING THE ABOVE TIMES..... |
| 1          | 784.100  |
| 3          | 786.300  |
| 4          | 780.400  |

GROUND LEVEL DATA - FOR NODES WHICH MAY BE AFFECTED BY A RISING WATER TABLE  
=====

| TIMES..... |  |
|------------|--|
| 0.000      |  |
| NODE NO    | GROUND LEVELS UP TO AND INCLUDING THE ABOVE TIMES..... |

64 870.300  
90 876.100  
114 882.500

PRESCRIBED FLUXES DISTRIBUTED OVER ELEMENTS (L/T) - VOLUME PER UNIT TIME PER UNIT ELEMENT AREA  
E.G. EVAPOTRANSPIRATION, NATURAL RECHARGE, IRRIGATION OR DISTRIBUTED WELLS

TIMES.....

0.000

ELEMENT FLUXES ARE READ INDIVIDUALLY FOR 2272 ELEMENTS

ELEMENT NO ELEMENT FLUXES UP TO AND INCLUDING THE ABOVE TIMES ..... FLOW IN(+), FLOW OUT(-)

1 0.000000  
2 0.000000  
3 0.000000

INITIAL HEAD VECTOR

| NODE | HEAD   | NODE | HEAD   | NODE | HEAD   | NODE | HEAD   | NODE | HEAD   | NODE | HEAD   | NODE | HEAD   | NODE | HEAD   | NODE | HEAD   | NODE | HEAD   |
|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|
| 1    | 787.08 | 2    | 781.53 | 3    | 792.87 | 4    | 783.25 | 5    | 775.41 | 6    | 781.56 | 7    | 776.66 | 8    | 797.55 | 9    | 779.92 | 10   | 776.76 |

(w3in) - 60,70,80's and .02's, constant head 3e-4

TIME = 0.00000

X COORDINATES RANGE FROM 1600.00 TO 31000.00

Y COORDINATES RANGE FROM 2200.00 TO 20600.00

| NODE NO<br>----- | PIEZOMETRIC HEAD<br>----- |                 | INTERNAL FLUXES<br>-----<br>(INSIDE THE AQUIFER) |              | EXTERNAL FLUXES<br>-----<br>(THROUGH THE BOUNDARIES) |                              |                                    | ID          | LOCATION OF NODE<br>----- |           |           |
|------------------|---------------------------|-----------------|--|--------------|--|------------------------------|------------------------------------|-------------|---------------------------|-----------|-----------|
|                  | HEAD<br>(L)               | DRAWDOWN<br>(L) | QX<br>(L2/T)                                     | QY<br>(L2/T) | SOURCE/SINK<br>INFLOWS<br>(L3/T)                     | LEAKAGE<br>INFLOWS<br>(L3/T) | INFLOWS AT<br>BOUNDARIES<br>(L3/T) |             | X<br>(L)                  | Y<br>(L)  |           |
| 1                | 784.100                   | PHR             | 0.000  | -1.642       | -0.590   | 6.080                        | 0.000                              | -50.280     | 1                         | 1800.000  | 12500.000 |
| 2                | 786.689                   |                 | 0.000  | -2.364       | -1.217   | 24.932                       | 0.000                              | 0.000       | 0                         | 1941.000  | 12384.000 |
| 3                | 786.300                   | PHR             | 0.000  | -2.634       | -0.442   | 11.096                       | 0.000                              | -325.130    | 1                         | 1900.000  | 12575.000 |
| 4                | 780.400                   | PHR             | 0.000  | -2.076       | -1.311   | 11.649                       | 0.000                              | -198.960    | 1                         | 1750.000  | 12375.000 |
| 1187             | 2477.741                  |                 | 0.000  | -0.001       | 0.000  | 0.000                        | 0.000                              | 0.848       | 1                         | 27300.000 | 6400.000  |
| TOTALS           |                           |                 |  |              |  | 129318.170                   | 0.000                              | -113874.158 |                           |           |           |

NET FLOW INTO AQUIFER (L3/T) 15444.011

740 0.1221E+04  
743 0.1243E+04  
791 0.1246E+04  
794 0.1276E+04  
844 0.1270E+04  
897 0.1292E+04  
953 0.1270E+04  
954 1.3115E+03  
1073 0.1240E+04  
1011 0.1250E+04  
1074 0.1250E+04  
1072 0.1263E+04  
1071 0.1275E+04  
1070 0.1295E+04  
1127 0.1280E+04  
1129 0.1270E+04  
1130 0.1261E+04  
1128 0.1254E+04  
1138 1.2134E+03  
1137 1.1923E+03  
1141 1.1782E+03  
1086 0.1181E+04  
1028 1.1583E+03  
971 0.1150E+04  
972 1.1552E+03  
973 0.1167E+04  
923 0.1141E+04  
921 0.1128E+04  
977 0.1131E+04  
1033 0.1138E+04  
1038 0.1160E+04  
1048 0.1166E+04  
1049 0.1177E+04  
990 0.1195E+04  
991 0.1189E+04  
994 0.1188E+04  
992 0.1182E+04  
993 0.1184E+04  
937 1.2155E+03  
938 1.1953E+03  
883 0.1212E+04  
884 0.1173E+04  
829 0.1194E+04  
830 0.1161E+04  
777 1.1935E+03  
727 0.1178E+04  
673 0.1224E+04  
674 0.1160E+04  
616 1.1734E+03  
617 0.1119E+04  
618 0.1103E+04  
619 0.1088E+04  
561 0.1086E+04  
562 0.1057E+04  
563 0.1056E+04  
509 0.1041E+04  
451 1.0462E+03  
452 0.9952E+03  
453 0.9802E+03  
501 0.9771E+03  
502 0.9825E+03  
503 0.9924E+03  
491 0.9951E+03  
437 0.9955E+03  
379 0.1003E+04  
319 0.1009E+04  
273 0.1009E+04  
229 0.1021E+04  
190 0.9202E+03  
191 0.9892E+03  
192 0.1014E+04  
200 0.9601E+03  
241 0.9793E+03  
284 0.1001E+04  
339 0.9419E+03  
337 0.9068E+03  
336 0.9380E+03  
338 0.8971E+03  
392 0.8792E+03  
533 1.0431E+03  
370 1.0772E+03  
534 1.0765E+03  
479 0.9399E+03  
457 0.9199E+03  
55 0.8861E+03  
56 0.9653E+03  
68 0.8355E+03  
85 0.9530E+03  
759 1.0539E+03  
326 1.0731E+03  
282 0.9011E+03  
180 0.9314E+03  
171 1400.943  
174 1448.297  
172 1480.925  
209 1522.821  
210 1560.121  
251 1614.633  
250 1637.076  
294 1671.001

295 1664.733  
 296 1685.690  
 351 1742.159  
 404 1759.040  
 405 1763.306  
 462 1753.879  
 519 1776.177  
 572 1780.716  
 573 1739.730  
 630 1735.850  
 689 1770.227  
 741 1785.499  
 790 1818.386  
 792 1833.794  
 841 1929.267  
 893 2080.001  
 949 2129.271  
 1004 2177.244  
 1062 2352.865  
 1118 2523.619  
 1121 2511.157  
 1153 2499.175  
 1169 2759.826  
 1175 2929.080  
 1174 2933.627  
 1173 2848.057  
 1172 2737.372  
 1171 2600.323  
 1182 2570.405  
 1187 2477.741  
 1179 2274.792  
 1185 2415.027  
 1186 2363.224  
 1184 2464.829  
 1183 2405.875  
 1181 2314.643  
 1168 2249.092  
 1151 2167.190  
 1107 2115.208  
 1045 2025.657  
 987 1897.865  
 935 1802.267  
 882 1747.065  
 828 1737.439  
 776 1734.298  
 724 1743.954  
 672 1779.004  
 671 1826.338  
 670 1842.785  
 669 1832.062  
 613 1784.527  
 612 1741.509  
 611 1741.823  
 557 1697.390  
 556 1673.523  
 505 1623.008  
 504 1576.969  
 449 1520.108  
 393 1479.937  
 333 0842.920  
 279 0826.200  
 237 0804.451  
 236 0787.860  
 235 0778.048  
 234 0772.820  
 483 1069.810  
 429 1120.900  
 420 1178.090  
 381 920.500  
 371 1112.000  
 1112 1129.700  
 1104 1116.160  
 1091 1264.180  
 368 1099.890  
 126 0.8419e+03  
 369 1.0164e+03  
 426 1.0174e+03  
 293 0.9152e+03  
 1093 1119.500  
 1068 1420.000  
 916 1128.400  
 283 909.900  
 84 944.500  
 1029 1241.700  
 268 937.630  
 240 893.350  
 160 819.880  
 154 900.900  
 228 908.500  
 549 974.100  
 1056 1147.295  
 999 1104.400  
 1092 1100.500  
 1055 1163.200  
 1053 1155.400  
 825 1008.700  
 872 1045.240  
 778 1050.345  
 834 1046.600  
 396 921.300



0.0000  
 64 0.8703E+03  
 90 0.8761E+03  
 114 0.8825E+03  
 147 0.8931E+03  
 162 0.9071E+03  
 163 0.9171E+03  
 136 0.9157E+03  
 107 0.9285E+03  
 108 0.9468E+03  
 133 0.9554E+03  
 164 0.9657E+03  
 169 0.9625E+03  
 181 0.9571E+03  
 182 0.9610E+03  
 214 0.9684E+03  
 213 0.9728E+03  
 218 0.9786E+03  
 219 0.9845E+03  
 216 0.1010E+04  
 217 0.1026E+04  
 215 0.1036E+04  
 256 0.1015E+04  
 302 0.1005E+04  
 306 0.1005E+04  
 360 0.1008E+04  
 359 0.1017E+04  
 362 0.1021E+04  
 361 0.1034E+04  
 416 0.1038E+04  
 464 0.1040E+04  
 520 0.1043E+04  
 527 0.1047E+04  
 581 0.1049E+04  
 580 0.1053E+04  
 639 0.1057E+04  
 695 0.1061E+04  
 749 0.1072E+04  
 755 0.1082E+04  
 756 0.1093E+04  
 802 0.1100E+04  
 805 0.1114E+04  
 852 0.1122E+04  
 100 0.8531E+03  
 99 0.8555E+03  
 71 0.8569E+03  
 69 0.8600E+03  
 49 0.8613E+03  
 67 0.8632E+03  
 65 0.8657E+03  
 92 0.8672E+03  
 91 0.8693E+03  
 117 0.8714E+03  
 148 0.8748E+03  
 185 0.8777E+03  
 224 0.8850E+03  
 267 0.8938E+03  
 318 0.9011E+03  
 377 0.9111E+03  
 433 0.9126E+03  
 488 0.9223E+03  
 515 0.9317E+03  
 514 0.9376E+03  
 567 0.9476E+03  
 568 0.9626E+03  
 624 0.9724E+03  
 628 0.9807E+03  
 647 0.9825E+03  
 648 0.9882E+03  
 605 0.9997E+03  
 604 0.1008E+04  
 602 0.1014E+04  
 662 0.1012E+04  
 663 0.1025E+04  
 714 0.1044E+04  
 715 0.1060E+04  
 764 0.1075E+04  
 765 987.580  
 817 1002.000  
 870 1019.330  
 918 1027.600  
 919 1037.350  
 976 1056.350  
 97 771.130  
 124 781.740  
 158 783.910  
 159 785.260  
 197 791.180  
 238 809.840  
 280 830.790  
 334 845.040  
 335 847.600  
 485 1018.260  
 244 884.360  
 245 896.070  
 290 908.100  
 340 918.920  
 348 936.060  
 374 945.930  
 375 945.580

|        |             |
|--------|-------------|
| 400    | 927.740     |
| 431    | 942.320     |
| 432    | 950.240     |
| 427    | 1052.610    |
| 534    | 1076.400    |
| 438    | 970.720     |
| 421    | 1095.820    |
| 380    | 964.030     |
| 312    | 1074.100    |
| 161    | 903.920     |
| 225    | 877.450     |
| 204    | 898.390     |
| 202    | 896.960     |
| 269    | 890.400     |
| 424    | 961.160     |
| 481    | 944.440     |
| 719    | 949.640     |
| 772    | 969.010     |
| 320    | 957.820     |
| 321    | 907.970     |
| 381    | 924.810     |
| 983    | 1105.250    |
| 1042   | 1123.570    |
| 1051   | 1161.000    |
| 1054   | 1166.000    |
| 1040   | 1091.000    |
| 984    | 1187.000    |
| 880    | 1030.000    |
| 436    | 1024.000    |
| 378    | 1039.000    |
| 492    | 973.780     |
| 818    | 993.340     |
| 819    | 1007.500    |
| 249    | 898.680     |
| 264    | 903.070     |
| 998    | 1120.310    |
| 982    | 1093.620    |
| 944    | 1062.110    |
| 931    | 1043.260    |
| 914    | 1083.510    |
| 888    | 1037.470    |
| 878    | 1025.010    |
| 810    | 1089.670    |
| 807    | 1071.040    |
| 761    | 1071.390    |
| 709    | 1056.640    |
| 656    | 1043.500    |
| 203    | 877.830     |
| 243    | 864.870     |
| 316    | 931.590     |
| 543    | 1021.880    |
| 056    | 936.893     |
| 276    | 1268.300    |
| 420    | 1145.850    |
| 403    | 1144.860    |
| 315    | 929.040     |
| 1094   | 1127.640    |
| 824    | 1003.220    |
| 782    | 950.300     |
| 598    | 1031.070    |
| 549    | 975.380     |
| 439    | 938.780     |
| 093    | 791.920     |
| 482    | 1038.130    |
| 493    | 950.170     |
| 926    | 1064.800    |
| 930    | 1075.330    |
| 927    | 1090.760    |
| 928    | 1065.720    |
| 942    | 1081.920    |
| 985    | 1085.400    |
| 112    | 981.660     |
| 312    | 1073.900    |
| 48     | 0.8148e+03  |
| 94     | 0.8266e+03  |
| 399    | 0.8936e+03  |
| 382    | 0.8934e+03  |
| 270    | 0.8554e+03  |
| 226    | 0.8351e+03  |
| 246    | 0.8397e+03  |
| 364    | 1.0574e+03  |
| 387    | 1.0590e+03  |
| 1043   | 1.1080e+03  |
| 1113   | 1142.000    |
| 1057   | 1128.000    |
| 874    | 1021.000    |
| 933    | 1059.000    |
| 934    | 1069.500    |
| 929    | 1055.000    |
| 917    | 1124.600    |
| 984    | 1087.500    |
| 0.0000 |             |
|        | 10.0000E+00 |
|        | 20.0000E+00 |
|        | 30.0000E+00 |
| 1      | 787.080     |
| 2      | 781.529     |
| 3      | 792.871     |

## APPENDIX C

```

program balance
dimension a(5000),b(5000),c(5000),d(5000),e(5000),f(5000)
real inflow, outflow, recharge, rivflow
character infile*20, outfile*20, title*40

```

```

c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc

```

```

c
c This code modified by R. Allard 11/29/93 from source
c code written by David Farrel from U Of Manitoba,
c Geological/Civil Engineering Department
c

```

```

cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc

```

```

c
write(*,*) 'enter the name of the input file'
read(*,5) infile
write(*,*) 'enter the name of the output file'
read(*,5) outfile
write(*,*) 'enter title'
read(*,5) title
5 format(a20)
6 format(a40)

```

```

c
open(unit=1,file=infile,status='old')
rewind 1
read(1,*) npts,inbound,outbound,rivnodes
open(unit=2, file=outfile, status='unknown')
rewind 2
write(2,*)"total model nodes      = ", npts
write(2,*)"inbound flux nodes      = ", inbound
write(2,*)"outbound flux nodes     = ", outbound
write(2,*)"outbound river flux nodes = ", rivnodes
read(1,*) (a(i),b(i),c(i),i=1,npts)
write(*,*) a(10),b(10),c(10)
read(1,*) (d(i),i=1,inbound)
read(1,*) (e(i),i=1,outbound)
read(1,*) (f(i),i=1,rivnodes)
WRITE(*,*) d(2),e(2),f(2)
inflow=0.0
outflow=0.0
rivflow=0.0
do 20 J=1,npts
if(c(j).eq.1.0)then
do 10 k=1,inbound
if(a(j).eq.d(k))then
r=d(k)
inflow=inflow + b(j)
write(2,*)"node= ",r," flux in= ",b(j)," cum flux in= ",inflow
end if
10 continue
end if
20 continue
write(2,*)"
do 40 J=1,npts
if(c(j).eq.1.0)then

```

```

do 30 I=1,outbound
  if(a(j).eq.e(i))then
    p=e(i)
    outflow=outflow + b(j)
    write(2,*)"node= ",p," flux out= ",b(j)," cum flux out= ",outflow
  end if
30 continue
end if
40 continue
write(2,*)"
do 60 J=1,npts
  if(c(j).eq.1.0)then
    do 50 k=1,rivnodes
      if(a(j).eq.f(k))then
        s=f(k)
        rivflow=rivflow + b(j)
        write(2,*)"node= ",s," river out= ",b(j),"cum river out=",rivflow
      end if
50 continue
    end if
60 continue
recharge=inflow-outflow
write(2,*)" total flux out= ",outflow
write(2,*)" total flux in = ",inflow
write(2,*)" total recharge= ",recharge
write(2,*)" total river flow= ",rivflow
close (unit=1)
close (unit=2)
stop
end

```

```

program addhead
dimension a(1000),b(1000),c(1000)
character infilea*20,outfile*20,title*40
real delta
integer a

c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc
c
c   This code written by R. Allard 11/29/93 at U Of
c   Manitoba, Geological/Civil Engineering Department
c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc
c
  write(*,*) 'name of upper recharge boundary elev file?'
  read(*,5) infilea
  write(*,*) infilea
  write(*,*) 'name for modified file?'
  read(*,5) outfile
  write(*,*) outfile
  write(*,*) 'enter title'
  read(*,6) title
5  format(a20)
6  format(a40)
c
  write(*,*) "how much do you wish to modify heads by in m?"
  read (*,*) delta
  open(unit=1,file=infilea,status='old')
  rewind 1
  open(unit=2, file=outfile, status='unknown')
  rewind 2
  read(1,*) nnodea,nnodeb
  do 10 i=1,nnodea
    read(1,*) a(i),b(i)
    c(i)= b(i) + delta
    write(2,8) a(i),c(i)
8   format(4X,15,1x,E10.4)
10  continue
    write(2,*)""
    do 20 i=1,nnodeb
      read(1,*) a(i),b(i)
      c(i)= b(i) + delta
      write(2,18) a(i),c(i)
18  format(4X,15,1x,E10.4)
20  continue
    close (unit=1)
    close (unit=2)
    stop
    end

```

```

program aquiprop
dimension a(10000),b(10000),c(10000),d(10000),e(10000)
dimension f(10000), g(10000)
integer nelem
character infilea*20,infileb*20,infilec*20,infiled*20
character outfile*20,title*40

```

```

c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc

```

```

c
c This code written by R. Allard 11/29/93 at U Of
c Manitoba, Geological/Civil Engineering Department

```

```

c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc

```

```

c
write(*,*) 'enter the name of the elevation input file'
read(*,5) infilea
write(*,*) infilea
write(*,*) 'enter the name of the aquifer thickness file'
read(*,5) infileb
write(*,*) infileb
write(*,*) 'enter the name of the transmissivity input file'
read(*,5) infilec
write(*,*) infilec
write(*,*) 'enter the name of the storativity input file'
read(*,5) infiled
write(*,*) infiled
write(*,*) 'enter the name of the output file'
read(*,5) outfile
write(*,*) outfile
write(*,*) 'enter title'
read(*,5) title
5 format(a20)
6 format(a40)

```

```

c
write(*,*) 'enter the number of elements to assign'
write(*,*) 'properties to '
read(*,*) nelem
write(*,*) nelem
open(unit=1,file=infilea,status='old')
rewind 1
open(unit=2,file=infileb,status='old')
rewind 2
open(unit=3,file=infilec,status='old')
rewind 3
open(unit=4,file=infiled,status='old')
rewind 4
open(unit=5, file=outfile, status='unknown')
rewind 5
read(1,*) (a(i),i=1,nelem)
read(2,*) (b(i),i=1,nelem)
read(3,*) (c(i),i=1,nelem)
read(4,*) (d(i),i=1,nelem)
do 7 i=1,nelem
f(i)=a(i)-b(i)

```



```

7 continue
  write(5,8) (i,f(i),b(i),c(i),c(i),e(i),d(i),g(i),i=1,nelem)
8 format(i10,e10.4,e10.4,e10.4,e10.4,e10.4,e10.4,e10.4)
close (unit=1)
close (unit=2)
close (unit=3)
close (unit=4)
close (unit=5)
stop
end

```

```

program compare
dimension a(5000),b(5000),c(5000),d(5000),e(5000)
dimension f(5000),u(5000)
integer nnode,numel,an,bn,cn,dn
real sum
character infilea*20,infileb*20
character outfile*20,title*40

```

```

c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc

```

```

c
c   This code written by R. Allard 11/29/93 at U Of
c   Manitoba, Geological/Civil Engineering Department

```

```

c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc

```

```

c
write(*,*) 'enter the name of the original node elevation file'
read(*,5) infilea
write(*,*) infilea
write(*,*) 'enter the name of modified aquifer head file'
read(*,5) infileb
write(*,*) infileb
write(*,*) 'enter the name of your output file'
read(*,5) outfile
write(*,*) outfile
write(*,*) 'enter title'
read(*,5) title

```

```

5  format(a20)
6  format(a40)

```

```

c
nnode=1187
numel=2272
open(unit=1,file=infilea,status='old')
rewind 1
open(unit=2,file=infileb,status='old')
rewind 2
open(unit=3, file=outfile, status='unknown')
rewind 3
read(1,*) (a(i),i=1,nnode)
read(1,*) (f(i),i=1,numel)
do 10 i=1,numel
read(1,*)an,bn,cn,dn
if(f(i).eq.0.0)then
u(cn)=0.0
u(bn)=0.0
u(dn)=0.0
else
u(cn)=1.0
u(bn)=1.0
u(dn)=1.0
end if
10 continue
read(2,*) (d(i),e(i),b(i),i=1,nnode)
do 20 i=1,nnode
c(i)=b(i)-a(i)

```

```

20  continue
    sum=0.0
    write(3,*)"lower recharge area"
    write(3,*)"
    do 40 i=1,nnode
        if(u(i).ne.0.0) then
            c(i)=b(i)-a(i)
            sum=sum+c(i)
            write(3,30) i,a(i),b(i),d(i),e(i),c(i)
30  format(i10,1x,f8.3,1x,f8.3,1x,f8.3,1x,f8.1,1x,f8.1,1x,f8.3)
            end if
40  continue
    write(3,*)"sum= ",sum
    write(3,*)"
    sum=0.0
    write(3,*)"upper recharge area"
    write(3,*)"
    do 60 i=1,nnode
        if(u(i).eq.0.0) then
            c(i)=b(i)-a(i)
            sum=sum+c(i)
            write(3,50) i,a(i),b(i),d(i),e(i),c(i)
50  format(i10,1x,f8.3,1x,f8.3,1x,f8.3,1x,f8.1,1x,f8.1,1x,f8.3)
            end if
60  continue
    write(3,*)"sum= ",sum
    write(3,*)"
    close (unit=1)
    close (unit=2)
    close (unit=3)
    stop
end

```

```

program elemconv
dimension x(10000),y(10000),z(10000)
integer x,y,z
character infile*20,outfile*20,title*40

```

```

c
c
c This code modified by R. Allard 11/29/93 from source
c code written by David Farrel from U Of Manitoba,
c Geological/Civil Engineering Department
c

```

```

c
c
c write(*,*) 'enter the name of the input file'
c read(*,5) infile
c write(*,*) 'enter the name of the output file'
c read(*,5) outfile
c write(*,*) 'enter title'
c read(*,6) title
5 format(a20)
6 format(a40)

```

```

c
c
c open(unit=1,file=infile,status='old')
c rewind 1
c read(1,*) nelem
c open(unit=2, file=outfile, status='unknown')
c rewind 2
c write(2,*) nelem
c write(*,*) nelem
c read(1,*) (x(i),y(i),z(i),i=1,nelem)
c write(*,*) x(1),y(1),z(1)
c write(2,15) (i,x(i),y(i),z(i),i=1,nelem)
15 format(i10,i10,i10,i10)
c close (unit=1)
c close (unit=2)
c stop
c end

```

```

program nodconv
dimension x(5000),y(5000)
character infile*20,outfile*20,title*40

```

```

c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc

```

```

c
c   This code modified by R. Allard 11/29/93 from source
c   code written by David Farrel from U Of Manitoba,
c   Geological/Civil Engineering Department

```

```

c
cccccccccccccccccccccccccccccccccccccccccccccccccccccccccccc

```

```

c
write(*,*) 'enter the name of the input file'
read(*,5) infile
write(*,*) 'enter the name of the output file'
read(*,5) outfile
write(*,*) 'enter title'
read(*,5) title
5 format(a20)
6 format(a40)

```

```

c
open(unit=1,file=infile,status='old')
rewind 1
read(1,*) npts
open(unit=2, file=outfile, status='unknown')
rewind 2
write(2,*) npts
read(1,*) (x(i),y(i),i=1,npts)
write(2,15) (i,x(i),y(i),i=1,npts)
15 format(i10,f10.3,f10.3)
close (unit=1)
close (unit=2)
stop
end

```

15

13

1



```

write(*,*) '**
write(*,*) /*****
write(*,2501)
2501 format (////)
write(*,*) 'enter 1 to continue'
write(*,*) sgr0
read(*,*) icon
if (icon.ne.1) go to 1312

write(*,520) ed
520 format(1x,a)
write(*,*) 'enter the title for this work -> '
read(*,1) title
1 format(a50)
c
c
c main problem parameters
c
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'the following MAIN PROBLEM PARAMETERS are required'
write(*,*) 'refer to the AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'enter F (false) or T (true) when prompted'
write(*,*) 'linear analysis (T); non-linear analysis (F) -> '
read(*,2) linear
write(*,*) 'steady analysis (T); un-steady analysis (F) -> '
read(*,2) steady
write(*,*) 'program computes initial guess (T); user supplies init
#ial guess (F) -> '
read(*,2) initial
write(*,*) 'final steady state solution required using b.c. at tim
#e=endtime (T); otherwise (F) -> '
read(*,2) final
write(*,*) 'execution stops after printing and plotting finite ele
#ment grid (T); program runs to completion (F) -> '
read(*,2) check
2 format(l1)
write(*,*) /*****
c
c
c geometric parameters
c
write(*,520) ed
WRITE(*,1) TITLE
write(*,*) /*****
write(*,*) 'GEOMETRIC PARAMETERS'
write(*,*) 'geometric data to be printed out (T); otherwise (F) ->
# '
write(*,*) 'Enter the name of the Geometric Parameter file'
read(*,1399) card3
open(unit=30,file=card3,status='old')
rewind 30

```

```

read(30,*) numel,numnp
read(30,2) prgeom
read(30,2) plgeom
read(30,*) xscale,yscale,maxelt,maxnod
close(unit=30)
write(*,*) '*****'

```

aquifer property parameters

```

write(*,520) ed
write(*,*) '*****'
write(*,520) sgr1
write(*,*) 'AQUIFER PROPERTY PARAMETERS'
write(*,*) 'refer to card 4, p179 AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'enter naqr -> '
read(*,*) naqr
write(*,*) 'enter nspec -> '
read(*,*) nspec
write(*,*) 'enter bynode -> '
read(*,*) bynode
write(*,*) 'enter perm -> '
read(*,*) perm
write(*,*) '*****'

```

boundary and initial conditions

```

write(*,520) ed
write(*,*) '*****'
write(*,520) sgr1
write(*,*) 'BOUNDARY AND INITIAL CONDITIONS'
write(*,*) 'refer to card 5, p180 AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the Boundary and Initial Conditions'
# file --> '
read(*,1399) card5
open(unit=26,file=card5,status='old')
rewind 26
read(26,*) nhnode,ntbh,ngrd,ntgrd,nflxe,ntflxe,nefr
read(26,*) nflxs,ntflxs,nflxn,ntflxn,nbc3,ntbc3,nnod3
read(26,2) bedbc3
read(26,*) nhadj,nthadj
read(26,2) attop
read(26,2) havary
read(26,2) icvary
close(unit=26)
write(*,*) '*****'

```

time integration and iteration parameters

```

write(*,520) ed

```

```

write(*,*) /*****
write(*,520) sgr1
write(*,*) 'TIME INTEGRATION AND ITERATION PARAMETERS'
write(*,*) 'refer to card 6, p182 AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the Integration Parameters file -->
# '
read(*,1399) card6
open(unit=27,file=card6,status='old')
rewind 27
read(27,*) strtim,endtim,tol,itol,maxit
read(27,*) dt,alpha,dtparm,idt,ndt,nsys
close(unit=27)
write(*,*) /*****

```

```

c
c
c output control parameters
c

```

```

write(*,520) ed
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'OUTPUT CONTROL PARAMETERS'
write(*,*) 'refer to card 7, p183, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the Output Control Parameters file
# --> '

```

```

read(*,1399) card7
open(unit=28,file=card7,status='old')
rewind 28
read(28,*) istprt,ndtpprt,nout,istplt,ndtplt
read(28,*) nplt,pscale,pdelta,nrflag,nbound,ndp
close(unit=28)
write(*,*) /*****

```

```

c
c
c node point coordinates
c

```

```

write(*,520) ed
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'NODE POINT COORDINATES'
write(*,*) 'refer to card 8, p184, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'enter the name of the input node file **.NOD -> '
read(*,5) innode
940 write(*,*) 'ENTER THE VERSION OF GRDBLDR USED TO CREATE GRID'
write(*,*) 'enter 1 for files created by GRDBLDR V1.0 --> '
write(*,*) 'enter 2 for files created by GRDBLDR V2.0 --> '
read(*,*) iver

```

```

c
c reading the node file
c

```

```

if (iver.eq.1) then
open(unit=1,file=innode,form='formatted',status='old')

```

```

rewind 1
read(1,*) numnp
c 10 format(i10)
c do 601 i=1,numnp
c read(1,11) ndmb,x(i),y(i)
c 601 write(*,*) ndmb,x(i),y(i)
read(1,11) (ndmb,x(i),y(i),i=1,numnp)
11 format(i10,2f10.0)
c 11 format(8e15.8)
close(unit=1)
write(*,*) /*****/

c
c
c element connectivities

c
c
c write(*,520) ed
c write(*,*) /*****/
c write(*,520) sgr1
c write(*,*) 'ELEMENT CONNECTIVITIES'
c write(*,*) 'refer to card 9, p185, AQUIFEM user manual'
c write(*,520) sgr0
c write(*,*) 'enter the name of the input element file **.INC -> '
c read(*,5) inelem

c
c reading the element file

c
c open(unit=3,file=inelem,form='formatted',status='old')
c rewind 3
c read(3,*) numel
c do 602 j=1,numel
c read(3,30) (ndmb,in(j,1),in(j,2),in(j,3),j=1,numel)
c 602 write(*,*) ndmb,in(j,1),in(j,2),in(j,3)
30 format(4i10)
c 30 format(26i5)
close(unit=3)
else
c reading version 2 files.
if (iver.eq.2) then
open(unit=1,file=innode,form='formatted',status='old')
rewind 1
read(1,*) numnp
c 10 format(i10)
c do 6001 i=1,numnp
c read(1,11) ndmb,x(i),y(i)
c 6001 write(*,*) ndmb,x(i),y(i)
read(1,411) (ndmb,x(i),y(i),i=1,numnp)
411 format(i10,2f10.2)
c 411 format(7(e15.8,1x))
close(unit=1)
write(*,*) /*****/

c
c
c element connectivities
c

```

```

write(*,520) ed
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'ELEMENT CONNECTIVITIES'
write(*,*) 'refer to card 9, p185, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'enter the name of the input element file **.INC -> '
read(*,5) inelem

c
c reading the element file
c

open(unit=3,file=inelem,form='formatted',status='old')
rewind 3
read(3,*) numel
c do 6002 j=1,numel
read(3,340) (ndmb,in(j,1),in(j,2),in(j,3),j=1,numel)
c 6002 write(*,*) ndmb,in(j,1),in(j,2),in(j,3)
340 format(4i10)
c 340 format(20(i5,1x))
close(unit=3)
else
write(*,*) 'INCORRECT VERSION NUMBER'
go to 940
endif
endif
write(*,*) /*****

c
c
c default aquifer properties
c

write(*,520) ed
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'DEFAULT AQUIFER PROPERTIES'
write(*,*) 'refer to card 10, p186, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the default properties file -> '
read(*,1399) dname
open(unit=25,file=dname,status='old')
rewind 25
read(25,*) (aqprop(il), il=1,7)
close(unit=25)
write(*,*) /*****

c
c
c number of nodes/elements in each aquifer property region
c

if (naqr.gt.0) then
write(*,520) ed
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'NUMBER OF NODES/ELEMENTS IN EACH AQUIFER PROPERTY REGI
#ON'
write(*,*) 'refer to cards 11 & 12, p186, AQUIFEM user manual'

```

```

write(*,520) sgr0
write(*,*) 'number of nodes/elements in the mth region of the aquifer has uniform aquifer properties different from the default value'
#es'
write(*,*) naqr,' regions specified'
write(*,*) 'Enter the name of the node/element file: k region --> '
# '
read(*,1399) rfile
1399 format(a20)
open(unit=10,file=rfile,status='old')
rewind 10
read(10,*) (naqreg(m),m=1,naqr)
c 100 format(14i5)
c write(*,*) '*****'
c
c
c
c node/element numbers for aquifer property regions
c
c write(*,520) ed
c write(*,*) '*****'
c write(*,*) 'NODE/ELEMENT NUMBERS FOR AQUIFER PROPERTY REGIONS'
c write(*,*) 'refer to card 12, p187, AQUIFEM user manual'
do 102 k=1,naqr
read(10,*) (num(k,n),n=1,naqreg(k))
c 1400 format(14i5)
c reading aquifer properties
read(10,*) (aqprop(k,j),j=1,7)
c 1401 format(7f8.3)
102 continue
close(unit=10)
write(*,520) ed
write(*,*) '*****'
endif
c
c
c aquifer properties of individual nodes/elements
c
if (nspec.gt.0) then
write(*,520) ed
write(*,*) '*****'
write(*,520) sgr1
write(*,*) 'AQUIFER PROPERTIES OF INDIVIDUAL NODES/ELEMENTS'
write(*,*) 'refer to card 13, p187, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the Aquifer Properties File --> '
read(*,1399) afile
open(unit=12,file=afile,status='old')
rewind 12
do 104 i=1,nspec
104 read(12,*) nmb(i),(aqprop(i,ni),ni=1,7)
c 1402 format(i5,7f8.3)
close(unit=12)
write(*,520) ed
write(*,*) '*****'

```

```

endif
c
c
c times for fixed head boundary conditions
c
if (nhnode.gt.0) then
write(*,520) ed
write(*,*) /*****/
write(*,520) sgr1
write(*,*) 'FIXED HEAD BOUNDARY CONDITIONS'
write(*,*) 'refer to cards 14 & 15, p188, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the Fixed Head Boundary File --> '
read(*,1399) hfile
open(unit=11,file=hfile,status='old')
rewind 11
read(11,*) (tbh(i),i=1,ntbh)
c 1510 format(9f8.3)
c write(*,*) /*****/
c
c fixed head (1st type) boundary condition
c
c write(*,520) ed
c write(*,*) 'FIXED HEAD (1st TYPE) BOUNDARY CONDITION'
c write(*,*) 'refer to card 15, p188, AQUIFEM user manual'
c do 1006 i=1,nhnode
c read(11,*) nbhn(i),(hnode(m,i),m=1,ntbh)
c 1403 format(i5,8f8.3)
1006 continue
close(unit=11)
write(*,520) ed
write(*,*) /*****/
endif
c
c
c times for 1st type rising water ground levels
c
if (ntgrd.gt.0) then
write(*,520) ed
write(*,*) /*****/
write(*,520) sgr1
write(*,*) '1st TYPE RISING WATER GROUND LEVELS'
write(*,*) 'refer to cards 16 & 17, p189, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the Rising Water Ground Level Data
# file --> '
read(*,1399) rwgfile
open(unit=13,file=rwgfile,status='old')
rewind 13
read(13,*) (tgrd(i),i=1,ntgrd)
c write(*,*) /*****/
endif
c

```



```

c
c 1st TYPE RISING WATER GROUND LEVEL DATA
c
c if (ngrd.gt.0) then
c   write(*,520) ed
c   write(*,*) /*****
c   write(*,*) '1st TYPE RISING WATER GROUND LEVEL DATA'
c   write(*,*) 'refer to card 17, p189, AQUIFEM user manual'
c   do 108 i=1,ngrd
108   read(13,*) nodgrd(i),(grd(m,i),m=1,ntgrd)
c 1406 format(i5,5f8.3)
c   close(unit=13)
c   write(*,520) ed
c   write(*,*) /*****
c   endif
c
c times for prescribed element fluxes
c
c if (nflxe.gt.0) then
c   write(*,520) ed
c   write(*,*) /*****
c   write(*,520) sgr1
c   write(*,*) 'TIMES FOR PRESCRIBED ELEMENT FLUXES'
c   write(*,*) 'refer to card 18, p190, AQUIFEM user manual'
c   write(*,520) sgr0
c   write(*,*) 'Enter the name of the Regionally Defined Flux File -->
# '
c   read(*,1399) rdffile
c   open(unit=14,file=rdffile,status='old')
c   rewind 14
c   read(14,*) (tflxe(i),i=1,ntflxe)
c   write(*,*) /*****
c   endif
c
c regionally defined element fluxes
c
c if (nflxe.gt.0.and.nefr.gt.0) then
c   write(*,520) ed
c   write(*,*) /*****
c   write(*,*) 'REGIONALLY DEFINED ELEMENT FLUXES'
c   write(*,*) 'refer to card 19, p190, AQUIFEM user manual'
c   do 111 i=1,nefr
111   read(14,*) nqreg(i),(qreg(i,m),m=1,ntflxe)
c 1408 format(i5,5f8.3)
c   close(unit=14)
c   write(*,520)
c   write(*,*) /*****
c
c element numbers in the ith flux region
c
c   write(*,520) ed

```

```

write(*,*) /*****
write(*,520) sgr1
write(*,*) 'ELEMENT NUMBERS IN ith ELEMENT FLUX REGION'
write(*,*) 'refer to card 20, p191, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the Element Number File for the var
ious flux regions --> '
read(*,1399) enffile
open(unit=16,file=enffile,status='old')
rewind 16
do 112 i=1,nEFR
if ((nqreg(i).eq.nflxe).and.(nqreg(i).eq.numel).and.(numel.eq.
#nflxe))then
go to 113
else
read(16,*) fl1
read(16,*) (nqe(i,m),m=1,nqreg(i))
c 1410 format(14i5)
endif
112 continue
close(unit=16)
write(*,520) ed
write(*,*) /*****
endif
113 continue
c
c
c element fluxes for individual elements
c
iadd=0
do 115 i=1,nEFR
115 iadd=iadd+nqreg(i)
nn=nflxe-iadd
if (nn.gt.0) then
write(*,520) ed
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'ELEMENT FLUXES FOR INDIVIDUAL ELEMENTS'
write(*,*) 'refer to card 21, p191, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of the Element Flux for Individual Elem
#ent File --> '
read(*,1399) efiefile
open(unit=17,file=efiefile,status='old')
rewind 17
do 116 i=1,nn
116 read(17,*) nqee(i),(qe(i,m),m=1,ntflxe)
c 1106 format(i5,8f8.3)
close(unit=17)
write(*,520) ed
write(*,*) /*****
endif
c
c

```

```

c   times for prescribed side fluxes
c
  if (nflxs.gt.0) then
    write(*,520) ed
    write(*,*) '*****'
    write(*,520) sgr1
    write(*,*) 'TIMES FOR PRESCRIBED SIDE FLUXES'
    write(*,*) 'refer to cards 22 & 23, p192, AQUIFEM user manual'
    write(*,520) sgr0
    write(*,*) 'Enter Side Flux Boundary file name --> '
    read(*,1399) sfbfile
    open(unit=18,file=sfbfile,status='old')
    rewind 18
    read(18,*) (tflxs(i),i=1,ntflxs)
c 117 format(9f8.2)
    write(*,*) '*****'
  endif

c
c
c   side flux (2nd type) boundary conditions
c
  if (nflxs.gt.0) then
    write(*,520) ed
    write(*,*) '*****'
    write(*,*) 'SIDE FLUX (2nd TYPE) BOUNDARY CONDITIONS'
    do 118 i=1,nflxs
118  read(18,*) nqs(1,i),(nqs(2,i),qs(j,i),j=1,ntflxs)
c 1414 format(2i5,5f8.3)
    close(unit=18)
    write(*,520) ed
    write(*,*) '*****'
  endif

c
c
c   times for prescribed nodal fluxes
c
  if (nflxn.gt.0) then
    write(*,520) ed
    write(*,*) '*****'
    write(*,520) sgr1
    write(*,*) 'TIMES FOR PRESCRIBED NODAL FLUXES'
    write(*,*) 'refer to cards 24 & 25, p193, AQUIFEM user manual'
    write(*,520) sgr0
    write(*,*) 'Enter the name of the Nodal Flux Boundary File --> '
    read(*,1399) nfbfile
    open(unit=19,file=nfbfile,status='old')
    rewind 19
    read(19,*) (tflxn(i),i=1,ntflxn)
c 119 format(9f8.2)
    write(*,*) '*****'
c
c
c   nodal flux boundary conditions
c

```

```

c      write(*,520) ed
c      write(*,*) /*****
c      write(*,*) 'NODAL FLUX BOUNDARY CONDITIONS'
c      write(*,*) 'refer to card 25, p193, AQUIFEM user manual'
      do 120 i=1,nflxn
120  read(19,*) nqn(i),(qn(m,i),m=1,ntflxn)
c 1416 format(i5,5f8.3)
      close(unit=19)
      write(*,520) ed
      write(*,*) /*****
      endif

c
c
c      times for mixed (3rd type) boundary conditions

c
      if (nbc3.gt.0) then
      write(*,520) ed
      write(*,*) /*****
      write(*,520) sgr1
      write(*,*) 'TIMES FOR MIXED (3rd TYPE) BOUNDARY CONDITIONS'
      write(*,*) 'refer to cards 26,27 & 28, p194, AQUIFEM user manual'
      write(*,520) sgr0
      write(*,*) 'Enter the name of the 3rd Type Boundary Link file'
      read(*,1399) bc3file
      open(unit=20,file=bc3file,status='old')
      rewind 20
      read(20,*) (tbc3(i),i=1,ntbc3)
c 121  format(9f8.2)
      write(*,*) /*****
c
c
c      location and properties of links on 3rd type boundary condition
c
c      write(*,520) ed
c      write(*,*) /*****
c      write(*,*) 'LOCATION AND PROPERTIES OF LINKS ON 3rd TYPE BOUNDARY
c      #CONDITION'
c      write(*,*) 'refer to card 27, p194, AQUIFEM user manual'
      do 122 i=1,nbc3
122  read(20,*) ns3(1,i),ns3(2,i),perm3(i),width(i)
c 1220 format(2i5,2f8.4)
      write(*,*) /*****
c
c
c      nodal heads on 3rd type boundary
c
c      write(*,520) ed
c      write(*,*) /*****
c      write(*,*) 'NODAL HEADS ON 3rd TYPE BOUNDARY'
c      write(*,*) 'refer to card 28, p194, AQUIFEM user manual'
      do 123 i=1,nnod3
123  read(20,*) nn3(i),bedlvl(i),(hbc3(m,i),m=1,ntbc3)
c 1420 format(i5,f8.3,5f8.3)
      close(unit=20)

```

```

write(*,520) ed
write(*,*) /*****
endif

c
c
c   times for heads in adjacent aquifers
c
   if (nhadj.GT.0) then
write(*,520) ed
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'TIMES FOR HEADS IN ADJACENT AQUIFERS'
write(*,*) 'refer to card 29, p195, AQUIFEM user manual'
write(*,520) sgr0
write(*,*) 'Enter the name of Heads in Adjacent Aquifer file --> '
read(*,1399) haafile
open(unit=22,file=haafile,status='old')
rewind 22
read(22,*) (thadj(i),i=1,nthadj)
c 124 format(9f8.2)
   write(*,*) /*****
c
c
c   heads in adjacent aquifer
c
   write(*,520) ed
   write(*,*) /*****
   write(*,*) 'HEADS IN ADJACENT AQUIFER'
   write(*,*) 'refer to card 30, p195, AQUIFEM user manual'
   if (havary) then
do 125 i=1,nhadj
125 read(22,*) nadj(i),(hadj(m,i),m=1,nthadj)
c 1422 format(i5,5f8.3)
   go to 1612
   else
do 126 m=1,nthadj
   write(*,*) 'enter head in adjacent aquifer at time ',m,' -> '
126 read(*,*) hadj(m,1)
   endif
   write(*,520)
1612 close(unit=22)
   write(*,*) /*****
   endif
c
c
c   initial conditions/guesses
c
   if ((linear.and.steady).or.inital) go to 999
write(*,520) ed
write(*,*) /*****
write(*,520) sgr1
write(*,*) 'INITIAL CONDITIONS/GUESSES'
write(*,*) 'refer to card 31, p196, AQUIFEM user manual'
write(*,520) sgr0

```

```

write(*,*) 'Enter input file name'
read(*,973) card31
973 format(a20)

open(unit=31,file=card31,status='old')
rewind 31

if (icvary) then
all nodal points must be read in

do 127 i=1,nump
127 read(31,*) nmp(i),HZ(I)
else
only one initial guess needed (applied to all nodes)

read(31,*) hzz
endif
CLOSE(UNIT=31)
write(*,*) '*****'
999 continue

special times for printed output

if (nout.gt.0) then
write(*,520) ed
write(*,*) '*****'
write(*,520) sgr1
write(*,*) 'SPECIAL TIMES FOR PRINTED OUTPUT'
write(*,*) 'refer to card 32, p197, AQUIFEM user manual'
write(*,520) sgr0
do 128 i=1,nout
write(*,*) 'enter time',i,' -> '
128 read(*,*) prtime(i)
write(*,*) '*****'
endif

special times for plotted output

if (nplt.gt.0) then
write(*,520) ed
write(*,*) '*****'
write(*,520) sgr1
write(*,*) 'SPECIAL TIMES FOR PLOTTED OUTPUT'
write(*,*) 'refer to card 33, p197, AQUIFEM user manual'
write(*,520) sgr0
do 130 i=1,nplt
write(*,*) 'enter plot time ',i,' -> '
130 read(*,*) pltime(i)
write(*,*) '*****'
endif

```

```

c writing to the output file
c
write(*,520) ed
write(*,*) /*****
write(*,*) 'WRITING TO THE OUTPUT FILE'
write(*,*) 'enter the name of the output file -> '
read(*,5) outfile
5 format(a20)
open(unit=4,file=outfile,form='formatted',status='unknown')
rewind 4
write(4,1) title
WRITE(*,1) 'CARD 1'
write(4,50) linear,steady,ital,final,check
WRITE(*,*) 'CARD 2'
50 format(5l5)
write(4,51) numel,numnp,prgeom,plgeom,xscale,yscale,maxelt,maxnod
WRITE(*,*) 'CARD 3'
51 format(2i5,2l5,2f10.3,2i5)
write(4,52) naqr,nspec,bynode,perm
52 format(2i5,2l5)
write(4,53) nhnode,ntbh,ngrd,ntgrd,nflxe,ntflxe,nfr,nflxs,ntflxs,
#nflxn,ntflxn,nbc3,ntbc3,nnod3,bedbc3,nhadj,nthadj,atop,havary,icv
#ary
53 format(11i5/3i5,l5,2i5,3l5)
write(4,54) strtim,endtim,tol,itol,maxit,dt,alpha,dtparm,idt,ndt,n
#sys
54 format(2f10.2,f5.1,2i5,f10.2,2f5.1,3i5)
write(4,55) istprt,ndtprt,nout,istplt,ndtplt,nplt,pscale,pdelta,nr
#flag,nbound,ndp
55 format(6i5,2f10.2,3i5)
do 40 i=1,numnp
40 write(4,41) i,x(i),y(i)
41 format(i10,2f10.2)
do 42 j=1,numel
42 write(4,43) j,in(j,1),in(j,2),in(j,3)
43 format(4i10)
write(4,56) (aqprop(j),j=1,7)
56 format(10x,7e12.4)
if (naqr.gt.0) then
write(4,57) (naqreg(m),m=1,naqr)
57 format(5i5)
do 58 k=1,naqr
write(4,59) (num(k,npp),npp=1,naqreg(k))
59 format(16i5)
write(4,60) (aqpropr(k,nnp),nnp=1,7)
60 format(10x,7e12.4)
58 continue
endif
if (nspec.gt.0) then
do 61 i=1,nspec
write(4,62) nmb(i),(aqpropi(i,kk),kk=1,7)
62 format(i10,7e12.4)
61 continue
endif

```



```

      if (nbc3.gt.0) then
        write(4,81) (tbc3(i),i=1,ntbc3)
81      format(8f12.4)
        do 82 i=1,nbc3
82      write(4,83) ns3(1,i),ns3(2,i),perm3(i),width(i)
83      format(2i10,2e12.5)
        do 84 i=1,nbc3
84      write(4,85) nn3(i),bedlvl(i),(hbc3(m,i),m=1,ntbc3)
85      format(i10,7e12.5/(8e12.5))
        endif
        if (nhadj.gt.0) then
          write(4,86) (thadj(i),i=1,nthadj)
86      format(8f12.4)
          if (havary) then
            do 87 i=1,nhadj
87      write(4,88) nadj(i),(hadj(m,i),m=1,nthadj)
            else
              write(4,88) idum,(hadj(m,1),m=1,nthadj)
            endif
88      format(i10,7e12.5/(8e12.5))
          endif
          if ((linear.and.steady).or.inital) go to 998
          if (icvary) then
            do 89 i=1,numnp
89      write(4,90) nmpp(i),hz(i)
            else
              write(4,90) idum,hzz
            endif
90      format(i10,e12.5)
998      continue
          if (nout.gt.0) then
            write(4,92) (prtime(i),i=1,nout)
92      format(8f12.4)
          endif
          if (nplt.gt.0) then
            write(4,93) (pltime(i),i=1,nplt)
93      format(8f12.4)
          endif
          close(unit=4)

c
      stop
      end

```

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Directory of C:\GRID

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| W.IN3 | W.GIF | W.BNI | W.N00 | W.INC |
| W.BNL | W.F01 | W.T01 | W.T02 | W.T03 |
| W.T04 | W.T05 | W.T06 | W.T07 | W.T08 |
| W.E03 | W.B01 | W.T09 | W.E04 | W.DIG |
| W.GEN | W.GRD | W.XYC | W.E05 | W.E06 |
| W.E07 | W.E08 | W.E09 | W.T10 | W.T11 |
| W.T13 | W.ELA | W.N01 | W.T14 | W.E10 |
| W.E11 | W.T15 | W.T16 | W.E12 | W.E14 |
| W.E15 | W.T17 | W.T18 | W.T19 | W.T20 |
| W.T21 | W.T22 | W.T23 | W.E16 | W.E17 |
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| W.IN3 | W.GIF | W.BNI | W.N00 | W.INC |
| W.BNL | W.F01 | W.T01 | W.T02 | W.T03 |
| W.T04 | W.T05 | W.T06 | W.T07 | W.T08 |
| W.E03 | W.B01 | W.T09 | W.E04 | W.DIG |
| W.GEN | W.GRD | W.XYC | W.E05 | W.E06 |
| W.E07 | W.E08 | W.E09 | W.T10 | W.T11 |
| W.T13 | W.ELA | W.N01 | W.T14 | W.E10 |
| W.E11 | W.T15 | W.T16 | W.E12 | W.E14 |
| W.E15 | W.T17 | W.T18 | W.T19 | W.T20 |
| W.T21 | W.T22 | W.T23 | W.E16 | W.E17 |
| W.E18 | W.T24 | W.E19 | W.T25 | W.E20 |

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